

ADXRS150

ABSOLUTE MAXIMUM RATINGS

Table 2.

| Parameter | Rating |
|--|------------------|
| Acceleration (Any Axis, Unpowered, 0.5 ms) | 2000 g |
| Acceleration (Any Axis, Powered, 0.5 ms) | 2000 g |
| +V _s | -0.3 V to +6.0 V |
| Output Short-Circuit Duration (Any Pin to Common) | Indefinite |
| Operating Temperature Range | -55°C to +125°C |
| Storage Temperature | -65°C to +150°C |

Stresses above those listed under Absolute Maximum Ratings may cause permanent damage to the device. This is a stress rating only and functional operation of the device at these or any other conditions above those indicated in the operational section of this specification is not implied. Exposure to absolute maximum rating conditions for extended periods may affect device reliability.

Applications requiring more than 200 cycles to MIL-STD-883 Method 1010 Condition B (-55°C to +125°C) require underfill or other means to achieve this requirement.

Drops onto hard surfaces can cause shocks of greater than 2000 g and exceed the absolute maximum rating of the device. Care should be exercised in handling to avoid damage.

ESD CAUTION

ESD (electrostatic discharge) sensitive device. Electrostatic charges as high as 4000 V readily accumulate on the human body and test equipment and can discharge without detection. Although this product features proprietary ESD protection circuitry, permanent damage may occur on devices subjected to high energy electrostatic discharge. Therefore, proper ESD precautions are recommended to avoid performance degradation or loss of functionality.

RATE SENSITIVE AXIS

This is a Z-axis rate-sensing device that is also called a yaw rate sensing device. It produces a positive going output voltage for clockwise rotation about the axis normal to the package top, i.e., clockwise when looking down at the package lid.

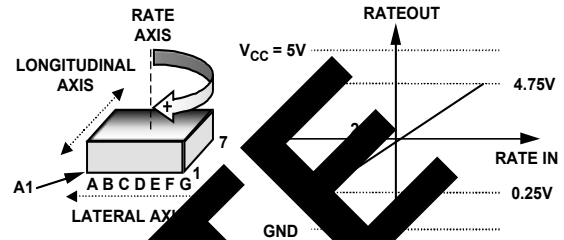


Figure 2. RATEOUT Signal Increases with Clockwise Rotation

OBSOLETE



PIN CONFIGURATION AND FUNCTION DESCRIPTIONS

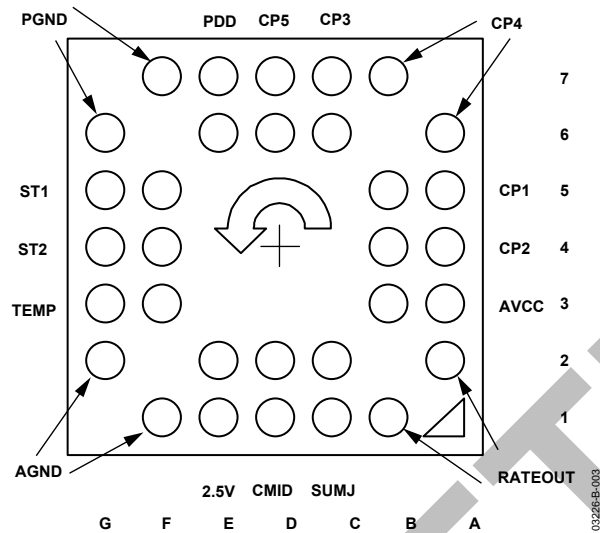


Figure 3. BGA-32 (Bottom View)

Table 3. Pin Function Descriptions

| Pin No. | Mnemonic | Description |
|---------|----------|-----------------------------|
| 6D, 7D | CP5 | HV Filter Capacitor—47 nF |
| 6A, 7B | CP4 | Charge Pump Capacitor—22 nF |
| 6C, 7C | CP3 | Charge Pump Capacitor—22 nF |
| 5A, 5B | CP1 | Charge Pump Capacitor—22 nF |
| 4A, 4B | CP2 | Charge Pump Capacitor—22 nF |
| 3A, 3B | AVCC | + Analog Supply |
| 1B, 2A | RATEOUT | Rate Signal Output |
| 1C, 2C | SUMJ | Output Amp Summing Junction |
| 1D, 2D | CMID | HF Filter Capacitor—100 nF |
| 1E, 2E | 2.5V | 2.5 V Precision Reference |
| 1F, 2G | AGND | Analog Supply Return |
| 3F, 3G | TEMP | Temperature Voltage Output |
| 4F, 4G | ST2 | Self-Test for Sensor 2 |
| 5F, 5G | ST1 | Self-Test for Sensor 1 |
| 6G, 7F | PGND | Charge Pump Supply Return |
| 6E, 7E | PDD | + Charge Pump Supply |

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TYPICAL PERFORMANCE CHARACTERISTICS

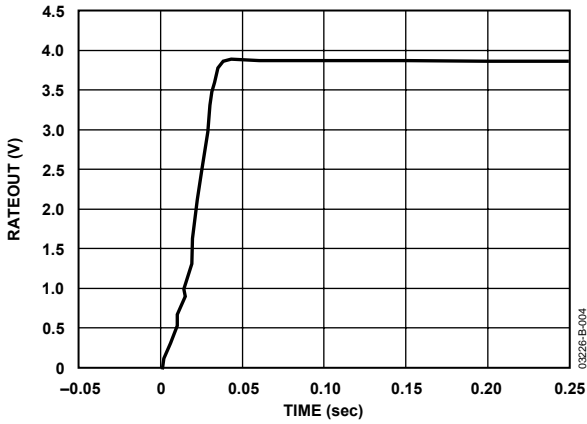


Figure 4. Rate Sensing Start-Up Time

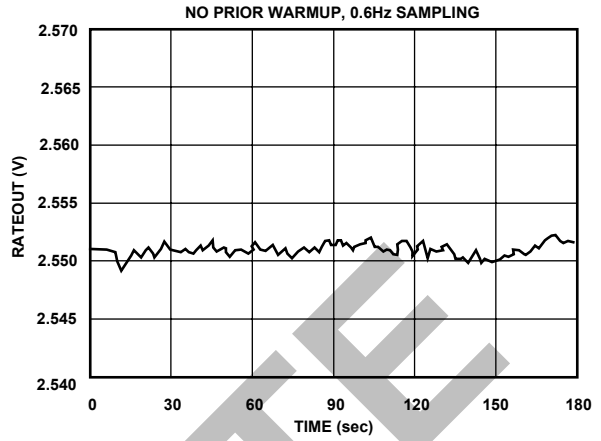


Figure 7. Null Settling Time

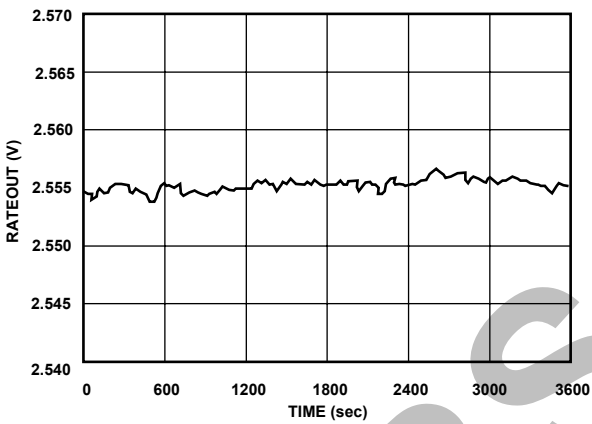


Figure 5. Null Stability for 1 Hour

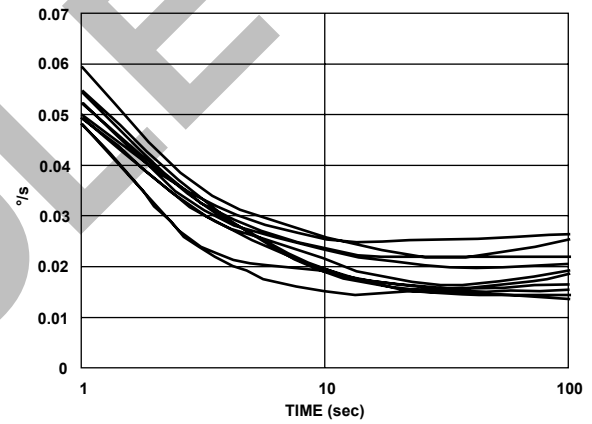


Figure 8. Root Allan Variance vs. Averaging Time

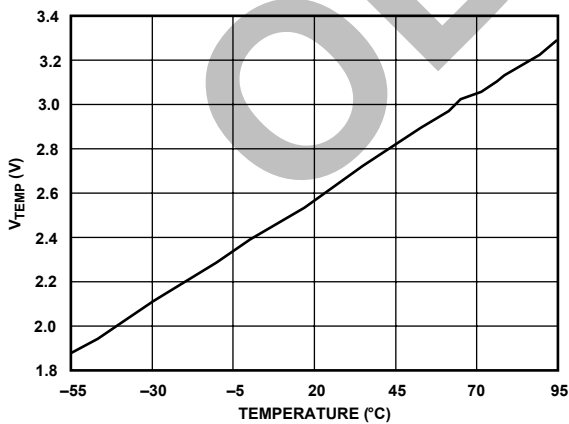


Figure 6. Temperature Sensor Output

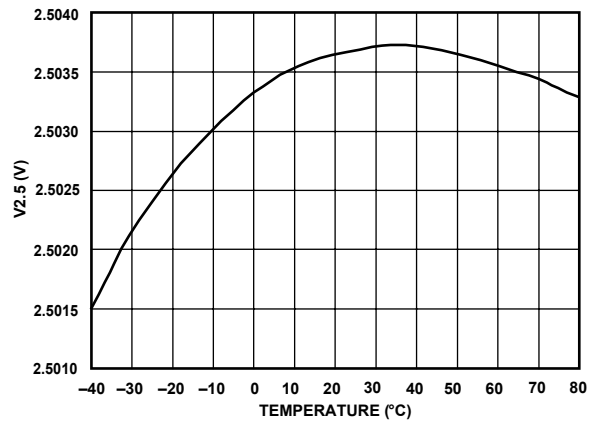


Figure 9. 2.5 V Voltage Reference vs. Temperature

@ BW = 40 Hz, Typical Vibration Characteristics, 10 g Flat Band, 20 Hz to 2 kHz

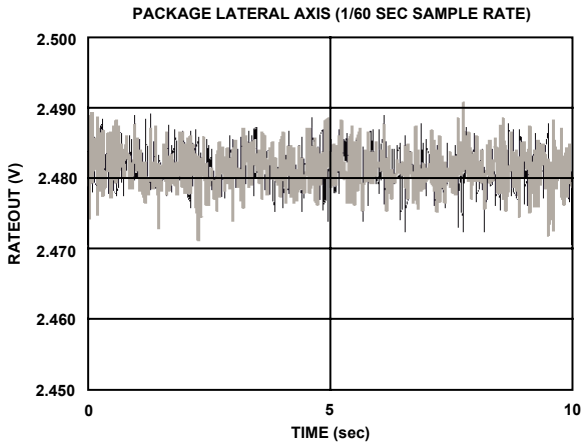


Figure 10. 10 g Random Vibration in Package-Lateral Axis Orientation

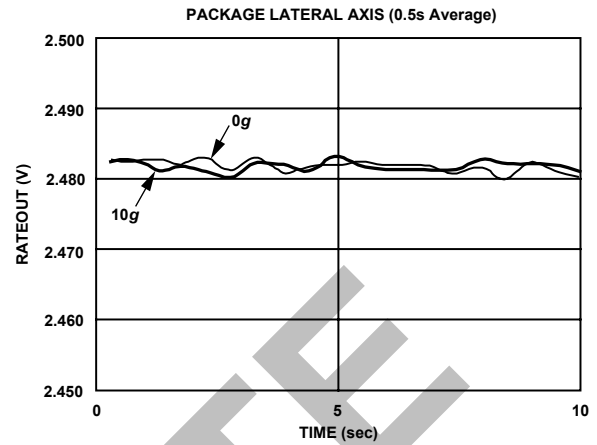


Figure 13. 10 g Random Vibration in Package-Lateral Axis Orientation

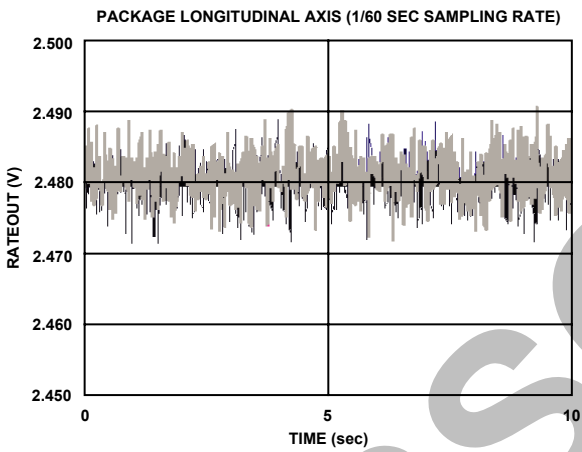


Figure 11. 10 g Random Vibration in Package-Longitudinal Axis Orientation

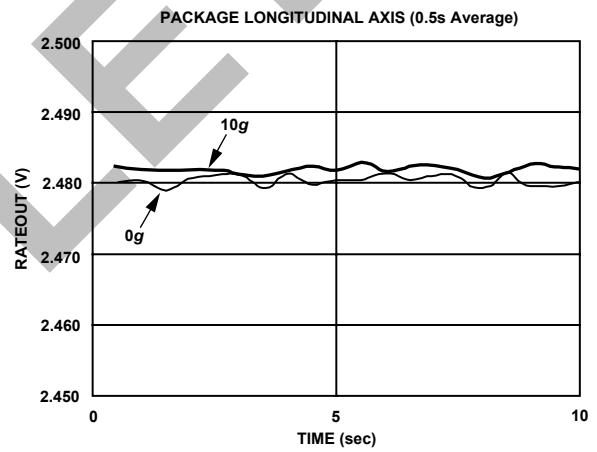


Figure 14. 10 g Random Vibration in Package-Longitudinal Axis Orientation

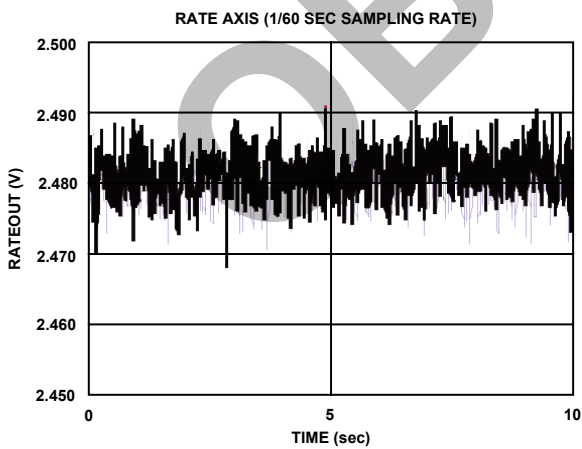


Figure 12. 10 g Random Vibration in Rate Axis Orientation

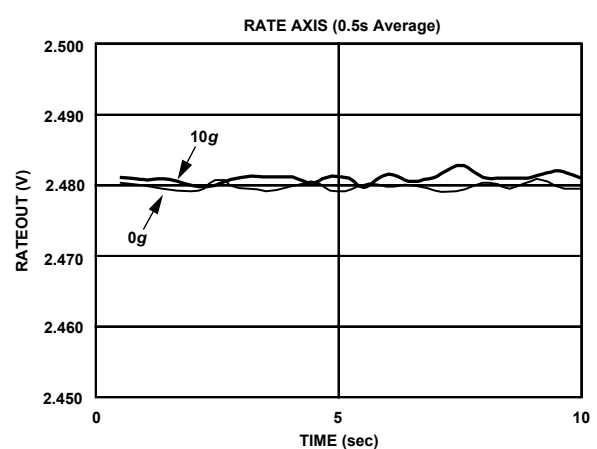


Figure 15. 10 g Random Vibration in Rate Axis Orientation

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Behavior under Various Shock Test Conditions

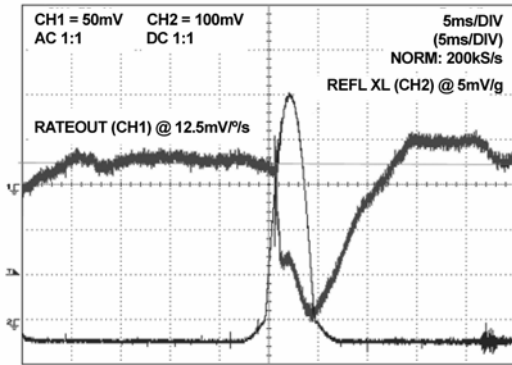


Figure 16. Shock Test 100 g, 5 ms in Lateral Axis (40 Hz)

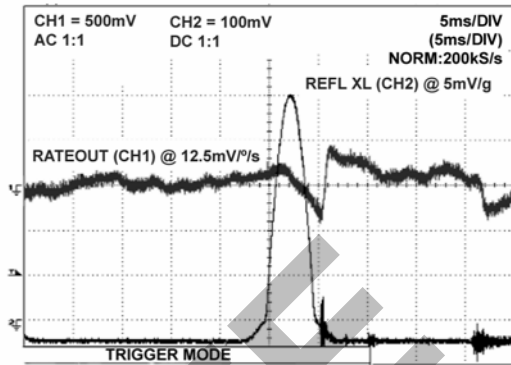


Figure 19. Shock Test 100 g, 5 ms in Longitudinal Axis (40 Hz)

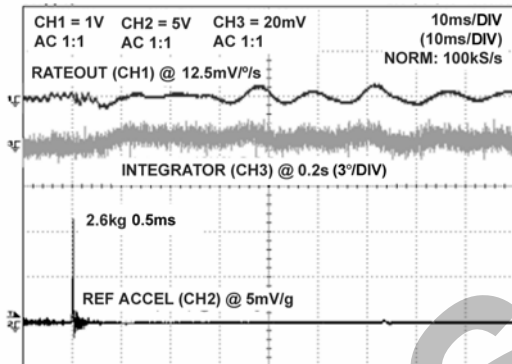


Figure 17. Hi-g Shock Test in Lateral Axis (40 Hz)

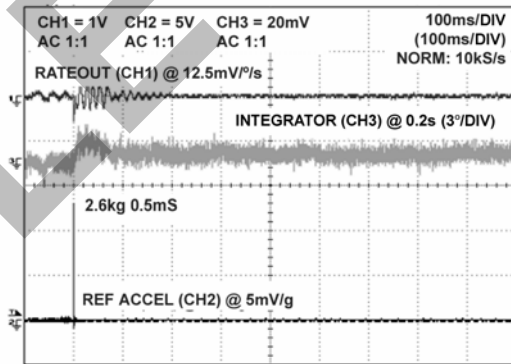


Figure 20. Hi-g Shock Test, Lateral Axis, 10x Time Base (40 Hz)

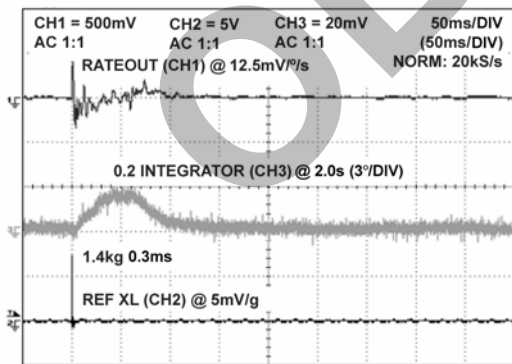


Figure 18. Hi-g Shock in Rate Axis (40 Hz)

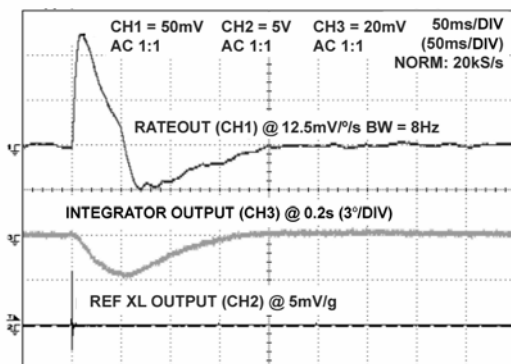


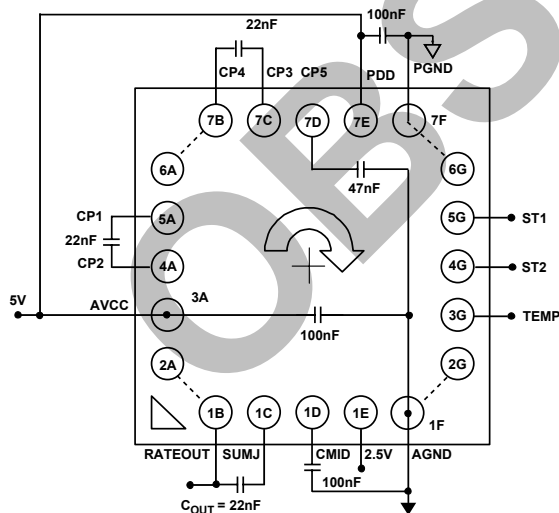
Figure 21. Hi-g Shock, Rate Axis, BW Reduced to 8Hz

THEORY OF OPERATION

The ADXRS150 operates on the principle of a resonator gyro. Two polysilicon sensing structures each contain a dither frame, which is electrostatically driven to resonance. This produces the necessary velocity element to produce a Coriolis force during angular rate. At two of the outer extremes of each frame, orthogonal to the dither motion, movable fingers are placed between fixed pickoff fingers to form a capacitive pickoff structure that senses Coriolis motion. The resulting signal is fed to a series of gain and demodulation stages that produce the electrical rate signal output. The dual-sensor design rejects external *g*-forces and vibration. Fabricating the sensor with the signal conditioning electronics preserves signal integrity in noisy environments.

The electrostatic resonator requires 14 V to 16 V for operation. Since only 5 V is typically available in most applications, a charge pump is included on-chip. If an external 14 V to 16 V supply is available, the two capacitors on CP1–CP4 can be omitted, and this supply can be connected to CP5 (Pin 7D) with a 100 nF decoupling capacitor in place of the 47 nF.

After the demodulation stage, there is a single-pole low-pass filter consisting of an internal 9 kΩ resistor (R_{SEN1}) and an external user-supplied capacitor (CMID). A CMID capacitor of 100 nF sets a 400 Hz \pm 35% low-pass pole and is used to limit high frequency artifacts before final amplification. The bandwidth limit capacitor, C_{OUT} , sets the pass bandwidth (see Figure 23 and the Setting Bandwidth section).



NOTE THAT INNER ROWS/COLUMNS OF PINS HAVE BEEN OMITTED FOR CLARITY BUT SHOULD BE CONNECTED IN THE APPLICATION.

Figure 22. Example Application Circuit (Top View)

SUPPLY AND COMMON CONSIDERATIONS

Only power supplies used for supplying analog circuits are recommended for powering the ADXRS150. High frequency noise and transients associated with digital circuit supplies may have adverse effects on device operation.

Figure 22 shows the recommended connections for the ADXRS150 where both AVCC and PDD have a separate decoupling capacitor. These should be placed as close to their respective pins as possible before routing to the system analog supply. This will minimize the noise injected by the charge pump that uses the PDD supply.

It is also recommended to place the charge pump capacitors connected to the CP1–CP4 pins as close to the part as possible. These capacitors are used to produce the on-chip high voltage supply switched at the dither frequency at approximately 14 kHz. Care should be taken to ensure that there is no more than 50 pF of stray capacitance between CP1–CP4 and ground. Surface-mount chip capacitors are suitable as long as they are rated for over 15 V.

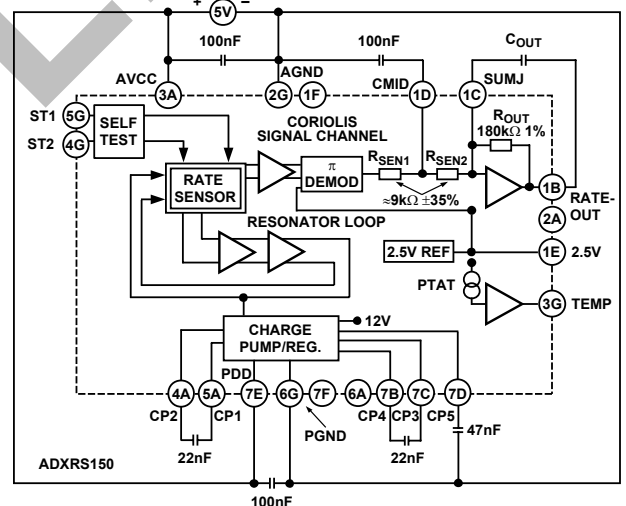


Figure 23. Block Diagram with External Components

SETTING BANDWIDTH

External capacitors CMID and C_{OUT} are used in combination with on-chip resistors to create two low-pass filters to limit the bandwidth of the ADXRS150's rate response. The -3 dB frequency set by R_{OUT} and C_{OUT} is

$$f_{OUT} = 1/(2 \times \pi \times R_{OUT} \times C_{OUT})$$

and can be well controlled since R_{OUT} has been trimmed during manufacturing to be 180 kΩ \pm 1%. Any external resistor applied between the RATEOUT (1B,2A) and SUMJ (1C,2C) pins results in

$$R_{OUT} = (180 \text{ k}\Omega \times R_{EXT}) / (180 \text{ k}\Omega + R_{EXT})$$

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The -3 dB frequency is set by R_{SEN} (the parallel combination of R_{SEN1} and R_{SEN2}) at about 4.5 kΩ nominal; CMID is less well controlled since R_{SEN1} and R_{SEN2} have been used to trim the rate sensitivity during manufacturing and have a ±35% tolerance. Its primary purpose is to limit the high frequency demodulation artifacts from saturating the final amplifier stage. Thus, this pole of nominally 400 Hz @ 0.1 μF need not be precise. Lower frequency is preferable, but its variability usually requires it to be about 10 times greater (in order to preserve phase integrity) than the well-controlled output pole. In general, both -3 dB filter frequencies should be set as low as possible to reduce the amplitude of these high frequency artifacts as well as to reduce the overall system noise.

INCREASING MEASUREMENT RANGE

The full-scale measurement range of the ADXRS150 can be increased by placing an external resistor between the RATEOUT (1B, 2A) and SUMJ (1C, 2C) pins, which would parallel the internal R_{OUT} resistor that is factory-trimmed to 180 kΩ. For example, a 330 kΩ external resistor will give approximately 8.1 mV/°/sec sensitivity and a commensurate ~50% increase in the full-scale range. This is effective for up to a 4× increase in the full-scale range (minimum value of the parallel resistor allowed is 45 kΩ). Beyond this amount of external sensitivity reduction, the internal circuitry headroom requirements prevent further increase in the linear full-scale output range. The drawbacks of modifying the full-scale range are the additional output null drift (as much as 2°/sec over temperature) and the readjustment of the initial null bias (see the Null Adjustment section).

TEMPERATURE OUTPUT AND CALIBRATION

It is common practice to temperature-calibrate gyros to improve their overall accuracy. The ADXRS150 has a temperature-proportional voltage output that provides input to such a calibration method. The voltage at TEMP (3F, 3G) is nominally 2.5 V at 27°C and has a PTAT (proportional to absolute temperature) characteristic of 8.4 mV/°C. Note that the TEMP output circuitry is limited to 50 μA source current.

Using a 3-point calibration technique, it is possible to calibrate the ADXRS150's null and sensitivity drift to an overall accuracy of nearly 300°/hour. An overall accuracy of 70°/hour or better is possible using more points. Limiting the bandwidth of the device reduces the flat-band noise during the calibration process, improving the measurement accuracy at each calibration point.

USING THE ADXRS150 WITH A SUPPLY-RATIOMETRIC ADC

The ADXRS150's RATEOUT signal is nonratiometric, i.e., neither the null voltage nor the rate sensitivity is proportional to the supply. Instead they are nominally constant for dc supply changes within the 4.75 V to 5.25 V operating range. If the ADXRS150 is used with a supply-ratiometric ADC, the

ADXRS150's 2.5 V output can be converted and used to make corrections in software for the supply variations.

NULL ADJUSTMENT

Null adjustment is possible by injecting a suitable current to SUMJ (1C, 2C). Adding a suitable resistor to either ground or the positive supply is a simple way of achieving this. The nominal 2.5 V null is for a symmetrical swing range at RATEOUT (1B, 2A). However, a nonsymmetrical output swing may be suitable in some applications. Note that if a resistor is connected to the positive supply, supply disturbances may reflect some null instability. Digital supply noise should be avoided particularly in this case (see the Supply and Common Considerations section).

The resistor value to use is approximately

$$R_{NULL} = (2.5 \times 180,000) / (V_{NULL0} - V_{NULLI})$$

V_{NULL0} is the unadjusted zero-rate output, and V_{NULLI} is the target null value. If the initial value is below the desired value, the resistor should terminate on common or ground. If it is above the desired value, the resistor should terminate on the 5 V supply. Values typically are in the 1 MΩ to 5 MΩ range.

If an external resistor is used across RATEOUT and SUMJ, the parallel equivalent value is substituted into the above equation. Note that the resistor value is an estimate since it assumes $V_{CC} = 5.0$ V and $V_{SUMJ} = 2.5$ V.

SELF-TEST FUNCTION

The ADXRS150 includes a self-test feature that actuates each of the sensing structures and associated electronics in the same manner as if subjected to angular rate. It is activated by standard logic high levels applied to inputs ST1 (5F, 5G), ST2 (4F, 4G), or both. ST1 causes the voltage at RATEOUT to change about -0.66 V, and ST2 causes an opposite change of +0.66 V. The self-test response follows the viscosity temperature dependence of the package atmosphere, approximately 0.25%/°C.

Activating both ST1 and ST2 simultaneously is not damaging. Since ST1 and ST2 are not necessarily closely matched, actuating both simultaneously may result in an apparent null bias shift.

CONTINUOUS SELF-TEST

The one-chip integration of the ADXRS150 gives it higher reliability than is obtainable with any other high volume manufacturing method. Also, it is manufactured under a mature Bimos process that has field-proven reliability. As an additional failure detection measure, power-on self-test can be performed. However, some applications may warrant continuous self-test while sensing rate. Application notes outlining continuous self-test techniques are also available on the Analog Devices website.

ACCELERATION SENSITIVITY

The sign convention used is that lateral acceleration is positive in the direction from Pin Column A to Pin Column G of the package. That is, a device has positive sensitivity if its voltage output increases when the row of Pins 2A–6A are tipped under the row of Pins 2G–6G in the earth’s gravity.

There are two effects of concern, shifts in the static null and induced null noise. Scale factor is not significantly affected until the acceleration reaches several hundred m/s^2 .

Vibration rectification for frequencies up to 20 kHz is on the order of $0.00002(^{\circ}/s)/(m/s^2)^2$, is not significantly dependent on frequency, and has been verified up to 400 m/s^2 rms.

Linear vibration spectral density near the 14 kHz sensor resonance translates into output noise. In order to have a significant effect, the vibration must be within the angular rate bandwidth (typically ± 40 Hz of the resonance), so it takes considerable high frequency vibration to have any effect.

Away from the 14 kHz resonance the effect is not discernible, except for vibration frequencies within the angular rate pass band. This can be seen in Figure 10 to Figure 15 for the various sensor axes. The in-band effect can be seen in Figure 25. This is the result of the static g -sensitivity. The specimen used for Figure 25 had a g -sensitivity of $0.15^{\circ}/s/g$ and its total in-band noise degraded from 3 mV rms to 5 mV rms for the specified vibration. The effect of broadband vibration up to 20 kHz is shown in Figure 24 and Figure 26.

The output noise of the part falls away in accordance with the output low-pass filter and does not contain any spikes greater than 1% of the low frequency noise. A typical noise spectrum is shown in Figure 27.

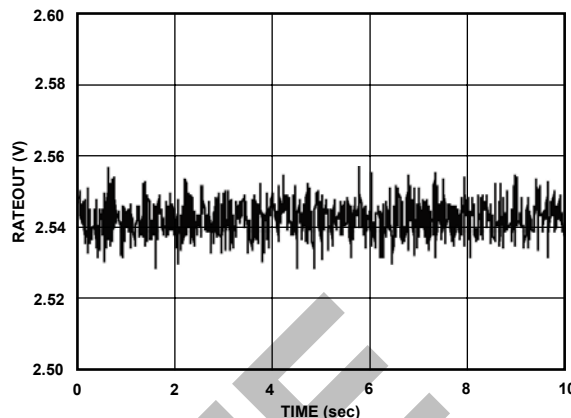


Figure 25. Random Vibration (Lateral) 2 Hz to 40 Hz, 3.2 g rms

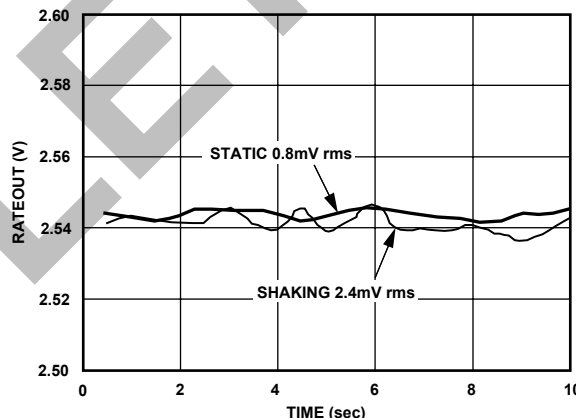


Figure 26. Random Vibration (Lateral) 10 kHz to 20 kHz at $0.01 g/\sqrt{Hz}$ with 60 Hz Sampling and 0.5 sec Averaging

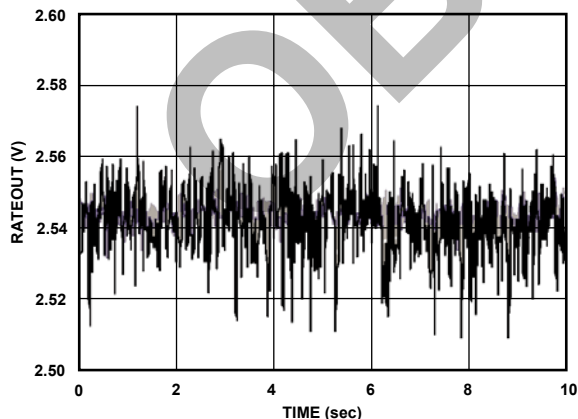


Figure 24. Random Vibration (Lateral) 10 kHz to 20 kHz at $0.01 g/\sqrt{Hz}$ with 60 Hz Sampling and 0.5 sec Averaging

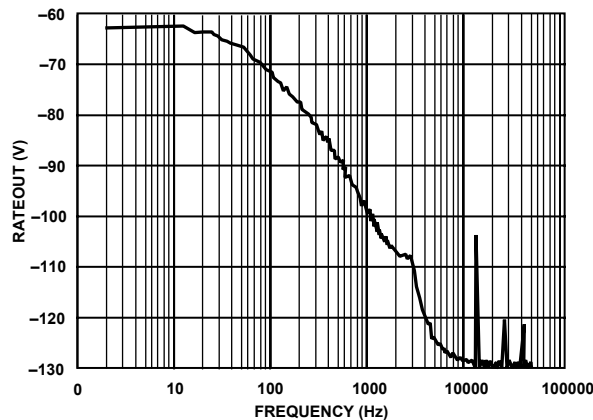


Figure 27. Noise Spectral Density at RATEOUT –BW = 4 Hz

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OUTLINE DIMENSIONS

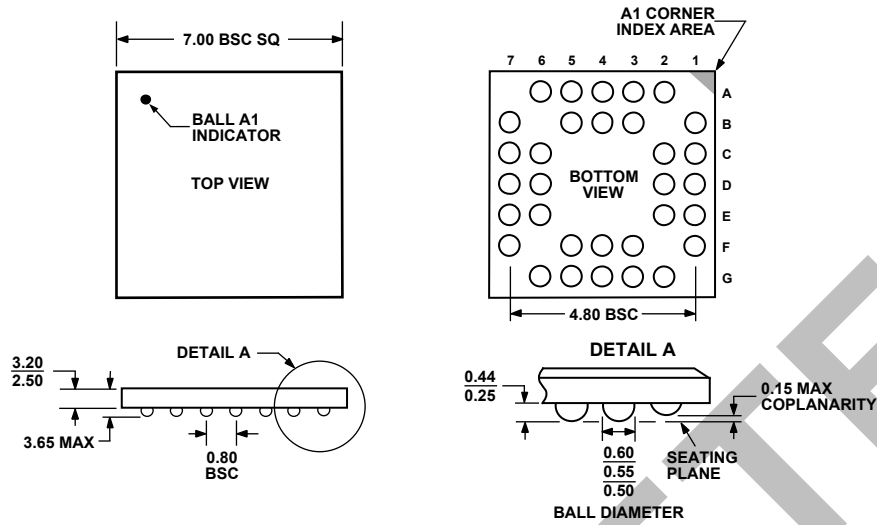


Figure 28. 32-Lead Chip Scale Ball Grid Array [CSPBGA]
(BC-32)
Dimensions shown in millimeters

ORDERING GUIDE

| Model | Temperature Range | Package Description | Package Outline |
|------------------|-------------------|---------------------|-----------------|
| ADXRS150ABG | -40°C to +85°C | 32-Lead BGA | BC-32 |
| ADXRS150ABG-Reel | -40°C to +85°C | 32-Lead BGA | BC-32 |
| ADXRS150EB | | Evaluation Board | |