Fast Rate Li-Ion Battery Charger

by Goran Perica

Introduction
The recent trend in notebook computers has been toward increasing battery operating time and faster processor speeds. These two requirements, in conjunction with a need for faster battery recharging (1–2 hours), have placed a strain on battery charging circuits and wall adapters. A typical notebook computer system configuration is shown in Figure 1.

Wall adapters are typically AC/DC converters with a 20V output at 3A–4A of load current. When a notebook computer is running, all of the available current from the wall adapter may be consumed by the system, with no power left for charging the battery. However, as soon as the system’s power requirements drop below the wall adapter’s current limit, the battery charging can resume. In order to recharge the battery in the shortest time possible, the recharging should start as soon as there is any current left over from the system. The ideal situation is when the sum of battery charging current and the system current is just below the wall adapter’s current limit:

\[ I_{IN\_MAX} > I_{SYS} + I_{CHARGER} \]

where \( I_{IN\_MAX} \) is the wall adapter current limit, \( I_{SYS} \) is the system load current and \( I_{CHARGER} \) is the battery charger current.

To achieve this objective, it is necessary to adjust the battery charger current so that the sum of the two currents is just below the maximum available input current, \( I_{IN\_MAX} \). The LT1505 incorporates a patented battery charger input current limiting function along with other functions necessary to provide a complete, single-chip battery charging circuit solution.

LT1505 Features
The LT1505 is a constant-current (CC), constant-voltage (CV) current mode switching battery charger circuit with the following features:

- 0.5% voltage reference
- 5% output current regulation
- Output voltage is preset for 3 or 4 Li-Ion cells (12.3V, 12.6V, 16.4V and 16.8V)
- Output voltage is programmable from 1V to 21V
- Low \( V_{IN} \)-to-\( V_{OUT} \) operation (dropout <0.5V)
- Programmable AC wall adapter current limiting
- Programmable peak battery charging current
- Battery drain <10\( \mu \)A in shutdown
- 94% efficiency

Circuit Description
The LT1505 is a synchronous buck converter using N-channel MOSFETs. The LT1505 operates at 200kHz and can be synchronized to an external clock with a frequency higher than 240kHz. The LT1505 IC has an undervoltage lockout circuit that detects the presence of an input power source and enables the battery charging. Once the undervoltage lockout has been exceeded, the PWM will start running and the input MOSFET M3 is turned ON, thus reducing the voltage drop across its internal body diode \( D_{BODY} \) (see Figure 2).

The LT1505 monitors the current from the wall adapter and controls the battery charger current. For example, if a 3A, 20V wall adapter is used along with a 12.6V Li-Ion battery pack, the peak battery charging current, when the system is off, can be set to:

\[ I_{BATT\_MAX} = \eta \times I_{IN\_MAX} \times \frac{V_{IN}}{V_{BATT}} \]

where \( I_{BATT\_MAX} \) is the maximum battery charging current when the system is idle, \( \eta \) is the efficiency of battery charger, \( V_{IN} \) is the wall adapter output voltage and \( V_{BATT} \) is the battery charging voltage.

Assuming an efficiency of 90%, the above example could provide battery charging current in excess of 4A. The LT1505 will reduce the battery charging current as soon as the system current exceeds \( I_{IN\_MAX} - I_{CHARGER} \) by 1A. The resulting battery charging current \( I_{BATT} \) will be:

\[ I_{BATT} = \eta \times I_{CHARGER} \times \frac{V_{IN}}{V_{BATT}} \]

or

\[ I_{BATT} = 0.9 \times 1A \times 20V / 12.6V = 1.428A \]

The input current from the wall adapter passes through a current sense resistor, \( R_{S4} \). One part of the input current goes to the system load and the remaining part goes to the LT1505 battery charger. The voltage drop across \( R_{S4} \) is monitored by a current comparator with a 90mV threshold. Once the threshold of 90mV is reached, the LT1505 will reduce the programmed battery charging current so that the peak input current does not exceed the preset limit. Thus, the maximum input current \( I_{IN\_MAX} \) will be:

\[ I_{IN\_MAX} = I_{SYSTEM} + I_{CHARGER} = 0.090V/R_{S4} \]
where $I_{\text{SYSTEM}}$ is the system load current, $I_{\text{CHARGER}}$ is the LT1505 battery charger current and $R_{S4}$ is the current sense resistor. With the resistor value of 0.025Ω in Figure 2, the input current limit $I_{\text{IN MAX}}$ will be set to 3.6A.

The battery charging current limit is set by $R_{\text{PROG}}$, $R_{S1}$ and $R_{S2}$ and is:

$$I_{\text{BAT MAX}} = \left( \frac{V_{\text{PROG}}}{R_{\text{PROG}}} \right) \times \left( \frac{R_{S2}}{R_{S1}} \right)$$

where $V_{\text{PROG}}$ is the reference voltage of 2.465V. The values in Figure 2 have been selected for a current limit ($I_{\text{BAT MAX}}$) of 4A. Changing $R_{S1}$ to 0.050Ω will set the $I_{\text{BAT MAX}}$ to 2A.

Also, the peak battery charging current ($I_{\text{BAT MAX}}$) can be programmed by the host computer. The $I_{\text{BAT MAX}}$ can be set in increments of 0.25A if $R_{\text{PROG}}$ is replaced by a network of resistors, as shown in Figure 3.

The battery charger in Figure 2 achieves high efficiency thanks to synchronous operation and input power FET. The efficiency is as high as 94%, as can be seen in Figure 4.

**PCB Layout**

When laying out the PCB, a multilayer layout with one of the inner layers as a solid ground plane is recommended. The LT1505 and low power components associated with it should be kept as close together as possible. Additionally, all power components should be kept together and next to LT1505 control circuitry. The goal is to keep all high power switching currents as localized as possible. Components that connect to the ground plane should have vias placed as close as possible to the pins connected to the ground plane. Also, power components should have larger or multiple vias connecting to the ground plane. Avoid placing the power components in such a way that input and output currents flow by the LT1505 IC. Also, to keep the component temperature rise low, use as much copper as possible. The use of polygon planes for high power nets such as the ones connecting to $V_{\text{IN}}$, $V_{\text{CC}}$, continued on page 35
band gain can be higher than 0dB or if internal nodes are allowed to have gains higher than 0dB. Please contact the LTC Filter Design and Applications Group for further details.

The low noise behavior of the filter makes it useful in applications where the input signal has a wide voltage range. This is true provided the filter magnitude response does not change with varying input signal levels, that is, the filter gain is linear. The gain linearity measured at the 100kHz theoretical center frequency of the filter is shown in Figure 7. The gain is perfectly linear for input amplitudes up to 1.25VRMS (3.5Vp-p) so an 84dB dynamic range can be claimed. The input signal, however, can reach amplitudes up to 3VRMS (8.4Vp-p, 92dB SNR) with some reduction in gain linearity.

**LTC1735/LTC1736, continued from page 6**

**Conclusion**

The LTC1735 and LTC1736 are the latest members of Linear Technology’s family of constant frequency, N-channel high efficiency controllers. With new protection features, improved circuit operation and strong MOSFET drivers, the LTC1735 is an ideal upgrade to the LTC1435/LTC1435A for higher current applications. With the integrated VID control, the LTC1736 is ideal for CPU power applications.

The high performance of these controllers with wide input range, 1% reference and tight load regulation makes them ideal for next generation designs.

**References**

4. LTC1562 Final Data Sheet.

**LTC1562-2, continued from page 10**

level is 44µVRMS over a bandwidth of 800kHz or 98dB below the maximum unclipped output.

**Acknowledgments**

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**Other Applications**

The LT1505 can also be used in other system topologies, such as the telecom application shown in Figure 5. The circuit in Figure 5 uses the battery to supply peak power demands. By doing so, the required peak power from the wall adapter can be much lower than the peak power required by the load. The wall adapter has to supply the average power only.

**Conclusion**

The LT1505 is a complete, single-chip battery charger solution for today’s demanding charging requirements in high performance laptop applications. The device requires a small number of external components and provides all necessary functions for battery charging and power management. High efficiency and small size allow for easy integration with the laptop circuits. Also, by adding a simple external circuit, charging can be easily controlled by the host computer, allowing for more sophisticated charging schemes.

**Step-Down Conversion, continued from page 30**

lower cost LTC1430A replacing the LTC1649. The LTC1430A does not include the 3.3V to 5V charge pump and requires a 5V supply to drive the external MOSFET gates. The current drawn from the 5V supply depends on the gate charge of the external MOSFETs but is typically below 50mA, regardless of the load current on the 2.5V output. The drains of the Q1/Q2 pair draw the main load current from the 3.3V supply. The remaining circuit works in the same manner as in Figure 1. Efficiency and performance are virtually the same as the LTC1649 solution, but parts count and system cost are lower.

In a 3.3V to 2.5V application, the steady-state, no-load duty cycle is 76%. If the input supply drops to 3.135V (3.3V – 5%), the duty cycle requirement rises to 80% at no load, and even higher under heavy or transient load conditions. Both the LTC1649 and the LTC1430A guarantee a maximum duty cycle of greater than 90% to provide acceptable load regulation and transient response. The standard LTC1430 (not the LTC1430A) can max out as low as 83%—not high enough for 3.3V to 2.5V circuits. Applications with larger step-down ratios, such as 3.3V to 2.0V, can use the circuit in Figure 3 successfully with a standard LTC1430.