2.7V to 40V Monolithic Buck-Boost DC/DC Expands Input Capabilities, Regulates Seamlessly through Automotive Cold-Crank and Load-Dump Transients

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Handheld devices, industrial instruments and automotive electronics all demand power supply solutions that can support an expansive range of input voltages resulting from automotive input voltage transients, resistive line drops and a wide variety of power sources. As a further design challenge, applications often require a variety of regulated voltage rails, including some that fall within the input voltage range. The LTC3115-1 buck-boost DC/DC converter, with its wide 2.7V to 40V input and output voltage capability, high efficiency, small footprint and seamless transition between step-up and step-down modes of operation, easily meets the requirements of such applications.

For automotive electronics, the LTC3115-1 provides uninterrupted operation through load dump transients and even the harshest cold-crank conditions. Its programmable switching frequency optimizes efficiency and supports operation at 2MHz to ensure that switching noise and harmonics are located above the AM broadcast band. The LTC3115-1 employs a proprietary low noise PWM control algorithm that minimizes electromagnetic emissions over all operating conditions even during transitions between the step-up and step-down modes of operation and over the full range of load current. An internal phase-locked loop allows switching edges to be synchronized with an external clock for further control of EMI in noise-sensitive applications.

An accurate RUN pin provides a programmable input undervoltage lockout threshold with independent control of hysteresis. By consuming only 30µA of quiescent current in Burst Mode® operation and 3µA in shutdown, the LTC3115-1 reduces standby current drain on automobile batteries to negligible levels.

Additionally, in an effort to reduce design overhead, many product families utilize a single power supply design that is shared across multiple versions of a product. This requires that the common power supply support the widest range of possible input voltages that will be seen by any device within the family. With its wide 2.7V to 40V input and output voltage ranges, internal power switches and high efficiency the LTC3115-1 has the features and flexibility required for these demanding applications.

**5V, 2MHz MINIATURE SIZE AUTOMOTIVE SUPPLY**

The proliferation of electronic subsystems in automobiles has created demand for small size, high reliability power supplies that can operate under the stringent conditions presented by the automotive environment. The LTC3115-1 is well suited for such applications given its ability to provide a stable well-regulated voltage over automotive operating conditions even when the battery voltage falls below the required output rail due to battery state of charge, line transients induced by switched high current loads and cold-cranking events.
Of commonly utilized power sources, the automotive supply rail presents one of the most challenging inputs to a power supply. Its nominal voltage varies from 10.6V to 15V depending on the state of charge of the battery, the ambient temperature and whether the alternator is charging or idle. Cold-crank conditions can push the rail below 4V and line transients can produce 40V spikes.

Figure 2 shows a 5V automotive supply ideal for use in engine control units and other critical functions including safety, fuel system and drive train subsystems where processors must remain powered without glitch during even the most severe input voltage transients. This application uses a 2MHz switching frequency to minimize its footprint and eliminate interference with the AM broadcast band.

The \( V_{CC} \) rail provides power to the internal circuitry of the LTC3115-1 including the power device gate drivers and is ordinarily powered from the input rail via an internal linear regulator. In this application, diode D1 bypasses the internal linear regulator and delivers power to the \( V_{CC} \) rail directly from the regulated output to improve efficiency and output current capability. This is particularly advantageous in applications with higher switching frequencies, given that the increased gate drive current is provided more efficiently from the converter’s output rail than through the internal linear regulator. Figure 3 shows the efficiency of this application circuit with a 500mA load for input voltages from 3.3V to 40V.

Riding Through Automotive Load-Dump and Inductive Line Transients

Of commonly utilized power sources, the automotive supply rail presents one of the most challenging inputs to a power supply. Its nominal voltage varies from 10.6V to 15V depending on the state of charge of the battery, the ambient temperature and whether the alternator is charging or idle. In addition to the variability in its nominal voltage, the automotive power rail is also subject to a wide range of dynamic disturbances induced by changes in engine RPM, transitioning loads such as power windows, wipers and air conditioning, and inductive transients in the wiring harness.

However, the most extreme conditions occur during a load-dump transient which can produce voltages in excess of 120V for a duration of hundreds of milliseconds.

A load-dump transient occurs when the alternator is charging the vehicle’s battery and an electrical open-circuit causes a momentary disconnection of the battery from the alternator. Until the voltage regulator can respond, the full alternator charging current is applied directly to the automotive power bus, raising its voltage to potentially dangerous levels. Such a transient could be caused through a physical disconnection of the battery by a mechanic working on the vehicle, but could also result from a faulty connection in the battery cable or corrosion at the battery terminals.

Automotive electronics must also be designed to survive a double-battery jump start, where they are subjected to 24V for extended durations as the vehicle is jump started using a series-connected second battery or from a commercial vehicle with a dual battery electrical system. An additional overvoltage condition on the automotive bus is caused by alternator voltage regulator failure and is often
Typically, automotive electronics located downstream from passive protection networks must survive up to a 40V transient without damage. Critical systems must survive high level transients, and function seamlessly through such transients without interruption. The LTC3115-1 can maintain uninterrupted regulation of a 5V supply rail through a 13.8V-to-40V momentary line transient with 1ms rise and fall times.

included in the battery of tests conducted by automotive electronics OEMs. Such a malfunction can result in full application of the alternator charge current to the battery and an overvoltage of approximately 18V for extended durations.

The automotive power rail is also polluted with short duration overvoltage transients due to rapid load changes produced by switching high power loads such as power doors, fans and cooling fan motors interacting with the significant inductance in the vehicle’s wiring harness.

In most vehicles a passive protection network consisting of a lowpass LC filter and transient voltage suppression (TVS) array is used as a first line of defense to clamp the peak excursions of the power bus. Typically, automotive electronics located downstream from the protection network must survive up to a 40V transient without damage. Critical systems must not only survive, but must also function seamlessly through such transients without interruption. Figure 4 illustrates the ability of the LTC3115-1 to maintain uninterrupted regulation of a 5V supply rail through a 13.8V-to-40V momentary line transient with 1ms rise and fall times.

SEAMLESS OPERATION THROUGH AUTOMOTIVE COLD-CRANK TRANSIENTS

High voltage transients are a problem on the automotive power bus, but perhaps the more challenging problem is undervoltage transients. The most severe of these is known as cold crank, which occurs when the engine is initially started.

A typical cold-crank voltage waveform is shown in Figure 5. The initial low voltage plateau is the most extreme and is caused when the starter motor begins turning over the engine from a dead stop. During this phase, the vehicle’s bus voltage can fall below 4V. Colder temperatures exacerbate the situation since the higher viscosity of the engine oil results in a higher required torque from the starter motor. The first plateau is followed by a second somewhat higher voltage plateau, typically near half the nominal battery voltage, as the starter maintains the engine rotation. Once the engine starts, the battery recovers to its nominal voltage.

Safety devices and engine critical components such as the engine control unit and fuel injection system are required to remain operational throughout a cold-crank transient. As shown in Figure 5, the LTC3115-1’s buck-boost architecture enables it to maintain output regulation through even the most severe cold-crank transients by automatically and seamlessly switching to boost mode operation during the undervoltage event.

Cold-crank capability for automotive electronics has expanded in importance as cars now include automated fuel-saving, on-demand engine start/stop, whereby the vehicle’s engine is turned off during momentary vehicle stops at stoplights or in traffic. Vehicles equipped with on-demand starting are subjected to frequent cranking undervoltage events. As a result, auxiliary electrical components that previously had no need to function through the occasional cold-crank event in a traditional vehicle must now operate through such transients to eliminate any disturbance to infotainment, navigation, dashboard electronics and lighting systems.
The LTC3115-1’s buck-boost architecture enables it to maintain output regulation through even the most severe cold-crank transients by automatically and seamlessly switching to boost mode operation during the undervoltage event.

LOW EMI AND NO EMISSIONS IN THE AM BAND

The LTC3115-1 features a low noise forced PWM mode where both switch pins operate at constant frequency for all loads, producing a low noise spectrum, independent of operating conditions. The predictable spectrum and minimal subharmonic emissions help reduce interference and aid in compliance with strict automotive EMI standards.

The LTC3115-1 supports switching frequencies up to 2MHz so that the fundamental switching frequency component, and all of its harmonics, can be located above the AM frequency band to minimize interference with radio reception. Figure 6 shows the spectral emission of the LTC3115-1 over the AM band for the automotive application circuit of Figure 2 operating at no load and with a 500mA load. In both cases the entire range of frequencies within the AM broadcast band is free from any significant spectral emission.

HANDLING MULTIPLE POWER SOURCES – UNREGULATED WALL ADAPTER, AUTOMOTIVE INPUT, USB, USB-PD AND FIREWIRE

To increase flexibility and enhance the user’s experience, many portable electronic devices are being designed to work from various power sources. These power sources can vary widely in voltage, especially when accounting for connector and cable drops. Under USB 3.0, the nominal supplied voltage is 5V ±5%, but a fully compliant powered device must be able to operate down to 4V when accounting for allowable cable and connector voltage drops. In addition, a downstream USB power rail is permitted to drop as low as 3.67V under transient conditions such as when additional devices are plugged into the host or powered hub.

The newly approved USB PD (power delivery) specification allows for higher power delivery over USB with support for supply voltages up to 20V. Firewire ports deliver an unregulated power rail with a voltage that varies over a wide range, typically 9V to 26V depending on the class of the power provider.
The ubiquitous wall adapter remains perhaps the most common source of power for portable devices. A typical wall adapter is simply a transformer followed by a bridge rectifier, offering no active regulation. That task is left to the end device to avoid the effects of cable drop. Unregulated wall adapters are designed to provide rated current at the specified typical output voltage. Being unregulated, the output voltage is a load line function, increasing substantially at lighter loads and decreasing under heavy load. In addition, the AC line voltage is permitted to vary between 105V and 125V, adding an additional 10% variability in the unregulated wall adapter’s output. It is not uncommon for a 12V unregulated wall adapter to produce an output voltage of 17V or greater at light load.

The LTC3115-1 operates directly from all of these portable power sources as well as from a variety of battery chemistries including lithium (single cell or series connected), sealed lead acid, three or more series alkaline cells and even a bank of supercapacitors for backup applications. Multiple power sources can be combined through a Schottky diode-OR circuit. For higher efficiency, the LTC3115-1 can be combined with an ideal diode PowerPath controller to provide automatic switchover between multiple power sources using the low voltage drop of a power p-channel MOSFET to replace the Schottky diode. Figure 7 shows how the LTC3115-1 can be combined with the LTC4412HV to obtain a dual input—single lithium and unregulated wall adapter—5V supply. In this case, a series PMOS is used on the lower voltage lithium input while an inexpensive Schottky diode is used on the higher voltage input where its voltage drop is insignificant. The overall efficiency of this supply including the converter and PowerPath is given in Figure 8 for each power input.

24V INDUSTRIAL RAIL RESTORER AND BACKUP

Industrial control and monitoring systems commonly utilize a 24V bus to power DIN mounted instrumentation such as programmable logic controllers, actuators and sensors. Being subject to high power switching loads and possible fault conditions, this bus can become corrupted with transients and momentary undervoltage transients. In severe cases there may even be momentary interruptions in bus power. Critical rail-powered systems are required to remain powered throughout such events to ensure control and monitoring of critical functions.

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package, which is internally connected to the negative supply rail, \( V_- \), and must be connected to the negative power plane. Connect as much PCB metal as practical to the exposed pad—the thermal resistance of the package is proportional to the amount of metal soldered to the exposed pad. In a best case scenario the thermal resistance, \( \theta_{JA} \), of the SO package is 33°C/w. For 1W of power, the junction temperature of the die increases 33°C above ambient temperature.

An important feature designed to protect the LTC6090 from exceeding 150°C junction temperature shuts down the output stage when the junction temperature gets too high. This is accomplished by connecting the overtemperature pin to the output disable pin. The overtemperature pin, or \( T\text{TEMP} \) pin, is an open drain pin that pulls low when the junction temperature of the die reaches 145°C. The 5°C built-in hysteresis releases the \( T\text{TEMP} \) pin when the junction temperature reaches 140°C. The output disable pin, or \( O\text{D} \) pin, is an active low pin that turns off the output stage and lowers the quiescent current of the device to 670μA when pulled low with respect to the \( COM \) pin. When these two pins are tied together, the LTC6090 is disabled if the junction temperature of the die reaches 145°C. Note that these pins can float and be tied together.

An additional thermal safety feature shuts off the output stage when the junction temperature of the die reaches approximately 175°C. The 7°C of hysteresis enables the output stage when it returns to approximately 168°C as shown in Figure 8. Note that Figure 8 shows the junction temperature. This feature is intended to prevent the device from thermal catastrophic failure. Operating the LTC6090 above its absolute maximum junction temperature of 150°C can reduce reliability and is discouraged.

CONCLUSION

The LTC6090 features the high performance specs of a low voltage precision amplifier, but with the ability to work with ±70V for high voltage applications. These features include high gain, low input bias current, low offset and low noise for a precision front end. A rail-to-rail output stage can drive a 200pF load capacitor and ±10mA of load current, making this part suitable for precision high voltage applications such as high impedance amplifiers. Easily interfaced control lines for disabling the output and a thermal shutdown function are simple to implement. Small 8-lead SO and 16-lead TSSOP packages both have exposed pads to reduce thermal resistance, eliminating the need for a heat sink.

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In addition, many devices must remain operating for a period of time after bus failure in order to initiate a controlled shutdown. The \text{LTC3115-1} application shown in Figure 9 is a 24V rail restorer application that maintains a clean and well-regulated 24V output rail from a noisy input supply rail, which can fluctuate above and below the regulation target. In addition, as shown in the waveforms of Figure 10, this supply is able to maintain regulation of its 24V output through momentary interruptions in bus power.

CONCLUSION

The flexibility and high efficiency of the \text{LTC3115-1} make it perfectly suited to meet the demanding needs of the next generation of automotive electronics and portable devices, especially those operated from multiple power sources. Its internal power switches and programmable switching frequency minimize the power solution footprint, supporting the increasing demand for miniaturization of electronic devices in the portable and automotive arenas. Low Burst Mode operation and shutdown quiescent currents prolong battery life and facilitate use in always-active automotive applications.

The \text{LTC3115-1} is ideal for noise-sensitive applications, given its low noise, fixed frequency PWM mode, which produces a predictable and well controlled EMI spectrum with switching edges that can be synchronized to a system clock. Internal soft-start minimizes inrush current during start-up and an internal divider in the control path reduces the impact of input voltage variations, and makes the loop easier to compensate in applications with widely varying input voltages. A programmable input undervoltage lockout allows the input voltage at which the part is enabled to be set by the user, and provides for independent control of the hysteresis. The \text{LTC3115-1} also features complete disconnect of the output from the input in shutdown, and is fully protected with output short-circuit protection and overtemperature shutdown. ■