**F₀ and Q in Filters**

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**IN THIS MINI TUTORIAL**

The cutoff frequency (F₀) and quality factor (Q) of a filter are described in this mini tutorial, one in a series of mini tutorials documenting discrete circuits incorporating operational amplifiers (op amps).

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The F₀ of a filter is defined as the cutoff frequency of the filter. Generally, this is the frequency where the amplitude response is down 3 dB from the pass band. For a Chebyshev filter, it can sometimes be defined as the frequency at which the amplitude response falls out of the pass band. For example, a 0.1 dB Chebyshev filter can have its F₀ defined at the frequency at which the response is down > 0.1 dB.

The shape of the attenuation curve (as well as the phase and delay curves, which define the time domain response of the filter) will be the same if the ratio of the actual frequency to the cutoff frequency is examined, rather than just the actual frequency itself. Normalizing the filter to 1 rad/s, a simple system for designing and comparing filters can be developed. The filter is then scaled by the cutoff frequency to determine the component values for the actual filter.

Q is defined as the quality factor of the filter. It is also sometimes given as \( \alpha \) where:

\[
\alpha = \frac{1}{Q}
\]  

(1)

This is commonly known as the damping ratio. Note that \( \xi \) is sometimes used where:

\[
\xi = 2\alpha
\]  

(2)

If Q is > 0.707, there will be some peaking in the filter response. If the Q is < 0.707, roll off at F₀ will be greater; it will have a more gentle slope and the roll off will begin sooner. The amount of peaking for a 2-pole low-pass filter vs. Q is shown in Figure 1.

Rewriting the transfer function \( H(s) \) in terms of \( \omega_0 \) and Q:

\[
H(s) = \frac{H_0}{s^2 + \frac{\omega_0}{Q} s + \omega_0^2}
\]  

(3)

where \( H_0 \) is the pass-band gain and \( \omega_0 = 2\pi F_0 \).

Now this the low-pass prototype will be used to design the filters.

**HIGH-PASS FILTER**

Changing the numerator of the transfer equation, \( H(s) \), of the low-pass prototype to \( H_0 s^2 \) transforms the low-pass filter into a high-pass filter. The response of the high-pass filter is similar in shape to a lowpass, just inverted in frequency

The transfer function of a highpass filter is then

\[
H(s) = \frac{H_0 s^2}{s^2 + \frac{\omega_0}{Q} s + \omega_0^2}
\]  

(4)

The response of a 2-pole high-pass filter is illustrated in Figure 2.
BAND-PASS FILTER

Changing the numerator of the low-pass prototype to $H_0 \omega_0^2$ converts the filter to a band-pass function.

The transfer function of a band-pass filter is then

$$H(s) = \frac{H_0 \omega_0 s^2}{s^2 + \omega_0^2 + \frac{\omega_0}{Q}}$$  \hspace{1cm} (5)

where:
- $\omega$ is the frequency ($\omega_0 = 2 \pi \omega_0$) at which the gain of the filter peaks.
- $H_0$ is the circuit gain and is defined $H_0 = H/Q$.  \hspace{1cm} (6)

$Q$ has a particular meaning for the band-pass response. It is the selectivity of the filter. It is defined as:

$$Q = \frac{F_0}{F_H - F_L}$$ \hspace{1cm} (7)

where $F_L$ and $F_H$ are the frequencies where the response is –3 dB from the maximum.

The bandwidth (BW) of the filter is described as

$$BW = F_H - F_L$$ \hspace{1cm} (8)

Note that it can be shown that the resonant frequency ($F_0$) is the geometric mean of $F_L$ and $F_H$, which means that $F_0$ will appear half way between $F_L$ and $F_H$ on a logarithmic scale.

$$F_0 = \sqrt{F_H F_L}$$

Also, note that the skirts of the band-pass response will always be symmetrical around $F_0$ on a logarithmic scale.

The response of a band-pass filter to various values of $Q$ are shown in Figure 3.

A word of caution is appropriate here. Band-pass filters can be defined two different ways. The narrow-band case is the classic definition that as shown in Figure 3.

In some cases, however, if the high and low cutoff frequencies are widely separated, the band-pass filter is constructed out of separate high-pass and low-pass sections. Widely separated in this context means separated by at least two octaves ($\times 4$ in frequency). This is the wide-band case.

BAND-REJECT (NOTCH) FILTER

By changing the numerator to $s^2 + \omega_0^2$, one can convert the filter to a band-reject, or notch, filter. As in the band-pass case, if the corner frequencies of the band-reject filter are separated by more than an octave (the wide-band case), it can be built out of separate low-pass and high-pass sections. Thus, the following convention will be adopted: A narrow-band band-reject filter will be referred to as a notch filter and the wide-band band-reject filter will be referred to as band-reject filter.

A notch (or band-reject) transfer function is

$$H(s) = \frac{H_0 (s^2 + \omega_0^2)}{s^2 + \frac{\omega_0}{Q}}$$ \hspace{1cm} (9)

There are three cases of the notch filter characteristics as illustrated in Figure 4. The relationship of the pole frequency, $\omega_0$, and the zero frequency, $\omega_z$, determines if the filter is a standard notch, a low-pass notch, or a high-pass notch.
If the zero frequency is equal to the pole frequency, a standard notch exists. In this instance, the zero lies on the jω plane where the curve that defines the pole frequency intersects the axis.

A low-pass notch occurs when the zero frequency is greater than the pole frequency. In this case, ωz lies outside the curve of the pole frequencies. What this means in a practical sense is that the filter's response below ωz will be greater than the response above ωz. This results in an elliptical low-pass filter.

A high-pass notch filter occurs when the zero frequency is less than the pole frequency. In this case, ωz lies inside the curve of the pole frequencies. What this means in a practical sense is that the filter's response below ωz will be less than the response above ωz. This results in an elliptical high-pass filter.

The variation of the notch width with Q is shown in Figure 5.

REFERENCES

REVISION HISTORY
1/12—Revision 0: Initial Version