

# Dual Switcher with Spread Spectrum Reduces EMI

by Jason Leonard

## Introduction

Switching DC/DC power supplies are increasingly popular in modern electronic devices because of their high efficiency, which reduces heat dissipation and increases battery run time. Nevertheless, the rapid switching of current makes them a potential source of radiated and conducted electromagnetic interference (EMI). EMI can cause a variety of problems, from the relatively benign addition of noise to a television picture or radio receiver to the more serious impairment of the operation of electronic devices in critical applications.

Unfortunately, the amount of EMI generated, and whether it will produce significant interference, is not easily quantifiable and is often not known until the late stages of the development. Therefore, it is wise to proactively minimize the potential sources of EMI to save troubleshooting time later on. There are many

Table 1. LTC3736-1's Switching Frequency

SSDIS pin	FREQ pin	Switching Frequency
GND	Filter Capacitor (e.g., 2200pF)	Spread Spectrum (450kHz to 580kHz)
$V_{IN}$	Floating	Constant 550kHz
$V_{IN}$	$V_{IN}$	Constant 750kHz
$V_{IN}$	GND	Constant 300kHz

techniques to significantly reduce EMI, but few are as simple as using Spread Spectrum Frequency Modulation (SSFM) in the clocking of a switching power supply.

Switching regulators operate on a cycle-by-cycle basis to transfer power to an output. In most cases, the frequency of operation is either fixed or is a constant based on the output load. This method of conversion creates high amplitude noise components at the

frequency of operation (fundamental) and at the multiples of the operating frequency (harmonics).

One way to knock down the amplitude of the fundamental and harmonic noise components is to spread the operating frequency around. If the frequency of the switcher is modulated using spread spectrum frequency modulation, the energy of the EMI is spread over many frequencies, instead of concentrated at one frequency and

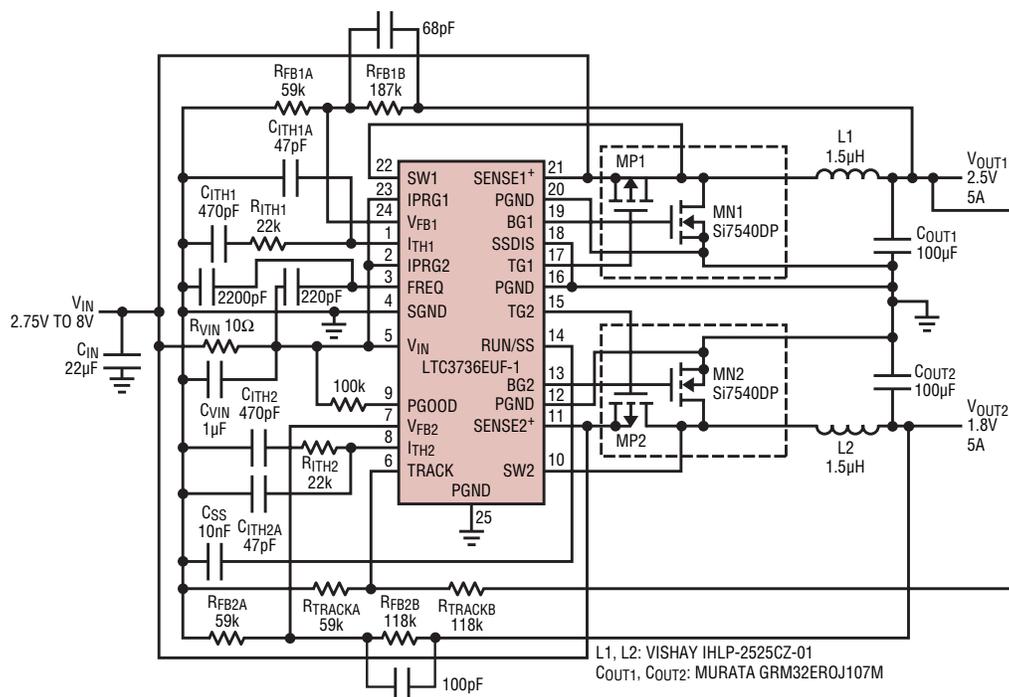
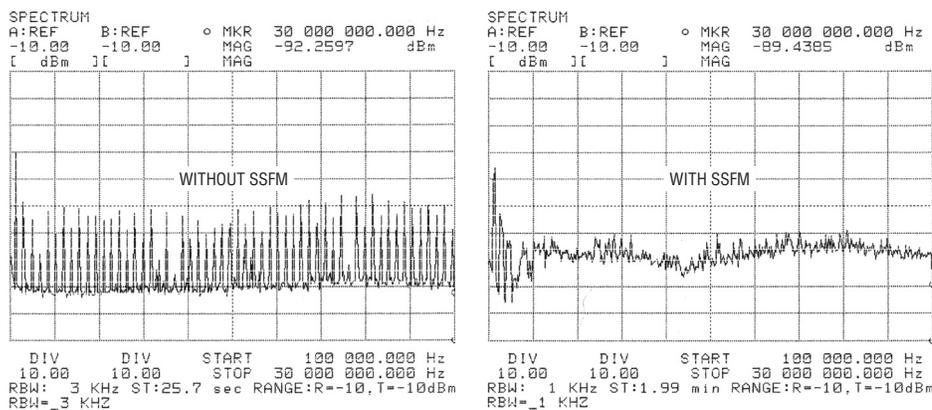
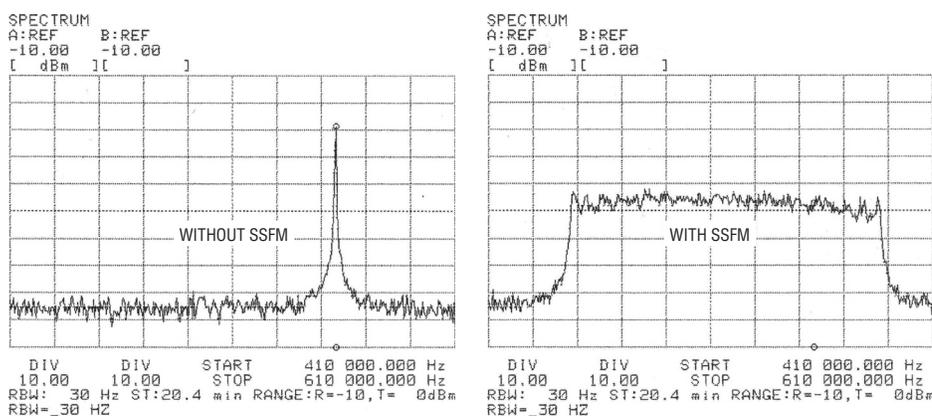


Figure 1. 3.3V to 2.5V and 1.8V dual DC/DC converter with spread spectrum frequency modulation (SSFM). The circuit uses only ceramic capacitors and requires no current sense resistors or Schottky diodes.



**Figure 2. Output voltage spectra for circuit of Figure 1 with and without SSFM enabled. Notice the diminished harmonic peaks with SSFM enabled.**



**Figure 3. Zoom-in of output voltage spectra showing fundamental frequency. Notice the >20dB reduction in peak noise with SSFM enabled.**

its harmonics, thus reducing the peak noise at any given frequency. The LTC3736-1 achieves this by integrating an SSFM oscillator with a dual synchronous switching regulator controller to randomly modulate its clock frequency.

### Circuit Description

The LTC3736-1 is a 2-phase dual synchronous step-down DC/DC controller that requires few external components. Its No  $R_{SENSE}^{TM}$ , current mode architecture eliminates the need for current sense resistors and improves efficiency, without requiring a Schottky diode. The two controllers are operated 180 degrees out of phase, reducing the required input capacitance and power loss and noise due to its ESR.

The LTC3736-1 is nearly identical to the LTC3736 (See ‘2-Phase Dual Synchronous DC/DC Controller with Tracking Provides High Efficiency in

a Compact Footprint’ in the August, 2004 issue of *Linear Technology Magazine*), except the LTC3736-1 has a built-in SSFM oscillator that randomly varies its switching frequency.

A tracking input allows the second output to track the first output (or another supply) during startup, allowing the LTC3736-1 to satisfy the power-up requirements of many microprocessors, FPGAs, DSPs and other digital logic circuits. The LTC3736-1 can operate from input voltages between 2.7V and 9.8V and is available in a low profile 4mm x 4mm leadless QFN package and 24-lead narrow SSOP package.

A typical application circuit using the LTC3736-1 is shown in Figure 1. This circuit provides two regulated outputs from a single 3.3V input supply. The 2200pF capacitor connected to the FREQ pin is used to filter and smooth out the abrupt changes in frequency of the LTC3736-1’s internal

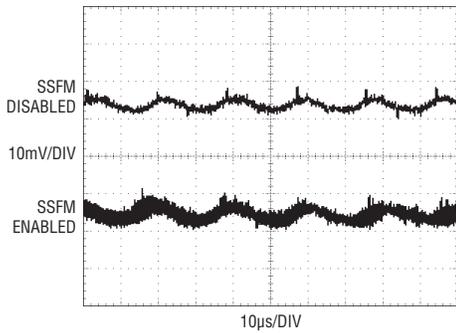
SSFM oscillator. This allows time for the regulator’s feedback control loop to adjust to the frequency changes without adversely affecting output voltage ripple or regulation. The digital input control pin SSDIS is used to disable the SSFM oscillator and force the LTC3736-1 to operate at constant frequency for debugging purposes. Table 1 summarizes how to use the LTC3736-1’s SSDIS and FREQ pins.

Figure 2 shows a comparison of the spectra of the LTC3736-1 with and without SSFM enabled. These show a spectrum analyzer view of the output voltage, using a peak measurement technique. Without SSFM, most of the signal energy in the output appears at the 550kHz switching frequency and its harmonics. With SSFM enabled, the energy is spread among many frequencies and the harmonic peaks are diminished or disappear.

Figure 3 shows a zoom-in of the spectra showing the fundamental frequency. With SSFM enabled, the output signal energy is spread nearly uniformly from 450kHz to 580kHz, with a peak energy more than 20dB below the 550kHz peak with SSFM disabled. In other words, with SSFM enabled, the EMI energy at any particular high frequency has an amplitude that is less than one-tenth that of the single fixed frequency with SSFM disabled. These lower amplitude frequency components reduce the amount of potential interference.

### No Adverse Effect on Transient Response, Ripple, Efficiency, or Tracking

One of the greatest difficulties in implementing an SSFM switcher is ensuring that the randomly changing frequencies do not cause the regulator’s control loop become unstable. This can manifest itself as significantly increased output voltage and inductor current ripples, or worse, total instability and loss of regulation. The LTC3736-1 is proof that these challenges have been overcome, and better yet, all that is required externally is a single capacitor connected to the FREQ pin.



**Figure 4. Output voltage ripple for 1.8V output using “envelope” oscilloscope function**

Figure 4 shows the output voltage ripple for the circuit of Figure 1 with and without SSFM enabled. Note that since SSFM is constantly changing the LTC3736-1 switching frequency, it is difficult to show the true behavior of SSFM using a still oscilloscope snapshot—a video would be much more informative.

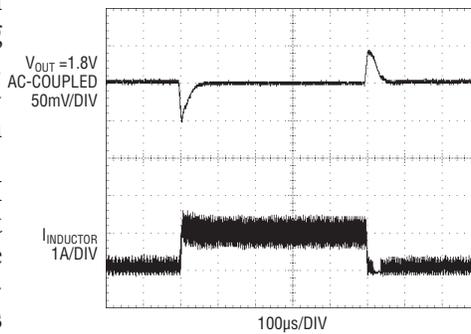
Nonetheless, the scope traces in Figure 4 have been acquired using the “envelope” oscilloscope function, which shows the leading and trailing waveform edges blending in with each other as the frequency is varied. The peak to peak ripple with SSFM enabled does increase slightly, but this is expected since output ripple is inversely proportional to switching frequency, and SSFM introduces some frequencies that are lower than the single fixed 550kHz frequency.

Although it is not easily detected from this still snapshot, note that while the frequency is varying—one can think of SSFM as introducing frequency jitter—the duty cycle is constant. In other words, there is no duty cycle jitter or sub-harmonic instability with SSFM enabled on the LTC3736-1.

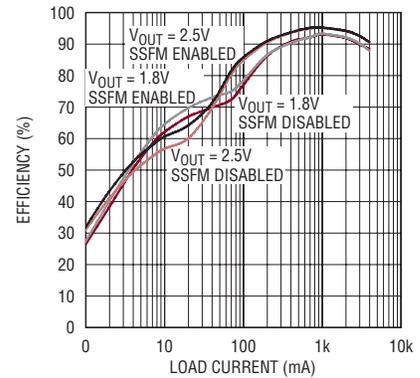
Figure 5 compares the efficiency of the circuit in Figure 1 with and without SSFM enabled. Figure 6 shows load step transients and Figure 7 shows tracking startup waveforms with SSFM enabled. In all cases, the behavior of the LTC3736-1 is unaffected by the addition of SSFM.

### Conclusion

The LTC3736-1 is an easy-to-use dual synchronous switching DC/DC controller that requires few external components. Additionally, it features

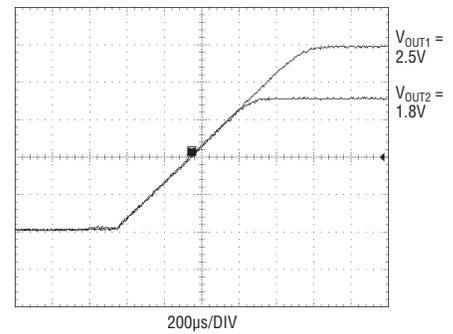


**Figure 6. Load step response for circuit of Figure 1 with SSFM enabled**



**Figure 5. Efficiency for circuit of Figure 1. There is little difference with SSFM enabled**

an internal spread spectrum oscillator that randomly varies the controllers’ switching frequency, providing a simple solution to reduce power-supply-induced EMI that otherwise might require significant and costly troubleshooting and redesign. 



**Figure 7. Startup of circuit of Figure 1 showing the two supplies tracking with SSFM enabled**

*LTC3802, continued from page 8*

reducing the duty cycle and hence the output voltage until the current drops below the limit. The soft-start capacitor needs to move a fair amount before it has any effect on the duty cycle, adding a delay until the current limit takes effect. This allows the LTC3802 to experience brief overload conditions while maintaining output voltage regulation.

Nevertheless, at high input voltages, even a small RUN/SS time delay could cause the output current to overshoot badly during a severe short circuit. To avoid that situation, LTC3802 adds a hard current limit circuit.

If the load current is 1.5 times larger than the programmed current limit threshold, the LTC3802 shuts off the top MOSFET immediately. This stops the increase in the inductor current. At this moment, if CMPIN (which samples  $V_{OUT}$ ) is 10% lower than its nominal value, the LTC3802 hard current-limit latches and discharges the RUN/SS capacitor with a current source of more than 1mA until RUN/SS hits its shutdown threshold. Once RUN/SS is completely discharged, the LTC3802 cycles its soft start cycle again. Figure 8 shows waveforms during a severe short circuit at the output of a 12V–3.3V converter.

### Conclusion

The high efficiency LTC3802 is the latest member of Linear Technology’s family of constant frequency, voltage feedback, synchronous N-channel controllers. With its unique set of powerful features and performance improvements (summarized in Table 1), it improves on the LTC1702/LTC1702A, and is ideal for high input voltage and low duty cycle applications. The LTC3802 is available in small 28-Lead SSOP and 32-Lead (5mm × 5mm) QFN Packages, allowing an entire 87W converter to be laid out in less than 6 square inches (Figure 9). 