EN55022B Compliant 40V, Dual 4A or Single 8A Step-Down or 50W Inverting µModule Regulator

FEATURES
- Dual 4A/Single 8A Low EMI Switch Mode Power Supply
- EN55022 Class B Compliant
- Two Fully Independent Channels, Each Configurable for Positive or Negative Output Voltage Polarity
- Output Voltage Range: 0.5V ≤ |VOUTn+ − VOUTn−| ≤ 26.5V
- Wide Input Voltage Range: Up to 40V
- 3.1V or 3.6V Start-Up, Configuration-Dependent
- ±1.67% Total DC Output Voltage Error Over Line, Load and Temperature
- Analog Output Current Indicator (Positive-VOUT Only)
- LDOOUT: 5V Fixed, 25mA Capable LDO
- Parallelable with LTM4651/LTM4653
- Constant-Frequency Current Mode Control
- Power Good Indicators and Programmable Soft-Start
- Overcurrent and Overtemperature Protection
- 16mm × 16mm × 5.01mm BGA Package

APPLICATIONS
- Automated Test and Measurement
- Avionics and Industrial Control Systems
- Video, Imaging and Instrumentation

DESCRIPTION
The LTM®4655 is an ultralow noise 40V, dual 4A or single 8A DC/DC µModule® regulator designed to meet the radiated emissions requirements of EN55022. Its channels are fully independent, parallelable and capable of delivering positive or negative output polarity. Conducted emission requirements can be met by adding standard filter components. Included in the package are the switching controllers, power MOSFETs, inductors, filters and support components. A 5V, 25mA LDO and clock generator enable phase interleaving of the power switching stages, for improved EMC performance.

The LTM4655 can regulate positive VOUTn+ voltages between 0.5V and 26.5V from a 3.1V to 40V input. The LTM4655 can regulate negative VOUTn− voltages between −0.5V and −26.5V from a maximum input range of 3.6V to 40V, with the span from Vinn to VOUTn− not to exceed 40V. A switching frequency range of 250kHz to 3MHz is supported.

The LTM4655 is offered in a 16mm × 16mm × 5.01mm BGA package with SnPb or RoHS compliant terminal finish.

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PIN CONFIGURATION

LTM4655

ABSOLUTE MAXIMUM RATINGS

(Note 1 and Note 5)

Channel 1 Terminal Voltages (All Channel 1 Terminal Voltages Relative to VOUT1– Unless Otherwise Indicated)

\[ V_{IN1}, V_{D1}, SV_{IN1}, SV_{INF1}, SW1 \ldots -0.3V \text{ to } 42V \]

\[ \text{GND, EXTVCC1, VOUT1+, VOSNS1+, ISET1a, ISET1b} \ldots -0.3V \text{ to } 28V \]

\[ \text{INTVCC1, PGDFB1, VINREG1, COMP1a, IMON1a, IMON1b} \ldots -0.3V \text{ to } 4V \]

\[ f_{SET1} \ldots \text{INTVCC1} \]

\[ \text{RUN1} \ldots \text{GND–0.3V to VOUT1– + 32V} \]

\[ \text{PGOOD1, CLKIN1 (Relative to GND)} \ldots -0.3V \text{ to } 6V \]

Channel 2 Terminal Voltages (All Channel 2 Terminal Voltages Relative to VOUT2– Unless Otherwise Indicated)

\[ V_{IN2}, V_{D2}, SV_{IN2}, SV_{INF2}, SW2 \ldots -0.3V \text{ to } 42V \]

\[ \text{GND, EXTVCC2, VOUT2+, VOSNS2+, ISET2a, ISET2b} \ldots -0.3V \text{ to } 28V \]

\[ \text{INTVCC2, PGDFB2, VINREG2, COMP2a, IMON2a, IMON2b} \ldots -0.3V \text{ to } 4V \]

\[ f_{SET2} \ldots \text{INTVCC2} \]

\[ \text{RUN2} \ldots \text{GND–0.3V to VOUT2– + 32V} \]

\[ \text{PGOOD2, CLKIN2 (Relative to GND)} \ldots -0.3V \text{ to } 6V \]

LDO and Clock Generator Voltages (All LDO and Clock Generator Terminal Voltages Relative to GND Unless Otherwise Indicated)

\[ \text{LDOIN} \ldots -0.3V \text{ to } 42V \]

\[ \text{CLKSET, MOD} \ldots -0.3V \text{ to } \text{LDOOUT} + 0.3V \]

Terminal Currents

\[ \text{INTVCCn Peak Output Current (Note 10)} \ldots 30mA \]

\[ \text{TEMP+} \ldots -1mA \text{ to } 10mA \]

\[ \text{TEMP–} \ldots -10mA \text{ to } 1mA \]

Temperatures Internal Operating Temperature Range (Note 2 and Note 9)

\[ \text{E- and I-Grade} \ldots -40°C \text{ to } 125°C \]

\[ \text{MP-Grade} \ldots -55°C \text{ to } 125°C \]

Storage Temperature Range \ldots -55°C \text{ to } 125°C

Peak Package Body Temperature During Reflow \ldots 245°C

For more information www.analog.com
LTM4655

ORDER INFORMATION

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<th>PAD OR BALL FINISH</th>
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<td>LTM4655Y e1</td>
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<td>–40°C to 125°C</td>
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<tr>
<td>LTM4655IY#PBF</td>
<td>SAC305 (RoHS)</td>
<td>LTM4655Y e1</td>
<td>BGA</td>
<td>3</td>
<td>–40°C to 125°C</td>
</tr>
<tr>
<td>LTM4655MPY#PBF</td>
<td>SAC305 (RoHS)</td>
<td>LTM4655Y e1</td>
<td>BGA</td>
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<td>LTM4655MPY</td>
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- Contact the factory for parts specified with wider operating temperature ranges. *Pad or ball finish code is per IPC/JEDEC J-STD-609.
- Recommended LGA and BGA PCB Assembly and Manufacturing Procedures
- LGA and BGA Package and Tray Drawings

ELECTRICAL CHARACTERISTICS

The ● denotes the specifications which apply over the specified internal operating temperature range (Note 2). Specified as each individual output channel (Note 5). TA = 25°C, Test Circuit 1 (positive-VOUT, noninverting step-down configuration with VOUT− = GND), VINn = SVINn = 36V, EXTVCOn = 24V, RUNn = 3.3V, RISETr = 480k, RISETRn = 57.6kΩ, fSWn = 1.5MHz (CLKIn driven with 1.5MHz clock signal) and voltages referred to GND unless otherwise noted.

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<td>VOUT− = GND</td>
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<td>125°C</td>
<td>●</td>
<td>V</td>
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<td>VOUTn(RANGE)+</td>
<td>Range of Positive Output Voltage Regulation</td>
<td>0.5V ≤ ISETna – SVOUTn− ≤ 26.5V, IOUTn+ = 0A</td>
<td>●</td>
<td>0.5</td>
<td>26.5</td>
<td>V</td>
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<td>VOUTn(24VDC)+</td>
<td>Output Voltage Total Variation with Line and Load at VOUTn+ = 24V</td>
<td>29V ≤ VIN ≤ 40V, 0A ≤ IOUTn+ ≤ 4A, CINHn = 4.7μF, CDn = 4.7μF, COUTHn = 2 × 47μF, CLKIn Driven with 1.5MHz Clock</td>
<td>●</td>
<td>23.6</td>
<td>24.4</td>
<td>V</td>
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<td>VOUTn(0.5VDC)+</td>
<td>Output Voltage Total Variation with Line and Load at VOUTn+ = 0.5V</td>
<td>Measuring VOSNS+ to ISETna 3.1V ≤ VINn ≤ 13.2V, 0A ≤ IOUTn+ ≤ 4A, CINHn = 4.7μF, CDn = 4.7μF, COUTHn = 2 × 47μF, ISETna = 500mV, RISETr = N/U (Note 6)</td>
<td>●</td>
<td>–15</td>
<td>0</td>
<td>15 mV</td>
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<td>RSVINF</td>
<td>Resistor Between SVINn and SVAFIn</td>
<td></td>
<td>1</td>
<td></td>
<td></td>
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Input Specifications

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<td>●</td>
<td>2.85</td>
<td>3.1</td>
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<td>300 mA</td>
<td>150</td>
<td>250</td>
<td>mA</td>
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<td>ID(VVINn)</td>
<td>Input Supply Bias Current</td>
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<td>16 μA</td>
<td>450</td>
<td>30</td>
<td>μA</td>
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<td>Input Supply Current</td>
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<td></td>
<td></td>
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<td>IS(VVINn, SHUTDOWN)</td>
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<td>IOUTn+ = 0A, 29V ≤ VINVn ≤ 40V</td>
<td>●</td>
<td>0.05</td>
<td>0.1</td>
<td>%</td>
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**ELECTRICAL CHARACTERISTICS**

The ● denotes the specifications which apply over the specified internal operating temperature range (Note 2). Specified as each individual output channel (Note 5). $T_A = 25^\circ C$, Test Circuit 1 (positive-$V_{OUT}$, noninverting step-down configuration with $V_{OUT} = GND$). $V_{IN} = SV_{IN} = 36V$, $EXTV_{CC} = 24V$, $RUN = 3.3V$, $R_{ISET} = 480k$, $R_{ISET}^+ = 57.6k\Omega$, $f_{SW} = 1.5MHz$ (CLKIN driven with 1.5MHz clock signal) and voltages referred to GND unless otherwise noted.

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<td>$V_{OUT}$芮 Ripple Frequency</td>
<td>$R_{ISET} = 57.6k$, CLKINn Open Circuit</td>
<td>● 1.7</td>
<td>1.95</td>
<td>2.2</td>
<td>MHz</td>
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<td>$\Delta V_{OUT}(START)^+$</td>
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<td>8</td>
<td>mV</td>
<td></td>
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<td>$t_{START}$</td>
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<td>Delay Measured from $V_{IN}$ Toggling from 0V to 36V to PGODn Exceeding 3V, PG00Dn. Having a 100kΩ Pull-Up to 3.3V with Respect to GND, VPGFBn Resistor Divider Network as Shown in Test Circuit 1, $R_{ISET} = 480k\Omega$ and ISETn Electrically Connected to ISETn and CLKIN Driven with 1.5MHz Clock</td>
<td>● 4</td>
<td>9</td>
<td>ms</td>
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<td>Peak Output Voltage Deviation for Dynamic Load Step</td>
<td>($I_{OUT}^+$: 0A to 2A and 2A to 0A Load Steps in 1μs, $C_{OUTH} = 47\mu F \times 2$)</td>
<td>400</td>
<td>mV</td>
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<td>Settling Time for Dynamic Load Step</td>
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<td>Reference Current of ISETn Pin</td>
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<td>50</td>
<td>50.7</td>
<td>μA</td>
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<td>$V_{VOSNSn} = 28V$</td>
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**Oscillator and Phase-Locked Loop (PLL)**

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<td>Oscillator Frequency Accuracy</td>
<td>$V_{IN} = 12V$, ISETn = 5V, and: $V_{ISETn} = 0.5V$, $3.1V \leq V_{IN} \leq 13.2V$ $V_{ISETn} = 24V$, $29V \leq V_{IN} \leq 40V$</td>
<td>● 360</td>
<td>400</td>
<td>440</td>
<td>kHz</td>
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<td>$f_{SYNC}$</td>
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<td>kHz</td>
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<td></td>
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<td>$V_{CLKIN}$</td>
<td>CLKINn Input Threshold</td>
<td>$V_{CLKIN} = 0V$, $V_{CLKIN} = 5V$, $V_{CLKIN} = 5V$, $V_{CLKIN} = 0V$</td>
<td></td>
<td></td>
<td></td>
<td></td>
</tr>
<tr>
<td>$I_{CLKIN}$</td>
<td>CLKINn Input Current</td>
<td>$V_{CLKIN} = 5V$</td>
<td>20</td>
<td>μA</td>
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**Power Good Feedback Input and Power Good Output**

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<td>PGDFBn Returning</td>
<td>8</td>
<td>mV</td>
<td></td>
<td></td>
</tr>
<tr>
<td>$R_{PGDFBn}$</td>
<td>Resistor Between PGDFBn and SVOUTn</td>
<td>4.94</td>
<td>4.99</td>
<td>5.04</td>
<td>kΩ</td>
<td></td>
</tr>
<tr>
<td>$R_{PGOODn}$</td>
<td>PGODn Pull-Down Resistance</td>
<td>$V_{PGOODn} = 0.1V$, $V_{PGOODn} = 0.1V$, $V_{PGOODn} &lt; UV_{PGOODn}$ or $V_{PGOODn} &gt; OV_{PGOODn}$</td>
<td>700</td>
<td>1500</td>
<td>Ω</td>
<td></td>
</tr>
<tr>
<td>$I_{PGOOD(n)(LEAK)}$</td>
<td>PGODn Leakage Current</td>
<td>$V_{PGOODn} = 3.3V$, $UV_{PGOODn} &lt; V_{PGOODn} &lt; OV_{PGOODn}$</td>
<td>0.1</td>
<td>1</td>
<td>μA</td>
<td></td>
</tr>
</tbody>
</table>
# ELECTRICAL CHARACTERISTICS

The ● denotes the specifications which apply over the specified internal operating temperature range (Note 2). Specified as each individual output channel (Note 5). $T_A = 25^\circ C$, Test Circuit 1 (positive-$V_{OUT}$, noninverting step-down configuration with $V_{OUT} = GND$). $V_{IN} = SV_{IN} = 36V$, $EXTV_{CC} = 24V$, $RUN = 3.3V$, $I_{SET} = 480k$, $R_{SET} = 57.6k\Omega$, $f_{SW} = 1.5MHz$ (CLKIN driven with 1.5MHz clock signal) and voltages referred to GND unless otherwise noted.

## SYMBOL | PARAMETER | CONDITIONS | MIN | TYP | MAX | UNITS
--- | --- | --- | --- | --- | --- | ---
$I_{PGOODn(Delay)}$ | $PGOODn$ Delay | $PGOODn$ Low to High (Note 4) $PGOODn$ High to Low (Note 4) | 16/$f_{SW(Hz)}$ | 64/$f_{SW(Hz)}$ | s | s

### Current Monitor and Input Voltage Regulation Pins

| SYMBOL | PARAMETER | CONDITIONS | MIN | TYP | MAX | UNITS
--- | --- | --- | --- | --- | --- | ---
$I_{IOUTn/IMONn}$ | $I_{IOUTn}$/$I_{IMONn}$ Ratio of $V_{OUTn}$ Output Current to $I_{IMONn}$ Current, $I_{OUTn}$ = 4A | ● | 36 | 40 | 44 | k
$I_{IMon(n)}$ | $I_{IMONn}$ Offset Current | $I_{IMONn}$ at $I_{OUTn}$ = 0A | -5 | 5 | μA
$IMON_{R(n)}$ | Resistor Between $IMON_{R(n)}$ and $SV_{OUTn}$ | 9.8 | 10 | 10.2 | kΩ
$V_{IMONn}$ | $IMONn$ Servo Voltage | $IMONn$ Voltage During Output Current Regulation | ● | 1.9 | 2.0 | 2.1 | V
$V_{VINREGn}$ | $VINREGn$ Servo Voltage | $VINREGn$ Voltage During Output Current Regulation | ● | 1.8 | 2.0 | 2.2 | V

## SYMBOL | PARAMETER | CONDITIONS | MIN | TYP | MAX | UNITS
--- | --- | --- | --- | --- | --- | ---
$SV_{IN(n)}$/$V_{IN(n)}$ | Input DC Voltage in Negative-$V_{OUT}$ Configuration | $V_{IN} + V_{OUT} \leq 40V$ | 3.6 | 40 | V

### ELECTRICAL CHARACTERISTICS

The ● denotes the specifications which apply over the specified internal operating temperature range (Note 2). Specified as each individual output channel (Note 5). $T_A = 25^\circ C$, Test Circuit 2 (negative-$V_{OUT}$, inverting buck-boost configuration with $V_{OUT} = GND$). $V_{IN} = 12V$ and electrically connected to $SV_{IN}$, $RUN = GND = 3.3V$, $I_{SET} = 24V$, $EXTV_{CC} = GND$, CLKIN open circuit, $R_{SET} = 57.6k\Omega$ and $R_{SET} = 480k\Omega$ and voltages referred to GND unless otherwise noted.

## SYMBOL | PARAMETER | CONDITIONS | MIN | TYP | MAX | UNITS
--- | --- | --- | --- | --- | --- | ---
$SV_{IN(n)}$/$V_{IN(n)}$ | Input DC Voltage in Negative-$V_{OUT}$ Configuration | $V_{IN} + V_{OUT} = 40V$ | 3.6 | 40 | V

### ELECTRICAL CHARACTERISTICS

The ● denotes the specifications which apply over the specified internal operating temperature range (Note 2). Specified as each individual output channel (Note 5). $T_A = 25^\circ C$, Test Circuit 2 (negative-$V_{OUT}$, inverting buck-boost configuration with $V_{OUT} = GND$). $V_{IN} = 12V$ and electrically connected to $SV_{IN}$, $RUN = GND = 3.3V$, $I_{SET} = 24V$, $EXTV_{CC} = GND$, CLKIN open circuit, $R_{SET} = 57.6k\Omega$ and $R_{SET} = 480k\Omega$ and voltages referred to GND unless otherwise noted.

## SYMBOL | PARAMETER | CONDITIONS | MIN | TYP | MAX | UNITS
--- | --- | --- | --- | --- | --- | ---
$SV_{IN(n)}$/$V_{IN(n)}$ | Input DC Voltage in Negative-$V_{OUT}$ Configuration | $V_{IN} + V_{OUT} = 40V$ | 3.6 | 40 | V

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## SYMBOL | PARAMETER | CONDITIONS | MIN | TYP | MAX | UNITS
--- | --- | --- | --- | --- | --- | ---
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## SYMBOL | PARAMETER | CONDITIONS | MIN | TYP | MAX | UNITS
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## SYMBOL | PARAMETER | CONDITIONS | MIN | TYP | MAX | UNITS
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## SYMBOL | PARAMETER | CONDITIONS | MIN | TYP | MAX | UNITS
--- | --- | --- | --- | --- | --- | ---
$SV_{IN(n)}$/$V_{IN(n)}$ | Input DC Voltage in Negative-$V_{OUT}$ Configuration | $V_{IN} + V_{OUT} = 40V$ | 3.6 | 40 | V

### ELECTRICAL CHARACTERISTICS

The ● denotes the specifications which apply over the specified internal operating temperature range (Note 2). Specified as each individual output channel (Note 5). $T_A = 25^\circ C$, Test Circuit 2 (negative-$V_{OUT}$, inverting buck-boost configuration with $V_{OUT} = GND$). $V_{IN} = 12V$ and electrically connected to $SV_{IN}$, $RUN = GND = 3.3V$, $I_{SET} = 24V$, $EXTV_{CC} = GND$, CLKIN open circuit, $R_{SET} = 57.6k\Omega$ and $R_{SET} = 480k\Omega$ and voltages referred to GND unless otherwise noted.
### ELECTRICAL CHARACTERISTICS

The ● denotes the specifications which apply over the specified internal operating temperature range (Note 2). Specified as each individual output channel (Note 5). $T_A = 25^\circ C$, Test Circuit 2 (negative-$V_{OUTn}^-$, inverting buck-boost configuration with $V_{OUTn}^+ = GND$). $V_{INn} = 12V$ and electrically connected to $SV_{INn}$, $RUNn$-$GND = 3.3V$, $ISETn$-$SV_{OUTn}^-$ = 24V, $EXTV_{CCN} = GND$, CLKIN$n$ open circuit, $R_{ISETn} = 57.6k\Omega$ and $R_{ISETn} = 480k\Omega$ and voltages referred to $GND$ unless otherwise noted.

#### SYMBOL | PARAMETER | CONDITONS | MIN | TYP | MAX | UNITS
--- | --- | --- | --- | --- | --- | ---

### Input Specifications

- $V_{INn(VLDO)}$ $\rightarrow$ SV$_{IN}$, Undervoltage Lockout Threshold
  - SV$_{IN}$ Rising
  - SV$_{IN}$ Falling
  - Hysteresis
  - $\bullet$ 3.2
  - $\bullet$ 2.1
  - $\bullet$ 2.5
  - $\bullet$ 2.8
  - $\bullet$ 3.6
  - $\bullet$ V

- $I_{INRUSH(VIN)}$ Input Inrush Current at Start-Up
  - $C_{INH} = 4.7\mu F$, $CDn = 4.7\mu F \times 2$, $C_{OUTH} = 47\mu F \times 2$; $I_{OUT} = 0A$, $ISET$ Electrically Connected to $ISET_{nb}$
  - $\bullet$ 1.1
  - $\bullet$ A

- $I_Q(SVINn)$ Input Supply Bias Current Shutdown, $RUNn$-$GND = 3.3V$
  - $\bullet$ 16
  - $\bullet$ 450
  - $\bullet$ 30
  - $\bullet$ μA

- $I_S(VINn)$ Input Supply Current
  - CLKIN$n$ Open Circuit, $I_{OUT} = 1.25A$
  - $\bullet$ 3.0
  - $\bullet$ A

### Output Specifications

- $I_{OUTn}^-$ $\rightarrow$ Output Continuous Current Range
  - $V_{IN} = 12V$, Regulating $V_{OUTn}^-$ = –24V at $f_{SW} = 1MHz$
  - $\bullet$ 0
  - $\bullet$ 1.25
  - $\bullet$ 3
  - $\bullet$ A

- $\Delta V_{OUTn}(LINE)/\Delta V_{OUTn}^-$ Line Regulation Accuracy
  - $I_{OUT}^-$ = 0A, 3.6V $\leq V_{IN} \leq 16V$, $ISETn$-$SV_{OUT}^-$ = 24V, CLKIN$n$ Driven by 1.8MHz Clock
  - $\bullet$ 0.05
  - $\bullet$ 0.25
  - $\bullet$ %

- $\Delta V_{OUTn}(LOAD)/\Delta V_{OUTn}^-$ Load Regulation Accuracy
  - $V_{IN} = 12V$, 0A $\leq I_{OUT}^-$ $\leq 1.25A$, CLKIN$n$ Driven by 1.5MHz Clock, $R_{ISETn} = 57.6k\Omega$, and $R_{ISETn} = 480k\Omega$
  - $\bullet$ 0.05
  - $\bullet$ 0.75
  - $\bullet$ %

- $V_{OUTn(AC)}$ Output Voltage Ripple, $V_{OUTn}^-$
  - $V_{IN} = 12V$, $ISETn$-$SV_{OUT}^-$ = 5V
  - $\bullet$ 1.7
  - $\bullet$ 1.95
  - $\bullet$ 2.2
  - $\bullet$ MHz

- $f_{SN}$ $\rightarrow$ Ripple Frequency
  - $V_{IN} = 12V$, $ISETn$-$SV_{OUT}^-$ = 5V
  - $\bullet$ 8
  - $\bullet$ mV

- $\Delta V_{OUTn}(START)$ Turn-On Overshoot
  - Delay Measured from $V_{INn}$, Toggling from 0V to 12V to PGOOD$n$ Exceeding 3V Above GND; PGOOD$n$ Having a 100kΩ Pull-Up to 3.3V with Respect to GND, $V_{PGFBn}$ Resistor Divider Network as Shown in Test Circuit 2, $R_{ISETn} = 480k\Omega$, $ISETn$ Electrically Connected to $ISETn$, and CLKIN$n$ Driven with 1.2MHz Clock
  - $\bullet$ 4
  - $\bullet$ 9
  - $\bullet$ ms

- $\Delta V_{OUTn}(LSI)$ Peak Output Voltage Deviation for Dynamic Load Step
  - $I_{OUT}^-$: 0A to 1A and 1A to 0A Load Steps in 1μs, $C_{OUTn} = 47\mu F \times 2$
  - $\bullet$ 400
  - $\bullet$ mV

- $\Delta V_{OUTn}(SETTLE)$ Settling Time for Dynamic Load Step
  - $I_{OUT}^-$: 0A to 1A and 1A to 0A Load Steps in 1μs, $C_{OUTn} = 47\mu F \times 2$ X5R
  - $\bullet$ 50
  - $\bullet$ μs

- $\Delta V_{OUTn}(OCL)$ $\rightarrow$ Output Current Limit
  - $\bullet$ 1.7
  - $\bullet$ A

### Control Section

- $I_{ISETn}$ Reference Current of $ISETn$ Pin
  - $ISETn$-$SV_{OUT}^-$ = 0.5V, 3.6V $\leq V_{IN} \leq 28V$
  - 0V $\leq V_{ISETn}$-$SV_{OUT}^-$ $\leq V_{INn}$-$SV_{OUT}^-$ $\leq 40V$
  - $\bullet$ 49.3
  - $\bullet$ 50
  - $\bullet$ 50.7
  - $\bullet$ μA

- $I_{VDSNSn}^+$ $\rightarrow$ Leakage Current
  - $V_{DSNSn}^+ = V_{DSNSn} = 28V$
  - $\bullet$ 290
  - $\bullet$ μA

- $I_{On(MIN)}$ Minimum On-Time
  - (Note 4 )
  - $\bullet$ 60
  - $\bullet$ ns

- $V_{RUNn}$ RUNn Turn-On/Off Thresholds
  - $V_{RUNn}$ Input Turn-On Threshold, $RUNn$ Rising $RUNn$ Hysteresis (RUNn Thresholds Measured with Respect to GND)
  - $\bullet$ 1.08
  - $\bullet$ 1.2
  - $\bullet$ 1.32
  - $\bullet$ V

- $I_{RUNn}$ $\rightarrow$ Leakage Current
  - $V_{IN} = 12V$, $RUNn$-$GND = 3.3V$
  - $\bullet$ 0.1
  - $\bullet$ 50
  - $\bullet$ nA
### Electrical Characteristics

The **denotes the specifications which apply over the specified internal operating temperature range (Note 2). Specified as each individual output channel (Note 5).** $T_A = 25^\circ C$, Test Circuit 2 (negative- $V_{OUT}^+$, inverting buck-boost configuration with $V_{OUT}^+ = GND$). $V_{INn} = 12V$ and electrically connected to $SVIN_n = 3.3V$, $ISET_n–SVOUT_n = 24V$, $EXTV_{CC} = GND$, $CLKIn_n$ open circuit, $R_{ISET_n} = 57.6k\Omega$ and $R_{ISET_n} = 480k\Omega$ and voltages referred to GND unless otherwise noted.

<table>
<thead>
<tr>
<th>SYMBOL</th>
<th>PARAMETER</th>
<th>CONDITIONS</th>
<th>MIN</th>
<th>TYP</th>
<th>MAX</th>
<th>UNITS</th>
</tr>
</thead>
<tbody>
<tr>
<td>$f_{OSCn}$</td>
<td>Oscillator Frequency Accuracy</td>
<td>$V_{INn} = 12V$, $ISET_n–SVOUT_n = 5V$, and: $f_{ISET_n}$ Open Circuit $R_{ISET_n} = 57.6k\Omega$ (See $f_{GN}$ Specification)</td>
<td>360</td>
<td>400</td>
<td>440</td>
<td>kHz</td>
</tr>
<tr>
<td>$f_{SYNCn}$</td>
<td>PLL Synchronization Capture Range</td>
<td>$V_{INn} = 12V$, $ISET_n–SVOUT_n = 5V$, $CLKIn_n$ Driven with a GND Referred Clock Toggling from 0.4V to 1.2V and Having a Clock Duty Cycle: From 10% to 90%; $f_{ISET_n}$ Open Circuit From 40% to 60%; $R_{ISET_n} = 57.6k\Omega$</td>
<td>250</td>
<td>550</td>
<td>MHz</td>
<td></td>
</tr>
<tr>
<td>$V_{CLKin}$</td>
<td>CLKin Input Threshold</td>
<td>$V_{CLKin}$ Rising with Respect to GND $V_{CLKin}$ Falling with Respect to GND</td>
<td>1.2</td>
<td>0.4</td>
<td>V</td>
<td></td>
</tr>
<tr>
<td>$I_{CLKin}$</td>
<td>CLKin Input Current</td>
<td>$V_{CLKin} = 5V$ with Respect to GND $V_{CLKin} = 0V$ with Respect to GND</td>
<td>−20</td>
<td>230</td>
<td>500</td>
<td>μA</td>
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<tr>
<td>$OV_{PGDFBn}$</td>
<td>Output Overvoltage $PGODn$ Upper Threshold</td>
<td>$PGDFBn$ Rising, Differential Voltage from $PGDFBn$ to $SVOUT_n$</td>
<td>620</td>
<td>645</td>
<td>675</td>
<td>mV</td>
</tr>
<tr>
<td>$UV_{PGDFBn}$</td>
<td>Output Undervoltage $PGODn$ Lower Threshold</td>
<td>$PGDFBn$ Falling, Differential Voltage from $PGDFBn$ to $SVOUT_n$</td>
<td>525</td>
<td>555</td>
<td>580</td>
<td>mV</td>
</tr>
<tr>
<td>$\Delta V_{PGDFBn}$</td>
<td>$PGODn$ Hysteresis</td>
<td>$PGDFBn$ Returning</td>
<td>8</td>
<td>mV</td>
<td></td>
<td></td>
</tr>
<tr>
<td>$R_{PGDFBn}$</td>
<td>Resistor Between $PGDFBn$ and $SVOUT_n$</td>
<td>4.94</td>
<td>4.99</td>
<td>5.04</td>
<td>kΩ</td>
<td></td>
</tr>
<tr>
<td>$R_{PGODn}$</td>
<td>$PGODn$ Pull-Down Resistance</td>
<td>$V_{PGODn} = 0.1V$ with Respect to GND, $V_{PGDFBn–SVOUT_n} &lt; UV_{PGDFBn}$ or $V_{PGDFBn–SVOUT_n} &gt; OV_{PGDFBn}$</td>
<td>700</td>
<td>1500</td>
<td>Ω</td>
<td></td>
</tr>
<tr>
<td>$I_{PGODn(LEAK)}$</td>
<td>$PGODn$ Leakage Current</td>
<td>$V_{PGODn} = 3.3V$ with Respect to GND, $V_{PGDFBn–SVOUT_n} &lt; UV_{PGDFBn}$</td>
<td>0.1</td>
<td>1</td>
<td>μA</td>
<td></td>
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<tr>
<td>$t_{PGODn(DELAY)}$</td>
<td>$PGODn$ Delay</td>
<td>$PGODn$ Low to High (Note 4) $PGODn$ High to Low (Note 4)</td>
<td>$16/f_{SW(Hz)}$</td>
<td>$64/f_{SW(Hz)}$</td>
<td>s</td>
<td></td>
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<tr>
<td>$V_{INREGn}$</td>
<td>$V_{INREGn}$ Servo Voltage</td>
<td>$V_{INREGn}$ Voltage During Output Current Regulation, Measured with Respect to $SVOUT_n$</td>
<td>1.8</td>
<td>2.0</td>
<td>2.2</td>
<td>V</td>
</tr>
<tr>
<td>$I_{INREGn}$</td>
<td>$V_{INREGn}$ Leakage Current</td>
<td>$V_{INREGn–SVOUT_n} = 2V$</td>
<td>1</td>
<td>nA</td>
<td></td>
<td></td>
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<tr>
<td>$INTV_{CCn}$</td>
<td>Regulator</td>
<td>Channel Internal $V_{CC}$ Voltage, No $INTV_{CC}$ Loading ($I_{INTVCCn} = 0mA$) $3.6V \leq V_{INn–SVOUT_n} \leq 40V$, $EXTV_{CC} = Open Circuit$ $5V \leq V_{INn–SVOUT_n} \leq 40V$, $3.2V \leq EXTV_{CC} &lt; 26.5V$ ($INTV_{CC}$ Measured with Respect to $SVOUT_n$)</td>
<td>3.15</td>
<td>3.4</td>
<td>3.65</td>
<td>V</td>
</tr>
<tr>
<td>$V_{EXTVCCn(TH)}$</td>
<td>$EXTV_{CC}$ Switchover Voltage ($EXTV_{CC}$ Measured with Respect to $SVOUT_n$) (Note 4)</td>
<td>3.15</td>
<td>V</td>
<td></td>
<td></td>
<td></td>
</tr>
<tr>
<td>$\Delta V_{INTVCCn(LOAD)}$/ $V_{INTVCCn}$</td>
<td>$INTV_{CC}$ Load Regulation</td>
<td>$0mA \leq I_{INTVCCn} \leq 30mA$</td>
<td>−2</td>
<td>0.5</td>
<td>2</td>
<td>%</td>
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</table>
### Electrical Characteristics

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<tbody>
<tr>
<td>LDOIN(DC)</td>
<td>LDO Input DC Voltage</td>
<td></td>
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<td></td>
<td></td>
<td>V</td>
</tr>
<tr>
<td>VLDOOUT(DC)</td>
<td>LDO Output Voltage</td>
<td>$VLDOIN = 36V, 0mA \leq I_{LDOOUT} \leq 25mA$</td>
<td>4.5</td>
<td>40</td>
<td></td>
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<tr>
<td></td>
<td></td>
<td>$VLDOIN = 4.5V, 0mA \leq I_{LDOOUT} \leq 20mA$</td>
<td>4.8</td>
<td>5.0</td>
<td>5.2</td>
<td>V</td>
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<td></td>
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<td></td>
<td>2.7</td>
<td>4.1</td>
<td></td>
<td>V</td>
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<tr>
<td>VLDOUT(AC)</td>
<td>Output Voltage Ripple</td>
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<td>2</td>
<td>mVp-p</td>
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<tr>
<td>ILDOOUT(OCL)</td>
<td>Output Current Limit, 5V LDO</td>
<td>$LDOIN = 36V$</td>
<td>140</td>
<td>mA</td>
<td></td>
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</tr>
</tbody>
</table>

#### Clock Generator

<table>
<thead>
<tr>
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<th>MAX</th>
<th>UNITS</th>
</tr>
</thead>
<tbody>
<tr>
<td>∆fOUT</td>
<td>Clock-Generator Frequency Accuracy</td>
<td>$2.7V \leq LDOOUT \leq 5.2V, 200kHz \leq f_{OUT} \leq 3MHz$, MOD Connected to CLKOUT2</td>
<td>±2.5</td>
<td>±7.5</td>
<td></td>
<td>%</td>
</tr>
<tr>
<td>RCLKSET(RANGE)</td>
<td>Frequency Setting Resistor Range</td>
<td>$R_{CLKSET}$ Resistance for Which $–7.5% \leq \Delta f_{OUT} \leq 7.5%$, Over $2.7V \leq LDOOUT \leq 5.2V$, MOD Electrically Connected to CLKOUT2</td>
<td>33.2</td>
<td>499</td>
<td>kΩ</td>
<td></td>
</tr>
<tr>
<td>Period Variation</td>
<td></td>
<td>$LDOOUT = 5V, R_{CLKSET} = 100k\Omega$, MOD Open Circuit</td>
<td>±10</td>
<td></td>
<td></td>
<td></td>
</tr>
<tr>
<td>Duty Cycle</td>
<td></td>
<td>$2.7V \leq LDOOUT \leq 5.2V, 200kHz \leq f_{OUT} \leq 3MHz$, MOD Electrically Connected to CLKOUT2</td>
<td>40</td>
<td>60</td>
<td></td>
<td>%</td>
</tr>
<tr>
<td>φCLKOUT1/φCLKOUT2</td>
<td>Phase Relationship of CLKOUT2 to</td>
<td>$2.7V \leq LDOOUT \leq 5.2V, 200kHz \leq f_{OUT} \leq 3MHz$, MOD Electrically Connected to CLKOUT2</td>
<td>180</td>
<td></td>
<td>Deg</td>
<td></td>
</tr>
<tr>
<td>VOLCLKOUTn</td>
<td>CLKOUTn Output Voltage, Logic High</td>
<td>$CLKOUTn \phi_{VOL}$ Measured with Respect to LDOOUT, $2.7V \leq LDOOUT \leq 5.2V$, $I_{CLKOUTn} = –100\mu A$</td>
<td>–0.4</td>
<td></td>
<td>V</td>
<td></td>
</tr>
<tr>
<td>VOLCLKOUTn</td>
<td>CLKOUTn Output Voltage, Logic Low</td>
<td>$CLKOUTn \phi_{VOL}$ Measured with Respect to GND, $2.7V \leq LDOOUT \leq 5.2V$, $I_{CLKOUTn} = 100\mu A$</td>
<td>0.4</td>
<td></td>
<td>V</td>
<td></td>
</tr>
</tbody>
</table>

#### Temperature Sensor

<table>
<thead>
<tr>
<th>SYMBOL</th>
<th>PARAMETER</th>
<th>CONDITIONS</th>
<th>MIN</th>
<th>TYP</th>
<th>MAX</th>
<th>UNITS</th>
</tr>
</thead>
<tbody>
<tr>
<td>∆VTMP</td>
<td>Temperature Sensor Forward Voltage, $V_{TEMP^+}$ to $V_{TEMP^-}$</td>
<td>$I_{TEMP^+} = 100\mu A$ and $I_{TEMP^-} = –100\mu A$ at $T_A = 25^\circ$C</td>
<td>0.598</td>
<td></td>
<td>V</td>
<td></td>
</tr>
<tr>
<td>TCVTMP</td>
<td>∆VTMP Temperature Coefficient</td>
<td></td>
<td>–2.0</td>
<td></td>
<td>mV/°C</td>
<td></td>
</tr>
<tr>
<td>n</td>
<td>Idealty Factor</td>
<td></td>
<td>1.004</td>
<td></td>
<td></td>
<td></td>
</tr>
</tbody>
</table>

**Note 1:** Stresses beyond those listing under Absolute Maximum Ratings may cause permanent damage to the device. Exposure to any Absolute Maximum Rating conditions for extended periods may affect device reliability and lifetime.

**Note 2:** The LTM4655 is tested under pulsed load conditions such that $V_{J} = T_A$. The LTM4655E is guaranteed to meet performance specifications over the 0°C to 125°C internal operating temperature range. Specifications over the full –40°C to 125°C internal operating temperature range are assured by design, characterization and correlation with statistical process controls.

The LTM4655 is guaranteed to meet specifications over the full –40°C to 125°C internal operating temperature range. The LTM4655MP is tested and guaranteed over the full –55°C to 125°C operating temperature range. Note that the maximum ambient temperature consistent with these specifications is determined by specific operating conditions in conjunction with board layout, the rated package thermal resistance and other environmental factors.

**Note 3:** See output current derating curves for different $V_{IN}$, $V_{OUT}$, and $T_A$, located in the Applications Information section.

**Note 4:** Minimum on-time, PGOOD delay, and $EXTVC_{CR}$ switchover threshold are tested at wafer sort.

**Note 5:** The two power inputs—$V_{IN1}$ and $V_{IN2}$—and their respective power outputs—$V_{OUT1}$ or $V_{OUT2}$, and $V_{OUT1}$ or $V_{OUT2}$, depending on operational configuration—are tested independently in production, in both positive-$V_{OUT}$ (noninverting step-down) and negative-$V_{OUT}$ (inverting buck-boost) configurations. On occasion, a shorthand notation is used in this document that allows $V_{IN}$ to refer to both $V_{IN1}$ and $V_{IN2}$ by virtue of $n$ being permitted to take on a value of 1 or 2. This italicized $n$ notation and convention is extended to all such pin names.

**Note 6:** To ensure minimum on-time criteria is met, $V_{OUT}$ (0.5$V_{DC}$) high line regulation is tested at 13.2$V_{IN}$, with $I_{SET}$ and $CLKIN$ open circuit. $V_{OUT}$ (–0.5$V_{DC}$)– low line regulation is tested at 3.6$V_{IN}$- $I_{SET}$, and $CLKIN$ open circuit.

**Note 7:** See the Applications Information section for dropout criteria.

**Note 8:** $V_{OUT}$ (–24$V_{DC}$)– is tested at 3.6$V_{IN}$ and 16$V_{IN}$, with $CLKIN$ driven with a 1.8MHz clock, $I_{SET}$ to $SV_{OUT}$ = 12V, and $R_{SET}$ = 57.6k. It is also tested at 12$V_{IN}$, with $CLKIN$ driven with a 1.5MHz clock, $R_{SET}$ = 57.6k, and $R_{SET}$ = 480k.

**Note 9:** This IC includes overtemperature protection that is intended to protect the device during momentary overload conditions. Junction temperature may exceed 125°C when overtemperature protection is active. Continuous operation above the specified maximum operating junction temperature may impair device reliability.

**Note 10:** The INTVC$_{CR}$ Abs Max peak output current is specified as the sum of current drawn by circuits internal to the module biased off of INTVC and current drawn by external circuits biased off of INTVC$_{CR}$. Specified independently, for each channel. See the Applications Information section.
TYPICAL PERFORMANCE CHARACTERISTICS

Efficiency vs Load Current at
5V\textsubscript{IN}, Forced Continuous Mode

Efficiency vs Load Current at
12V\textsubscript{IN}, Forced Continuous Mode

Efficiency vs Load Current at
15V\textsubscript{IN}, Forced Continuous Mode

Efficiency vs Load Current at
24V\textsubscript{IN}, Forced Continuous Mode

Efficiency vs Load Current at
36V\textsubscript{IN}, Forced Continuous Mode

1V Transient Response, 24V\textsubscript{IN}
TYPICAL PERFORMANCE CHARACTERISTICS

TA = 25°C, single channel positive-VOUT+ operation only, unless otherwise noted.

Start-Up, No Load

Start-Up, 4A Load

Start-Up, Pre-Bias

Short Circuit, No Load

Short Circuit, 4A Load

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**TYPICAL PERFORMANCE CHARACTERISTICS**

\( T_A = 25^\circ C, \) single channel negative-V\(_{\text{OUT}}\) operation only, unless otherwise noted.

*Current limit frequency-foldback activates at load currents higher than indicated curves. Continuous channel output current capability subject to details of application implementation. Switching frequency set per Table 1. See Notes 2 and 3.*
TYPICAL PERFORMANCE CHARACTERISTICS

$T_A = 25^\circ C$, single channel negative-$V_{\text{OUT-}}$ operation only, unless otherwise noted.

- **5V Transient Response, 24V$_{\text{IN}}$**
  - $V_{\text{OUT-}}$ 100mV/DIV AC-COUPLED
  - $I_{\text{OUT-}}$ 1A/DIV

- **24V Transient Response, 12V$_{\text{IN}}$**
  - $V_{\text{OUT-}}$ 100mV/DIV AC-COUPLED
  - $I_{\text{OUT-}}$ 0.4A/DIV

- **Start-Up, No Load**
  - $V_{\text{IN}}$ 5V/DIV
  - $V_{\text{OUT-}}$ 10V/DIV
  - $R_{\text{PGOOD}}$ 2V/DIV
  - $V_{\text{GOOD}}$ 5V/DIV
  - $I_{\text{PGOOD}}$ 100mA/DIV

- **Start-Up, 1.25A Load**
  - $V_{\text{IN}}$ 5V/DIV
  - $V_{\text{OUT-}}$ 10V/DIV
  - $R_{\text{RUN}}$ 2V/DIV
  - $V_{\text{GOOD}}$ 2V/DIV
  - $I_{\text{PGOOD}}$ 2V/DIV

- **Start-Up, Pre-Bias**
  - $V_{\text{OUT-}}$ 10V/DIV
  - $I_{\text{DIODE}}$ 500mA/DIV
  - $P_{\text{GOOD}}$ 2V/DIV

- **Short Circuit, No Load**
  - $V_{\text{OUT-}}$ 10V/DIV
  - $I_{\text{OUT-}}$ 1A/DIV

- **Short Circuit, 1.25A Load**
  - $V_{\text{OUT-}}$ 10V/DIV
  - $I_{\text{OUT-}}$ 1A/DIV

**FIGURE 48 CIRCUIT, 24V$_{\text{IN}}$**
- $C_{\text{INOUT}} = C_{\text{IGH}} = C_{\text{INH}} = 4.7\mu F$
- $C_{\text{OUT}} = 47\mu F \times 2$,
- $R_{\text{SET}} = 665k\Omega$,
- $R_{\text{EXTVCC}} = 20\Omega$,
- 1.8A TO 3.8A LOAD STEP AT 2AV/DIV

**FIGURE 48 CIRCUIT, APPLICATION OF 12V$_{\text{IN}}$, START-UP INTO NO LOAD**

**FIGURE 48 CIRCUIT, APPLICATION OF 12V$_{\text{IN}}$, START-UP INTO 19.2Ω LOAD**

**FIGURE 48 CIRCUIT, APPLICATION OF 12V$_{\text{IN}}$, START-UP INTO 19.2Ω LOAD**

**FIGURE 48 CIRCUIT, APPLICATION OF 12V$_{\text{IN}}$, START-UP INTO 19.2Ω LOAD**

**FIGURE 48 CIRCUIT, APPLICATION OF 12V$_{\text{IN}}$, START-UP INTO 19.2Ω LOAD**

**FIGURE 48 CIRCUIT, APPLICATION OF 12V$_{\text{IN}}$, START-UP INTO 19.2Ω LOAD**

**FIGURE 48 CIRCUIT, APPLICATION OF 12V$_{\text{IN}}$, START-UP INTO 19.2Ω LOAD**

**FIGURE 48 CIRCUIT, APPLICATION OF 12V$_{\text{IN}}$, START-UP INTO 19.2Ω LOAD**

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PIN FUNCTIONS

V_{IN1} (A1–A3, B3): Channel 1 Power Input Pins. Apply input voltage and input decoupling capacitance directly between V_{IN1} and a power ground (PGND) plane. Either connect PGND to V_{OUT1–} in noninverting step-down applications, where V_{OUT1+} is the regulated positive output voltage—or, connect PGND to V_{OUT1+} in inverting buck-boost applications, where V_{OUT1–} is the regulated negative output voltage.

V_{IN2} (A6–A8, B8): Channel 2 Power Input Pins. Apply input voltage and input decoupling capacitance directly between V_{IN2} and a power ground (PGND) plane. Either connect PGND to V_{OUT2–} in noninverting step-down applications, where V_{OUT2+} is the regulated positive output voltage—or, connect PGND to V_{OUT2+} in inverting buck-boost applications, where V_{OUT2–} is the regulated negative output voltage.

V_{D1} (A4, B4, C4): Drain of Channel 1’s Primary Switching MOSFET. Apply at least one 4.7μF high frequency ceramic decoupling capacitor directly from V_{D1} to V_{OUT1–}. Give this capacitor higher layout priority (closer proximity to the module) than any V_{IN1} decoupling capacitors.

V_{D2} (A9, B9, C9): Drain of Channel 2’s Primary Switching MOSFET. Apply at least one 4.7μF high frequency ceramic decoupling capacitor directly from V_{D2} to V_{OUT2–}. Give this capacitor higher layout priority (closer proximity to the module) than any V_{IN2} decoupling capacitors.

SV_{IN1} (C3): Channel 1 Input Voltage Supplies for Small Signal Circuits. SV_{IN1} is the input to the INTV_{CC1} LDO. Connect SV_{IN1} directly to V_{IN1}.

SV_{IN2} (C8): Channel 2 Input Voltage Supplies for Small Signal Circuits. SV_{IN2} is the input to the INTV_{CC2} LDO. Connect SV_{IN2} directly to V_{IN2}.

SV_{INF1} (B11): Channel 1 Filtered Voltage Supply for Small Signal Circuits. If powering the LTM4655’s 5V LDO from channel 1’s supply for small signal circuits, electrically connect SV_{INF1} and LDO_{IN} with a short trace capable of carrying up to 25mA.

SV_{INF2} (C11): Channel 2 Filtered Voltage Supply for Small Signal Circuits. If powering the LTM4655’s 5V LDO from channel 2’s supply for small signal circuits, electrically connect SV_{INF2} and LDO_{IN} with a short trace capable of carrying up to 25mA.

LDO_{IN} (B12): Input to 5V LDO. Connect LDO_{IN} to either SV_{INF1} or SV_{INF2} with a short trace capable of carrying up to 25mA, depending on which input rail is better suited for powering the 5V LDO. If LDO_{IN} is being powered from SV_{INF1} or SV_{INF2}, no bypass capacitance from LDO_{IN} to GND is needed; otherwise, 0.1μF-to-1μF local bypass capacitance is recommended.

V_{OUT1–} (A5, B5, C5, D5, E5, F5, G4–5, H3, H5, J3–5, K4–5, L4–5, M4–5): Negative Power Output of Channel 1. Either connect V_{OUT1–} to a PGND plane in noninverting step-down applications, where V_{OUT1+} is the regulated positive output voltage—or, connect V_{OUT1+} to PGND in inverting buck-boost applications, where V_{OUT1–} is the regulated negative output voltage.

SV_{OUT1–} (E4, G2, H2): Signal Return of Channel 1. The SV_{OUT1–} pins are the reference node for channel 1’s control loop. A small island of SV_{OUT1–} copper should be extended from the module and used to shield sensitive channel 1 pins and signals from noise—such as those routing to \( f_{SET1} \), \( ISET_{1a/b} \), and \( COMP_{1a/b} \). All SV_{OUT1–} pins are connected to each other internal to the module. Connect Pin H2 to V_{OUT1–} directly under the LTM4655. The remaining SV_{OUT1–} pins can be used for redundant connectivity or routed to an ICT test point for design-for-test considerations, as desired. See the Applications Information section for the layout checklist.

V_{OUT1+} (K1–3, L1–3, M1–3): Positive Power Output of Channel 1. Bypass V_{OUT1+} to V_{OUT1–} local to the module with at least 1μF. The remainder of V_{OUT1+} to V_{OUT1–} bypass caps should be located near channel 1’s load. Either connect V_{OUT1+} to a PGND plane in inverting buck-boost applications, where V_{OUT1–} is the regulated negative output voltage—or, connect V_{OUT1–} to a PGND plane noninverting step-down applications, where V_{OUT1+} is the regulated positive output voltage.
PIN FUNCTIONS

\( V_{\text{OSNS1}}^+ (G1, H1) \): Positive Voltage Sense Input for Channel 1. Route a signal trace from \( V_{\text{OSNS1}}^+ \) to \( V_{\text{OUT1}}^+ \) at channel 1's point-of-load (POL). This provides the feedback signal to channel 1’s control loop. In noisy environments, shield \( V_{\text{OSNS1}}^+ \) from electrical noise by sandwiching the trace between PGND copper. Pins G1 and H1 are electrically connected to each other internal to the module, and thus it is only necessary to connect one \( V_{\text{OSNS1}}^+ \) pin to \( V_{\text{OUT1}}^+ \) at the POL. The remaining \( V_{\text{OSNS1}}^+ \) pin can be used for redundant connectivity or routed to an ICT test point for design-for-test considerations, as desired.

\( V_{\text{OUT2}}^- (A10–12, B10, C10, D10–11, E10–11, F10–11, G9–11, H8, H10–12, J8–10, K9–12, L9–12, M9–12) \): Negative Power Output of Channel 2. Either connect \( V_{\text{OUT2}}^- \) to a PGND plane in noninverting step-down applications, where \( V_{\text{OUT2}}^- \) is the regulated positive output voltage—or, connect \( V_{\text{OUT2}}^- \) to PGND in inverting buck-boost applications, where \( V_{\text{OUT2}}^- \) is the regulated negative output voltage.

\( SV_{\text{OUT2}}^- (E9, G7, H7) \): Signal Return of Channel 2. The \( SV_{\text{OUT2}}^- \) pins are the reference node for channel 2’s control loop. A small island of \( SV_{\text{OUT2}}^- \) copper should be extended from the module and used to shield sensitive channel 2 pins and signals from noise—such as those routing to \( f_{\text{SET2}}, ISET2a/b, \text{and COMP2a/b.} \) All \( SV_{\text{OUT2}}^- \) pins are connected to each other internal to the module. Connect Pin H7 to \( V_{\text{OUT2}}^- \) directly under the LTM4655. The remaining \( SV_{\text{OUT2}}^- \) pins can be used for redundant connectivity or routed to an ICT test point for design-for-test considerations, as desired. See the Applications Information section for the layout checklist.

\( V_{\text{OUT2}}^+ (K6–8, L6–8, M6–8) \): Positive Power Output of Channel 2. Bypass \( V_{\text{OUT2}}^+ \) to \( V_{\text{OUT2}}^- \) local to the module with at least 1μF. The remainder of \( V_{\text{OUT2}}^+ \) to \( V_{\text{OUT2}}^- \) bypass caps should be located near channel 2’s load. Either connect \( V_{\text{OUT2}}^+ \) to a PGND plane in inverting buck-boost applications, where \( V_{\text{OUT2}}^- \) is the regulated negative output voltage—or, connect \( V_{\text{OUT2}}^+ \) to a PGND plane noninverting step-down applications, where \( V_{\text{OUT2}}^+ \) is the regulated positive output voltage.

\( V_{\text{OSNS2}}^+ (G6, H6) \): Positive Voltage Sense Input for Channel 2. Route a signal trace from \( V_{\text{OSNS2}}^+ \) to \( V_{\text{OUT2}}^+ \) at channel 2’s point-of-load (POL). This provides the feedback signal to channel 2’s control loop. In noisy environments, shield \( V_{\text{OSNS2}}^+ \) from electrical noise by sandwiching the trace between PGND copper. Pins G6 and H6 are electrically connected to each other internal to the module, and thus it is only necessary to connect one \( V_{\text{OSNS2}}^+ \) pin to \( V_{\text{OUT2}}^+ \) at the POL. The remaining \( V_{\text{OSNS2}}^+ \) pin can be used for redundant connectivity or routed to an ICT test point for design-for-test considerations, as desired.

\( GND (D4, D9, D12) \): Ground Pins. The logic thresholds for \( RUNn, \text{PGOODn, and CLKINn are electrically referred to GND.} \) GND is also the reference voltage for the 5V-fixed LDO and the \( CLKOUTn \) clock generator. Connect all GND pins to a solid ground plane, PGND.

\( RUN1 (F4) \): Channel 1 Run Control Pin. A voltage above ~1.2V (with respect to GND) commands the module to regulate its output voltage. Undervoltage lockout (UVLO) can be implemented by connecting \( RUN1 \) to the midpoint node formed by a resistor divider between \( V_{\text{IN1}} \) and GND. \( RUN1 \) features ~130mV of hysteresis.

\( RUN2 (F9) \): Channel 2 Run Control Pin. A voltage above ~1.2V (with respect to GND) commands the module to regulate its output voltage. Undervoltage lockout (UVLO) can be implemented by connecting \( RUN2 \) to the midpoint node formed by a resistor divider between \( V_{\text{IN2}} \) and GND. \( RUN2 \) features ~130mV of hysteresis.

\( INTV_{\text{CC1}} (G3) \): Channel 1 Internal Regulator, 3.3V Output with Respect to \( V_{\text{OUT1}}^- \). Channel 1 internal control circuits and MOSFET drivers derive power from \( INTV_{\text{CC1}} \) bias. Leave \( INTV_{\text{CC1}} \) open circuit. An LDO generates \( INTV_{\text{CC1}} \) from either \( SV_{\text{IN1}} \) or \( EXTV_{\text{CC1}} \), when \( RUN1 \) is logic high (\( RUN1–GND > 1.2V \)). The \( INTV_{\text{CC1}} \) LDO is turned off when \( RUN1 \) is logic low (\( RUN1–GND < 1.2V \)). (See \( EXTV_{\text{CC1}} \).)
PIN FUNCTIONS

**INTVCC2 (G8):** Channel 2 Internal Regulator, 3.3V Output with Respect to VOUT2–. Channel 2 internal control circuits and MOSFET drivers derive power from INTVCC2 bias. Leave INTVCC2 open circuit. An LDO generates INTVCC2 from either SVIN2 or EXTVCC2, when RUN2 is logic high (RUN2–GND > 1.2V). The INTVCC2 LDO is turned off when RUN2 is logic low (RUN2–GND < 1.2V). (See EXTVCC2.)

**EXTVCC1 (F3):** External Bias, Auxiliary Input to the INTVCC1 Regulator. When EXTVCC1–VOUT1– > 3.2V and SVIN1 > 5V and RUN1–GND > 1.2V, the INTVCC1 LDO derives power from EXTVCC1 bias instead of SVIN1. This technique reduces LDO losses considerably, resulting in a corresponding reduction in module junction temperature. For applications in which 4V < VOUT1+ – VOUT1– < 28V, connect EXTVCC1 to VOUT1+ through a 15Ω~110Ω resistor and locally decouple EXTVCC1 to VOUT1– with a 1μF ceramic capacitor. Otherwise, connect EXTVCC1 to VOUT1– or leave EXTVCC1 open circuit. See the Applications Information section.

**INTVCC2 (F8):** External Bias, Auxiliary Input to the INTVCC2 Regulator. When EXTVCC2–VOUT2– > 3.2V and SVIN2 > 5V and RUN2–GND > 1.2V, the INTVCC2 LDO derives power from EXTVCC2 bias instead of SVIN2. This technique reduces LDO losses considerably, resulting in a corresponding reduction in module junction temperature. For applications in which 4V < VOUT2+ – VOUT2– < 28V, connect EXTVCC2 to VOUT2+ through a 15Ω~110Ω resistor and locally decouple EXTVCC2 to VOUT2– with a 1μF ceramic capacitor. Otherwise, connect EXTVCC2 to VOUT2– or leave EXTVCC2 open circuit. See the Applications Information section.

**ISET1a (F2):** Accurate 50μA Current Source. Positive input to the error amplifier of channel 1. Connect a resistor RISET1a = ((VOUT1+ – VOUT1–)/50μA) from this pin to SVOUT1– local to the module to program the desired channel 1 output voltage magnitude, VOUT1+ – VOUT1–. A capacitor can be connected from ISET1a to SVOUT1– to soft-start channel 1’s output voltage, i.e., reduce its start-up inrush current. Connect ISET1a to ISET1b in order to achieve default soft-start characteristics if desired. (See ISET1b.)

In addition, the channel 1 output of the LTM4655 can track a voltage applied to this pin. (See the Applications Information section.)

**ISET2a (F7):** Accurate 50μA Current Source. Positive input to the error amplifier of channel 1. Connect a resistor RISET2a = ((VOUT2+ – VOUT2–)/50μA) from this pin to SVOUT2– local to the module to program the desired channel 2 output voltage magnitude, VOUT2+ – VOUT2–. A capacitor can be connected from ISET2a to SVOUT2– to soft-start channel 2’s output voltage, i.e., reduce its start-up inrush current. Connect ISET2a to ISET2b in order to achieve default soft-start characteristics if desired. (See ISET2b.)

In addition, the channel 2 output of the LTM4655 can track a voltage applied to this pin. (See the Applications Information section.)

**PGOOD1 (D1):** Channel 1 Power Good Indicator, Open-Drain Output Pin. PGOOD1 is high impedance when PGDFB1–SVOUT1– is within approximately ±7.5% of 0.6V. PGOOD1 is pulled to GND when PGDFB1 is outside this range.

**PGOOD2 (D6):** Channel 2 Power Good Indicator, Open-Drain Output Pin. PGOOD2 is high impedance when PGDFB2–SVOUT2– is within approximately ±7.5% of 0.6V. PGOOD2 is pulled to GND when PGDFB2 is outside this range.

**ISET1b (F1):** 1.5nF Soft-Start Capacitor for Channel 1. Connect ISET1b to ISET1a to achieve default soft-start characteristics on channel 1, if desired. See ISET1a.

**ISET2b (F6):** 1.5nF Soft-Start Capacitor for Channel 2. Connect ISET2b to ISET2a to achieve default soft-start characteristics on channel 2, if desired. See ISET2a.
**PIN FUNCTIONS**

**PGDFB1 (D2):** Channel 1 Power Good Feedback Programming Pin. Connect PGDFB1 to \( V_{OSNS1} \) through a resistor, \( R_{PGDFB1} \). \( R_{PGDFB1} \) configures the voltage threshold of \( (V_{OUT1^+} - V_{OUT1^-}) \) for which PGOOD1 toggles its state. If the PGOOD1 feature is used, set \( R_{PGDFB1} \) to:

\[
R_{PGDFB1} = \left( \frac{V_{OUT1^+} - V_{OUT1^-}}{0.6V} - 1 \right) \cdot 4.99k \quad (1)
\]

Otherwise, leave PGDFB1 open circuit.

A small filter capacitor (220pF) internal to the LTM4655 on this pin provides high frequency noise immunity for the PGOOD1 output indicator.

**PGDFB2 (D7):** Channel 2 Power Good Feedback Programming Pin. Connect PGDFB2 to \( V_{OSNS2} \) through a resistor, \( R_{PGDFB2} \). \( R_{PGDFB2} \) configures the voltage threshold of \( (V_{OUT2^+} - V_{OUT2^-}) \) for which PGOOD2 toggles its state. If the PGOOD2 feature is used, set \( R_{PGDFB2} \) according to Equation 2.

\[
R_{PGDFB2} = \left( \frac{V_{OUT2^+} - V_{OUT2^-}}{0.6V} - 1 \right) \cdot 4.99k \quad (2)
\]

Otherwise, leave PGDFB2 open circuit.

A small filter capacitor (220pF) internal to the LTM4655 on this pin provides high frequency noise immunity for the PGOOD2 output indicator.

**fSET1 (E3):** Channel 1 Oscillator Frequency Programming Pin. The default switching frequency of channel 1 is 400kHz. If needed, the programmed frequency can be increased by connecting a resistor between \( f_{SET1} \) and \( SV_{OUT1^-} \). Keep \( f_{SET1} \)-related trace lengths short. (See the Applications Information section.) Note the synchronization range of CLKIN1 is approximately ±40% of the oscillator frequency programmed by this \( f_{SET1} \) pin.

**fSET2 (E8):** Channel 2 Oscillator Frequency Programming Pin. The default switching frequency of channel 2 is 400kHz. If needed, the programmed frequency can be increased by connecting a resistor between \( f_{SET2} \) and \( SV_{OUT2^-} \). Keep \( f_{SET2} \)-related trace lengths short. (See the Applications Information section.) Note the synchronization range of CLKIN2 is approximately ±40% of the oscillator frequency programmed by this \( f_{SET2} \) pin.

**CLKIN1 (B1):** Channel 1 Mode Select and Oscillator Synchronization Input. Referred to GND. Leave CLKIN1 open circuit for forced continuous mode operation.

Alternatively, this pin can be driven so as to synchronize the switching frequency of channel 1 to a clock signal. In this condition, channel 1 operates in forced continuous mode and the cycle-by-cycle turn-on of its primary MOSFET is coincident with the rising edge of the clock applied to CLKIN1. Note the synchronization range of CLKIN1 is approximately ±40% of the oscillator frequency programmed by the \( f_{SET1} \) pin. (See the Applications Information section.) The LTM4655 contains a built-in dual 180° out-of-phase clock generator. Electrically connect CLKIN1 to CLKOUT1 with a short trace, if desired, to synchronize the switching frequency of channel 1 to CLKOUT1. If 0° phase interleaving is desired, connect CLKOUT1 to both CLKIN1 and CLKIN2.

**CLKIN2 (B6):** Channel 2 Mode Select and Oscillator Synchronization Input. Referred to GND. Leave CLKIN2 open circuit for forced continuous mode operation.

Alternatively, this pin can be driven so as to synchronize the switching frequency of channel 2 to a clock signal. In this condition, channel 2 operates in forced continuous mode and the cycle-by-cycle turn-on of its primary MOSFET is coincident with the rising edge of the clock applied to CLKIN2. Note the synchronization range of CLKIN2 is approximately ±40% of the oscillator frequency programmed by the \( f_{SET2} \) pin. (See the Applications Information section.) The LTM4655 contains a built-in dual 180° out-of-phase clock generator. Electrically connect CLKIN2 to CLKOUT2 with a short trace, if desired, to synchronize the switching frequency of channel 2 to CLKOUT2. If 0° phase interleaving is desired, connect CLKOUT1 to both CLKIN1 and CLKIN2.
PIN FUNCTIONS

COMP1a (E2): Current Control Threshold and Error Amplifier Compensation Node for Channel 1. The trip threshold of channel 1's current comparator increases with a respective rise in COMP1a voltage. A small filter cap (10pF) internal to the LTM4655 on this pin introduces a high frequency roll-off of the error amplifier response, yielding good noise rejection in the control loop. Often, COMP1a is electrically connected to COMP1b in one's application, thus applying default loop compensation. Loop compensation (a series resistor capacitor) can be applied externally from COMP1a to SVOUT1⁻, if desired or needed, instead. (See COMP1b.)

COMP2a (E7): Current Control Threshold and Error Amplifier Compensation Node for Channel 2. The trip threshold of channel 2's current comparator increases with a respective rise in COMP2a voltage. A small filter cap (10pF) internal to the LTM4655 on this pin introduces a high frequency roll-off of the error amplifier response, yielding good noise rejection in the control loop. Often, COMP2a is electrically connected to COMP2b in one's application, thus applying default loop compensation. Loop compensation (a series resistor capacitor) can be applied externally from COMP2a to SVOUT2⁻, if desired or needed, instead. (See COMP2b.)

COMP1b (E1): Channel 1 Internal Loop Compensation Network. For a majority of applications, the internal, default loop compensation of the LTM4655 is suitable to apply “as is”, and yields very satisfactory results: apply the default loop compensation to channel 1’s control loop by simply connecting COMP1a to COMP1b. When more specialized applications require a personal touch to the optimization of control loop response, this can be easily accomplished by connecting a series resistor-capacitor network from COMP1a to SVOUT1⁻ and leaving COMP1b open circuit.

COMP2b (E6): Channel 2 Internal Loop Compensation Network. For a majority of applications, the internal, default loop compensation of the LTM4655 is suitable to apply “as is”, and yields very satisfactory results: apply the default loop compensation to channel 2’s control loop by simply connecting COMP2a to COMP2b. When more specialized applications require a personal touch to the optimization of control loop response, this can be easily accomplished by connecting a series resistor-capacitor network from COMP2a to SVOUT2⁻ and leaving COMP2b open circuit.

IMON1a (C2): Channel 1 Power Inductor Current Analog Indicator Pin and Current Limit Programming Pin. In positive-VOUT step-down applications, only, the current flowing out of this pin is equal to 1/40,000 of the average channel 1 power inductor current. Optionally apply a parallel resistor-capacitor network to this pin and terminate it to SVOUT1⁻ in order to construct a voltage (VIMON1a⁻SVOUT1⁻) that is proportional to channel 1’s power inductor current.

IMON1a can be connected to IMON1b if the default resistor capacitor termination network provided by IMON1b is desired. If this analog indicator feature is not desired—or, in negative-VOUT– buck-boost applications: connect IMON1a to SVOUT1⁻.

If IMON1a–SVOUT1⁻ exceeds a trip threshold of approximately 2V, an IMON1 control loop servos channel 1 power inductor current accordingly and thus regulates IMON1a–SVOUT1⁻ at 2V. In this manner, the current limit inception threshold of channel 1 can be configured. (See the Applications Information section.)

IMON1b (C1): Channel 1 Power Inductor Analog Indicator Current Default Termination R-C Network. A 10k resistor in parallel with a 10nF capacitor and terminating to SVOUT1⁻ connect to this pin. Connect IMON1b to IMON1a to achieve default power inductor analog indicator current characteristics: 1V (with respect to SVOUT1⁻) at full-scale (4A) load current in positive-VOUT, noninverting step-down applications. (See IMON1a.) If unused, IMON1b can be left open circuit or connected to SVOUT1⁻.
PIN FUNCTIONS

IMON2a (C7): Channel 2 Power Inductor Current Analog Indicator Pin and Current Limit Programming Pin. In positive-V_{OUT} step-down applications, only, the current flowing out of this pin is equal to 1/40,000 of the average channel 2 power inductor current. Optionally apply a parallel resistor-capacitor network to this pin and terminate it to SV_{OUT2} in order to construct a voltage (V_{IMON2a}–SV_{OUT2}) that is proportional to channel 2’s power inductor current.

IMON2a can be connected to IMON2b if the default resistor capacitor termination network provided by IMON2b is desired. If this analog indicator feature is not desired—or, in negative-V_{OUT} buck-boost applications: connect IMON2a to SV_{OUT2}.

If IMON2a–SV_{OUT2} exceeds a trip threshold of approximately 2V, an IMON2 control loop servos channel 2 power inductor current accordingly and thus regulates IMON2a–SV_{OUT2} at 2V. In this manner, the current limit inception threshold of channel 2 can be configured. (See the Applications Information section.)

IMON2b (C6): Channel 2 Power Inductor Analog Indicator Current Default Termination R-C Network. A 10k resistor in parallel with a 10nF capacitor and terminating to SV_{OUT2} connect to this pin. Connect IMON2b to IMON2a to achieve default power inductor analog indicator current characteristics: 1V (with respect to SV_{OUT2}) at full-scale (4A) load current in positive-V_{OUT}, noninverting step-down applications. (See IMON2a.) If unused, IMON2b can be left open circuit or connected to SV_{OUT2}.

VINREG2 (D8): Channel 2 Input Voltage Regulation Programming Pin. Optionally connect this pin to the midpoint node formed by a resistor divider between V_{D2} and V_{OUT2}. If VINREG2–SV_{OUT2} falls below approximately 2V, a VINREG2 control loop servos the power inductor current accordingly and thus regulates VINREG2 at 2V with respect to SV_{OUT2}. (See the Applications Information section.)

If this input voltage regulation feature is not desired on channel 2, connect VINREG2 to INTV_{CC2}.

TEMP+ (J6): Temperature Sensor, Positive Input. Emitter of a 2N3906-genre PNP bipolar junction transistor (BJT). Optionally interface to temperature monitoring circuitry such as LTC2997, LTC2990, LTC2974 or LTC2975. Otherwise leave electrically open.

TEMP− (J7): Temperature Sensor, Negative Input. Collector and base of a 2N3906-genre PNP bipolar junction transistor (BJT). Optionally interface to temperature monitoring circuitry such as LTC2997, LTC2990, LTC2974 or LTC2975. Otherwise leave electrically open.

SW1 (H4): Switching Node of Channel 1 Switching Converter Stage. Used for test purposes. May be routed a short distance with a thin trace to a local test point to monitor switching action of the converter, if desired, but do not route near any sensitive signals; otherwise, leave electrically open circuit.

SW2 (H9): Switching Node of Channel 2 Switching Converter Stage. Used for test purposes. May be routed a short distance with a thin trace to a local test point to monitor switching action of the converter, if desired, but do not route near any sensitive signals; otherwise, leave electrically open circuit.

LDOOUT (G12): Output of the LTM4655’s GND Referenced 5V-Fixed LDO. No bypass capacitance is needed. Powers the clock generator internal to the LTM4655. Can deliver up to 25mA of current.
PIN FUNCTIONS

CLKSET (F12): Clock Generator Frequency Setting Resistor Input. Apply a resistor, $R_{CLKSET}$, between LDOOUT and CLKSET. The clock frequency of CLKOUT1 and CLKOUT2 is set by $R_{CLKSET}$ according Equation 3.

$$f_{CLKOUT1, CLKOUT2} = \frac{10\text{MHz} \cdot 10k\Omega}{R_{CLKSET}(k\Omega)} \quad (3)$$

Resistor values between 32.2k and 400k are supported, corresponding to oscillator frequency settings of 3MHz to 250kHz, respectively. Minimize stray capacitance to this pin.

CLKOUT1 (B2): Squarewave Output of Clock Generator for Channel 1. 180° out-of-phase from CLKOUT2. Minimize stray capacitance to this pin. Connect CLKOUT1 to CLKin1, if desired, to synchronize channel 1 to CLKOUT1. If 0° phase interleaving is desired, connect CLKOUT1 to both CLKin1 and CLKin2.

CLKOUT2 (B7, C12): Squarewave Output of Clock Generator for Channel 2. 180° out-of-phase from CLKOUT1. Minimize stray capacitance to these pins. Connect CLKOUT2 (pin B7, only) to CLKin2, if desired, to synchronize channel 2 to CLKOUT2. If 0° phase interleaving is desired, connect CLKOUT1 to both CLKin1 and CLKin2.

To disable spread spectrum frequency modulation (SFFM), connect CLKOUT2 (pin C12, only) to the MOD pin (pin E12) with a short trace.

The CLKOUT2 pins at locations B7 and C12 are electrically connected together by a signal trace internal to the module. It is pinned out as described purely to facilitate routing of short traces to CLKin2 and MOD. CLKOUT2 should be routed with minimal trace lengths. Minimize stray capacitance to these pins.

MOD (E12): Modulation Setting Input. This three-state input selects among four modulation rate settings. The MOD pin should be tied to GND for the $f_{OUT}/16$ modulation rate. Leaving the MOD pin open circuit selects the $f_{OUT}/32$ modulation rate. The MOD pin should be electrically connected to LDOOUT for the $f_{OUT}/64$ modulation rate. Electrically connecting CLKOUT2 (pin C12, only) to the MOD pin (pin E12) turns the modulation off. Do not route high speed digital logic or signals with fast edges near MOD. Be advised that the $f_{OUT}/16$, $f_{OUT}/32$ and $f_{OUT}/64$ modulation rates are not explicitly tested in factory ATE to demonstrate their stated typical modulation rates; the modulation off setting, however, is.

NC (J1–2, J11–12): No Connect Pins, i.e., Pins with No Internal Connection. The NC pins predominantly serve to provide improved mounting of the module to the board. For drop-in compatibility of the LTM4651/LTM4653 into either half of a LTM4655 layout, these NC are recommended to be left electrically open circuit.
Test Circuit 1. Positive-V\textsubscript{OUT} Configuration, Regulating V\textsubscript{OUT\textsuperscript{+}}, One Channel Shown

Test Circuit 2. Negative-V\textsubscript{OUT\textsuperscript{−}} Configuration, Regulating V\textsubscript{OUT\textsuperscript{−}}, One Channel Shown

*Polarized output capacitors C\textsubscript{OUT\textsuperscript{+}}, if used, must be rated to withstand ~0.3V typical reverse polarity prior to LTM4655 start-up, stemming from a weakly forward-biased body diode. In such cases, a Schottky diode should be connected between PGND and V\textsubscript{OUT\textsuperscript{−}} to limit the voltage. See the Applications Information section and Figures 49a and 49b.

**Outside the ATE Test environment, R\textsubscript{EXTVCC}, if used, should not be \(\Omega\). See the Applications Information section.
### Test Circuit 3. Clock-Generator, 5V LDO and Temperature-Sensor

![Test Circuit Diagram](image)

**Decoupling Requirements**

\( T_A = 25°C \). Refer to Test Circuit 1 and Test Circuit 2.

<table>
<thead>
<tr>
<th>Application</th>
<th>Symbol</th>
<th>Parameter</th>
<th>Conditions</th>
<th>Min</th>
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<th>Max</th>
<th>Units</th>
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<tbody>
<tr>
<td>Positive-V(_{OUT}) Operation</td>
<td>( C_{INHn}, C_{Dn} )</td>
<td>External High Frequency Input Capacitor Requirement</td>
<td>( I_{OUT^+} = 4A )</td>
<td>9.4</td>
<td>( \mu F )</td>
<td></td>
<td></td>
</tr>
<tr>
<td></td>
<td>( C_{OUTHn} )</td>
<td>External High Frequency Output Capacitor Requirement</td>
<td>( I_{OUT^+} = 4A )</td>
<td>22</td>
<td>( \mu F )</td>
<td></td>
<td></td>
</tr>
<tr>
<td>Negative-V(_{OUT^-}) Operation</td>
<td>( C_{INHn}, C_{Dn} )</td>
<td>External High Frequency Input Capacitor Requirement</td>
<td>( I_{OUT^-} = 2A )</td>
<td>9.4</td>
<td>( \mu F )</td>
<td></td>
<td></td>
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<tr>
<td>(Inverting Output Buck-Boost)</td>
<td></td>
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<tr>
<td>(Test Circuit 2)</td>
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</tr>
<tr>
<td></td>
<td>( C_{OUTHn} )</td>
<td>External High Frequency Output Capacitor Requirement</td>
<td>( I_{OUT^-} = 2A )</td>
<td>22</td>
<td>( \mu F )</td>
<td></td>
<td></td>
</tr>
</tbody>
</table>

**Notes:**
- PINS NOT SHOWN AND NOT TESTED IN THIS TEST CIRCUIT.
- V\(_{IN1}\), SV\(_{IN1}\), V\(_{DIN1}\), RUN\(_{IN}\), V\(_{OUT^+}\),
- V\(_{OSNS^+}\), V\(_{OUT^-}\), SV\(_{OUT^-}\), CLK\(_{IN1}\),
- INTV\(_{CC}\), EXT\(_{CC}\), V\(_{INREG}\), COMP\(_{a}\),
- COMP\(_{b}\), f\(_{SET}\), I\(_{SET}\), f\(_{MON}\), IM\(_{MON}\),
- IM\(_{DFB}\), PG\(_{GOOD}\), NC

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LTM4655

OPERATION

Power Module Overview

The LTM4655 is a dual-channel non-isolated switch mode DC/DC power supply. Each channel is fully independent of the other. Each output can be configured for positive or negative polarity. A channel configured for positive-VOUT operation performs step-down DC/DC conversion and regulates a positive output voltage, VOUT+n. A channel configured for negative-VOUT operation performs two-switch buck-boost DC/DC conversion and regulates a negative output voltage, VOUT−n (this topology is also known as a ground-referred buck converter).

An integrated LDO provides up to 25mA of output current at +5V (LDOOUT) with respect to GND. This LDO powers an internal 2-phase clock oscillator, yielding flexibility to operate the switching channels 180° out-of-phase from each other.

A channel in positive-VOUT configuration (see Test Circuit 1) can deliver up to 4A output current with a few external input and output capacitors. Set by a single resistor, RİSETn, an LTM4655 channel regulates a positive output voltage, VOUT+n can be set to as low as 0.5V to as high as 26.5V of VINn. Channels in this positive-VOUT configuration can operate from a positive input supply rail, VINn, between 3.1V and 40V. The typical application schematic is shown in Figure 45.

A channel in negative-VOUT configuration (see Test Circuit 2) can deliver up to 4A output current with a few external input and output capacitors. The output current capability of the LTM4655 channel in this configuration is dependent on its VINn and VOUTn, as indicated in Figure 6. Set by a single resistor, RİSETn, the LTM4655 channel regulates a negative output voltage, VOUT−n. VOUT−n can be set to as low as −26.5V to as high as −0.5V. In this negative-VOUT configuration, an LTM4655 channel can operate from a positive input supply rail, VINn, between 3.6V and 40V. The LTM4655 channel’s safe operating area is defined by: VINn + |VOUT−n| ≤ 40V. The typical application schematic is shown in Figure 48. Though an LTM4655 channel configured to regulate VOUT−n is a ground-referred buck topology, built-in level-shift circuitry on the RUNn, CLKInn, and PGOODn pins result in these pins being conveniently referred to GND (not SVOUT−n).

Each channel of the LTM4655 contains an independent, integrated constant-frequency current mode regulator, power MOSFETs, power inductor, EMI filter and other supporting discrete components. The nominal switching frequency range is from 400kHz to 3MHz, and the default operating frequency is 400kHz. Each channel can optionally be synchronized to its built-in clock oscillator CLKOUTn pins or to an externally applied clock, from 250kHz to 3MHz. See the Applications Information section. Each channel of the LTM4655 supports internal and external control loop compensation. Internal loop compensation is selected by connecting the COMPna and COMPnb pins. Using internal loop compensation, the LTM4655 has sufficient stability margins and good transient performance with a wide range of output capacitors—even ceramic-only output capacitors. For external loop compensation, see the Applications Information section. LTPowerCAD® is available for transient load step and stability analysis. Input filter and noise cancellation circuitry reduces noise-coupling to the module’s inputs and outputs, ensuring the module’s electromagnetic interference (EMI) meets the limits of EN55022 Class B (see Figure 7 through Figure 9).

Pulling the RUNn pin below 1.2V (with respect to GND) forces the corresponding LTM4655 channel into a shutdown state. A capacitor can be applied from ISETna to SVOUTn− to program the output voltage ramp rate; or, the default LTM4655 ramp rate can be set by connecting ISETna to ISETnb; or, voltage tracking can be implemented by interfacing rail voltages to the ISETna pin. See the Applications Information section.

Multiphase operation can be employed by connecting the CLKOUTn pins to their respective CLKInn pins—or, by connecting an external clock source to the LTM4655’s CLKInn pins. See the Typical Applications section.

LDO losses within the module incurred primarily due to MOSFET driver power are optionally reduced by connecting EXTVCCn to VOUT+n through an RC filter or by connecting EXTVCCn to a suitable voltage source.

For channels configured for positive-VOUT operation, the IMONn pin is an analog output current indicator that sources a current proportional to its channel’s load current. (For channels configured for negative-VOUT− operation, the
IMON\textsubscript{na} pin does not support such a feature and must be connected to V\textsubscript{OUT\textsubscript{na}}. When IMON\textsubscript{na} is electrically connected to IMON\textsubscript{nb}, the voltage on the IMON\textsubscript{na}/IMON\textsubscript{nb} node is proportional to load current—with 1V corresponding to 4A load. If desired, IMON\textsubscript{na} can be interfaced to an external parallel RC network instead of the one provided by IMON\textsubscript{nb}. If IMON\textsubscript{na} ever exceeds 2V, a servo loop reduces the LTM4655’s output current in order to keep IMON\textsubscript{na} at or below 2V. Through this servo mechanism, a parallel RC network can be connected to IMON\textsubscript{na} to implement an average current limit function—if desired. When the feature is not needed, connect IMON\textsubscript{na} to V\textsubscript{OUT\textsubscript{na}}.

The LTM4655 features an additional control pin called VINREG\textsubscript{n}, which has a 2V servo threshold. This pin can be used to as an extra control pin, e.g., to reduce channel input current draw during input line sag (“brownout”) conditions. Connect VINREG\textsubscript{n} to INTVCC\textsubscript{n} when this feature is not needed.

TEMP\textsuperscript{+} and TEMP\textsuperscript{−} pins give access to a diode-connected PNP transistor, making it possible to monitor the LTM4655’s internal temperature—if desired.

External component selection is primarily determined by the maximum load current and output voltage. Refer to Table 11 and Table 12 and the Test Circuits for recommended external component values.

**V\textsubscript{IN} to V\textsubscript{OUT} Conversion Ratios**

There are restrictions on the V\textsubscript{IN} to V\textsubscript{OUT} conversion ratios that the LTM4655 can achieve. The maximum duty cycle of the LTM4655 is 96% typical. The V\textsubscript{IN} to V\textsubscript{OUT} minimum dropout voltage is a function of load current when operating in high duty cycle applications. As an example, \(V_{\text{OUT}(24\text{VDC})}\) from the Electrical Characteristics table highlights the LTM4655’s ability to regulate 24V\textsubscript{OUT} at up to 4A from 29V\textsubscript{IN}, when running at a switching frequency, \(f_{\text{SW}}\), of 1.5MHz.

At very low duty cycles, the LTM4655’s on-time of \(M_{Tn}\) each switching cycle should be designed to exceed the LTM4655 control loop’s specified minimum on-time of 60ns, \(T_{\text{ON(MIN)n}}\) (guardband to 90ns) see Equation 4.

\[
\frac{D_n}{f_{\text{SWn}}} > T_{\text{ON(MIN)n}}
\] (4)

where \(D_n\) (unitless) is the duty-cycle of \(M_{Tn}\), given by Equation 5:

\[
D_n = \frac{V_{\text{OUTn+}} - V_{\text{OUTn-}}}{V_{\text{INn}} - V_{\text{OUTn-}}}
\] (5)

In rare cases where the minimum on-time restriction is violated, the channel \(n\) frequency of the LTM4655 automatically and gradually folds back down to approximately one-fifth of its programmed switching frequency to allow V\textsubscript{OUT} to remain in regulation. See the Frequency Adjustment section. Be reminded of Notes 2 and 3 in the Electrical Characteristics section regarding output current guidelines.

**Input Capacitors, Positive-V\textsubscript{OUT} Operation**

The LTM4655 achieves low input conducted EMI noise due to tight layout and high frequency bypassing of MOSFETs \(M_{Tn}\) and \(M_{Bn}\) within the module itself. A small filter inductor (400nH) is integrated in the input line (from V\textsubscript{INn} to V\textsubscript{Dn}), providing further noise attenuation—again, local to the switching MOSFETs. The V\textsubscript{Dn} and V\textsubscript{INn} pins are available for external input capacitors—\(C_{\text{Dn}}\) and \(C_{\text{INHn}}\)—to form a high-frequency π filter. As shown in the Simplified Block Diagram, the ceramic capacitor \(C_{\text{Dn}}\) on the LTM4655’s V\textsubscript{Dn} pins handles the majority of the RMS current into the DC/DC converter power stage and requires careful selection, for that reason.

See Figure 7 through Figure 9 for demonstration of LTM4655’s EMI performance, meeting the radiated emissions requirements of EN55022B.

The input capacitance, \(C_{\text{Dn}}\), is needed to filter the pulsed current drawn by \(M_{Tn}\). To prevent excessive voltage sag on V\textsubscript{Dn}, a low-effective series resistance (low-ESR, such as an X7R ceramic) input capacitor should be used, sized appropriately for the maximum \(C_{\text{Dn}}\) RMS ripple current (Equation 6)

\[
I_{\text{CDn(RMS)}} = \frac{I_{\text{OUTn(MAX)}}}{\eta_n \%} \cdot \sqrt{D_n \cdot (1-D_n)}
\] (6)

where \(\eta_n \%\) is the estimated efficiency of the channel \(n\) power module. (See Typical Performance Characteristics graphs.)
Several capacitors may be paralleled to meet the application's target size, height, and $C_{DN}$ RMS ripple current rating. For lower input voltage applications, sufficient bulk input capacitance is needed to counteract line sag and transient effects during output load changes. The bulk capacitor can be a switcher-rated aluminum electrolytic capacitor or a Polymer capacitor. Suggested values for $C_{DN}$ and $C_{INHn}$ are found in Table 11.

A final precaution regarding ceramic capacitors concerns the maximum input voltage rating of the LTM4655’s $V_{INn}$, $SV_{IN}$, and $VDn$ pins. A ceramic input capacitor combined with trace or cable inductance forms a high Q (under-damped) tank circuit. If the LTM4655 circuit is plugged into a live supply, the input voltage can ring to twice its nominal value, possibly exceeding the device’s rating. This situation is easily avoided; see the Hot Plugging Safety section.

**Output Capacitors, Positive-V\textsubscript{OUT} Operation**

Output capacitors $C_{OUTHn}$ and $C_{OUTLn}$ are applied across the LTM4655’s $V_{OUTn}^+/V_{OUTn}^-$ power output pins. Sufficient capacitance and low ESR are called for, to meet the output voltage ripple, loop stability, and transient requirements. $C_{OUTLn}$ can be a low ESR tantalum or polymer capacitor. $C_{OUTHn}$ is a ceramic capacitor. The typical output capacitance is 22μF (type X5R material, or better), if ceramic-only output capacitors are used.

Table 11 shows a matrix of suggested output capacitors optimized for 2A transient step-loads applied at 2A/μs. Additional output filtering may be required by the system designer, if further reduction of output ripple or dynamic transient spike is required. The LTpowerCAD design tool is available for transient and stability analysis. Stability criteria are considered in the Table 11 matrix, and LTpowerCAD is available for stability analysis. Multiphase operation will reduce effective output ripple as a function of the number of phases. Application Note 77 discusses this noise reduction versus output ripple current cancellation, but the output capacitance should be considered carefully as a function of stability and transient response. LTpowerCAD can be used to calculate the output ripple reduction as the number of implemented phases increases by N times.

External loop compensation can be applied from COMPna to $SV_{OUTn}^-$, if needed, for transient response optimization.

**Forced Continuous Operation**

Leave the CLKIN\textsubscript{n} pin open circuit to command channel \textit{n} of the LTM4655 for forced continuous operation. In this mode, the control loop is allowed to command the inductor peak current to approximately –1A, allowing for significant negative average current. Clocking the CLKIN\textsubscript{n} pin at a frequency within ±40% of the target switching frequency commanded by the $f_{SETn}$ pin synchronizes $M_{Trn}$’s turn-on to the rising edge of the CLKin\textsubscript{n} pin.

**Output Voltage Programming, Tracking and Soft-Start**

The LTM4655 regulates its output voltage, $V_{OUTn}^+ - V_{OUTn}^-$, according to the differential voltage present from $ISET\textsubscript{n}$ to $SV_{OUT}^-$. In most applications, the output voltage is set by simply connecting a resistor, $R_{ISETn}$, from $ISET\textsubscript{n}$ to $SV_{OUT}^-$, according to Equation 7.

$$R_{ISETn} = \frac{V_{OUTn}^+ - V_{OUTn}^-}{50\mu A} \quad (7)$$

Since the LTM4655 control loop servos its output voltage according to the voltage between $ISET\textsubscript{n}$ and $SV_{OUT}^-$: placing a capacitor, $CSSn$, parallel to $R_{ISETn}$ configures the ramp-up rate of $ISET\textsubscript{n}$ and thus the output. In the time domain, the output voltage ramp-up after the RUN\textsubscript{n} pin is toggled from low to high (t = 0s) is given by Equation 8.

$$V_{OUTn}(t)^+ V_{OUTn}(t)^- = I_{SETna} \cdot R_{ISETn} \cdot \left(1 - e^{-\frac{t}{R_{ISETn} \cdot CSSn}}\right) \quad (8)$$

The soft-start time, $t_{SS}$, is defined as the time it takes for channel \textit{n}’s output voltage to ramp from 0V to 90% of its final value (Equation 9 or Equation 10)

$$t_{SSn} = -R_{ISETn} \cdot CSSn \cdot \ln (1 - 0.9) \quad (9)$$

or

$$t_{SSn} = 2.3 \cdot R_{ISETn} \cdot CSSn \quad (10)$$
A default value of $C_{SSn} = 1.5\,\text{nF}$ can be implemented by connecting ISET$n$ to ISET$n\!\!b$. For other ramp-up rates, connect an external $C_{SS}$ capacitor parallel to R$ISET$.

When starting up into a pre-biased $V_{OUT}$, the LTM4655 stays in a sleep mode, keeping $M_Tn$ and $M_Bn$ off until $V_{ISETn}$ equals $V_{OSNSn}$—after which, the DC/DC converter commences switching action and $V_{OUT}$ is ramped according to the voltage commanded by ISET$n$.

Since the LTM4655 control loop servos its $V_{OSNSn}$ voltage to match that of ISET$n$’s, the LTM4655’s channel $n$ output can be configured to track any voltage applied to ISET$n$, referenced to $SV_{OUTn}$–. See Figure 52 for an example of the LTM4655 configured as a DAC-controlled bipolar-output programmable power supply.

The LTM4655 can track the mirror-image of a positive rail to generate the negative half of a split-supply, as seen in Figure 50 (note the use of $R_{TRACK}$ and $R_{ISET2} = R_{ISET1} \parallel R_{TRACK}$).

**Frequency Adjustment**

The default switching frequency ($f_{SWn}$) of channel $n$ of the LTM4655 is 400kHz. This is suitable for low-$V_{IN}$ ($V_{INn} \leq 5\,\text{V}$) applications and low-$V_{OUT}$ ($V_{OUTn}^+ - V_{OUTn}^- \leq 3.3\,\text{V}$) applications. For a practical design, the LTM4655’s inductor ripple current ($\Delta I_{PK-PK}$) is suggested to be less than $\sim 2\,\text{A}_{PK-PK}$. Choose $f_{SWn}$ according to Equation 11.

$$f_{SWn} = \frac{V_{OUTn}^+ - V_{OUTn}^- \cdot (1-D_n)}{L_n \cdot \Delta I_{PK-PK}}$$  \hspace{1cm} (11)

where the value of LTM4655’s power inductor, $L_n$, is $4\,\mu\text{H}$.

To avoid cycle-skipping, impose restrictions on $f_{SWn}$ to ensure minimum on-time criteria is met (Equation 12).

$$f_{SWn} < \frac{D_n}{t_{ONn}(MIN)}$$  \hspace{1cm} (12)

The LTM4655’s minimum on-time, $t_{ONn}(MIN)$, is specified as 60ns. For a practical design, it is recommended to guardband to 90ns.

To configure channel $n$ of the LTM4655 for a higher switching frequency than its default of 400kHz, apply a resistor, $R_{ISETn}$, between the f$SETn$ pin and $SV_{OUTn}$+. $R_{ISETn}$ is given (in $\text{M}\Omega$) by Equation 13.

$$R_{ISETn}(\text{M}\Omega) = \frac{1}{10\,\text{pF} \cdot [f_{SWn}(\text{MHz}) - 0.4(\text{MHz})]}$$  \hspace{1cm} (13)

The relationship of $R_{ISETn}$ to programmed $f_{SWn}$ is shown in Figure 1. See Table 11 and Table 12 for recommended $f_{SWn}$ and corresponding $R_{ISETn}$ values for various combinations of $V_{INn}$, $V_{OUTn}^+$ and $V_{OUTn}^-$.
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Power Module Protection

The LTM4655’s current mode control architecture provides fast cycle-by-cycle current limit in an overcurrent condition, as shown in the Typical Performance Characteristics section. If the output voltage collapses sufficiently due to an overload or short-circuit condition, minimum on-time will be violated and the internal oscillator will then fold-back automatically to one-fifth of the LTM4655’s programmed switching frequency—thereby reducing the output current and affording the load a chance to recover.

The LTM4655 ceases channel $n$ switching action if the channel’s internal temperatures exceed 165°C. The channel’s control IC resumes operation after a 10°C cool-down hysteresis. Note that these typical parameters are based on measurements in a lab oven and are not production tested. This overtemperature protection is intended to protect the device during momentary overload conditions. The maximum rated junction temperature will be exceeded when this overtemperature protection is active. Continuous operation above the specified absolute maximum operating junction temperature may impair device reliability or permanently damage the device. See Note 1 of the Electrical Characteristics table.

The LTM4655 does not feature any specialized output overvoltage protection beyond what is inherent to the control loop’s servo mechanism.

RUN Pin Enable

The RUN$n$ pin is used to enable the power module or sequence the power module. The threshold is 1.2V. The RUN$n$ pin can be used to provide an undervoltage lockout (UVLO) function by connecting a resistor divider from the input supply to the RUN$n$ pin, as shown in Figure 2. Undervoltage lockout keeps channel $n$ of the LTM4655 in shutdown until the supply input voltage is above a certain voltage programmed by the user. The RUN$n$ pin hysteresis voltage prevents noise from falsely tripping UVLO. Resistors are chosen by first selecting $R_{BN}$ (refer to Figure 2 and Equation 14). Then:

$$R_{An} = R_{Bn} \cdot \left( \frac{V_{IN(n)(ON)}}{1.2V} - 1 \right)$$  \hspace{1cm} (14)

where $V_{IN(n)(ON)}$ is the input voltage at which the undervoltage lockout is overcome and the supply turns on. The $V_{IN(n)}$ turn-off voltage, $V_{IN(n)(OFF)}$ is given by Equation 15.

$$V_{IN(n)(OFF)} = 1.07V \cdot \left( R_{An} + 1 \right)$$  \hspace{1cm} (15)

If UVLO is not needed, RUN$n$ can be connected to LTM4655’s LDOOUT pin.

When RUN$n$ is below its threshold, UVLO of channel $n$ is engaged, $M_{Tn}$ and $M_{Bn}$ are turned off, INTVCC$n$ ceases to be regulated, and ISET$n$ is discharged to SVOUT$n$– by internal circuitry.

Loop Compensation

External loop compensation may be preferred for some applications and can be implemented easily, as follows: leave COMP$n$ open circuit; connect a series-RC network $R_{THn}$ and $C_{THn}$ from COMP$n$ to SVOUT$n$–; in some instances, connect a capacitor ($C_{THPn}$) from COMP$n$ to SVOUT$n$– (paralleling the $R_{THn}$–$C_{THn}$ series-RC network). See Table 10 for suggested input and output capacitances for a variety of operating conditions. Additionally, the LTpowerCAD design tool is available for transient and stability analysis.
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Hot Plugging Safely

The small size, robustness and low impedance of ceramic capacitors make them an attractive option for the input bypass capacitors ($C_{Di}$ and $C_{INH}$) of the LTM4655. However, these capacitors can cause problems if the LTM4655 is plugged into a live supply (see Analog Devices Application Note 88 for a complete discussion). The low loss ceramic capacitor combined with stray inductance in series with the power source forms an under damped tank circuit, and the voltage at the $V_{IN}$ pin of the LTM4655 can ring to twice the nominal input voltage, possibly exceeding the LTM4655’s rating and damaging the part. If the input supply is poorly controlled or the user will be plugging the LTM4655 into an energized supply, the input network should be designed to prevent this overshoot by introducing a damping element into the path of current flow. This is often done by adding an inexpensive electrolytic bulk capacitor ($C_{INL}$) across the input terminals of the LTM4655. The selection criteria for $C_{INL}$ calls for: an ESR high enough to damp the ringing; a capacitance value several times larger than $C_{INH}$; a suitable ripple current rating. $C_{INL}$ does not need to be located physically close to the LTM4655; it should be located close to the application board’s input connector, instead.

Input Disconnect/Input Short Considerations

If at any point the input supply is removed with the output voltage still held high through its capacitor, power will be drawn from the output capacitor to power the module, until the output voltage drops below the minimum $SV_{IN}$ requirements of the module.

However, if the $SV_{IN}$ pins are grounded while the output is held high, regardless of the RUN pin state, parasitic body diodes inside the LTM4655 will pull current from the output through the $V_{OUT}$ pins. Depending on the size of the output capacitor and the resistivity of the short, high currents may flow through the internal body diode, and cause damage to the part. If discharge of $SV_{IN}$ by the input source is possible, preventative measures should be taken to prevent current flow through the internal body diode. Simple solutions would be placing a Schottky diode in series with the supply (Figure 3), or placing a Schottky diode from $V_{OUT}$ to $SV_{IN}$ (Figure 4). Applications with loads that experience large load-step release, load dump or other mechanisms that invoke reverse energy flow in the Figure 3 circuit may need a suitably-rated Zener diode protection clamp, to limit the resulting transient voltage rise on $SV_{IN}$ and $C_{INH}$.

![Figure 3. Schottky Diode in Series with the Supply](image)

![Figure 4. Schottky Diode from $V_{OUT}$ to $SV_{IN}$](image)

### $INTV_{CCn}$ and $EXTV_{CCn}$ Connection

When RUN is logic high, an internal low dropout regulator regulates an internal supply, $INTV_{CCn}$, that powers the control circuitry for driving LTM4655’s channel $n$ internal MOSFETs. $INTV_{CCn}$ is regulated at 3.3V. In this manner, the LTM4655’s $INTV_{CCn}$ is directly powered from $SV_{IN}$ by default. The gate driver current through the $INTV_{CCn}$ LDO is about 20mA for a typical 1MHz application. The internal LDO power dissipation can be calculated as shown in Equation 16.

$$P_{LDO\_LOSS}(INTVCC) = 20mA \times (SV_{IN}^- - V_{OUT}^- - 3V) \quad (16)$$

The LDO draws current off of $EXTV_{CCn}$ instead of $SV_{IN}$ when $EXTV_{CCn} - V_{OUT}$ exceeds 3.2V and $SV_{IN} - V_{OUT}$ exceeds 5V. For output voltages of 4V and higher, $EXTV_{CCn}$

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can be connected to $V_{OUT}^+$ through an RC-filter. When the internal LDO derives power from EXTVCC instead of $SV_{IN}$, the internal LDO power dissipation is shown in Equation 17.

$$P_{LDO\_LOSS_{n(EXTVCC)}} = 20mA \cdot (V_{OUT} - V_{OUT}^+ - 3V)$$  \hspace{1cm} (17)

The recommended value of the resistor between $V_{OUT}^+$ and EXTVCC is roughly $(V_{OUT}^+ - V_{OUT}^+)^{-} \cdot 4\Omega/V$. This resistor, $R_{\text{EXTVCC}}$, must be rated to continually dissipate $(0.02A)^2 \cdot R_{\text{EXTVCC}}$. The primary purpose of this resistor is to prevent EXTVCC overstress under a fault condition. For example, when an inductive short-circuit is applied to the module’s output, $V_{OUT}^+$ may be briefly dragged below $V_{OUT}^-$—forward biasing the $V_{OUT}^-$-to-EXTVC body diode. This resistor limits the magnitude of current flow in EXTVCC. If the application requires a low resistive path to EXTVCC, apply a protective Schottky diode across EXTVCC and $V_{OUT}^-$. See Figure 52. Bypass EXTVCC to $V_{OUT}^-$ with 1µF of X5R (or better) MLCC.

**Multiphase Operation**

Multiple LTM4655 channels and modules can be paralleled for higher output current applications. For lowest input and output voltage and current ripples, it is advisable to synchronize paralleled LTM4655s to a clock (within ±40% of the target switching frequency set by $f_{\text{SET}}^n$.

LTM4655 channels and modules can be paralleled without synchronizing circuits: just be aware that some beat-frequency ripple will be present in the output voltage and reflected input current by virtue of the fact that such modules are not operating at identical, synchronized switching frequencies.

The LTM4655 device is an inherently current mode controlled device, so parallel channels and modules will have good current sharing as shown in Figure 45 and Figure 47.

To parallel LTM4655 channels and/or modules, connect the respective COMPna, ISETna, and $V_{\text{OSNS}n}$ pins of each LTM4655 together to share the current evenly. In addition, tie the respective RUNna pins of paralleled LTM4655 channels and/or modules together, to ensure proper start-up and shutdown behavior.

Note that for parallel applications, $V_{OUT}$ can be set by a single, common resistor on the ISETna net (see Equation 18).

$$R_{\text{ISET}^n} = \frac{V_{OUT}^+ - V_{OUT}^-}{50\mu A \cdot N}$$  \hspace{1cm} (18)

where $N$ is the number of LTM4655 channels in parallel configuration.

Depending on the duty cycle of operation, the output voltage ripple achieved by paralleled, synchronized LTM4655 modules may be considerably smaller than what is yielded by a single-phase solution. Application Note 77 provides a detailed explanation of multiphase operation (relevant to parallel LTM4655 applications) pertaining to noise reduction and output and input ripple current cancellation. Regardless of ripple current cancellation, it remains important for the output capacitance of paralleled LTM4655 applications to be designed for loop stability and transient response. LTpowerCAD is available for such analysis.

Figure 5 illustrates the RMS ripple current reduction as a function of the number of interleaved (parallelized and synchronized) LTM4655 modules—derived from Application Note 77.
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Negative Output Current Capability Varies as a Function of $V_{INn}$ to $V_{OUTn}$ Conversion Ratios, Negative-$V_{OUT}$ Operation

In negative-$V_{OUT}$ operation, the output current capability of the LTM4655 has a strong dependency on the operating input ($V_{INn}$) and output ($V_{OUTn}$) voltages. See Figure 6.

![Figure 6. Channel Output Current Capability*, Negative-$V_{OUT}$ Operation](image)

*Current limit frequency-foldback activates at load currents higher than indicated curves. Continuous channel output current capability subject to details of application implementation. Switching frequency set per Table 1. See Notes 2 and 3.

The reason for this is inherent in the two-switch buck-boost topology employed by the LTM4655 when so-configured for negative-$V_{OUT}$ operation. To protect the primary power MOSFET ($M_{Tn}$) from overstress (see Simplified Block Diagram), its peak current ($I_{nPK}$) is limited by control circuitry to 6A. When $M_{Tn}$ is on, observe that no current flows to LTM4655’s output; furthermore, observe that only when $M_{Tn}$ is off does current flow to the output of the LTM4655. As a consequence of this arrangement: for a given output voltage, current limit inception activates sooner at low line (higher, larger duty cycle) than at high line (lower, smaller duty cycle). A further consequence is: for a given input voltage, the output power capability of the LTM4655 is higher for lower-magnitude $V_{OUTn}$ (lower, smaller duty cycle) than for higher-magnitude $V_{OUTn}$ (higher, larger duty cycle). The combination of these effects is shown the plots in Figure 6 and described by Equation 19.

$$I_{OUTn(CAPABILITY)} = \frac{V_{INn} \cdot (I_{nPK} - \frac{\Delta I_{nPK-PK}}{2}) \cdot \eta_n}{V_{INn} - V_{OUTn}}$$  \hspace{1em} (19)$$

where:

$\Delta I_{nPK-PK}$ is the channel $n$ inductor ripple current, in amps, and $\eta_n$ (unitless) is the channel efficiency of the LTM4655.

For completeness, $\Delta I_{nPK-PK}$ is given by Equation 20.

$$\Delta I_{nPK-PK} = \frac{1}{L_n \cdot f_{SWn} \cdot \left(\frac{1}{V_{INn}} - \frac{1}{V_{OUTn}}\right)}$$  \hspace{1em} (20)$$

where:

$L_n$ is 4μH, the LTM4655 channel’s power inductor value, and $f_{SWn}$ is the switching frequency of the LTM4655’s channel, in MHz.

For a practical design, $\Delta I_{nPK-PK}$ is designed to be less than $\sim 2A_{PK-PK}$.

For a practical design, the LTM4655’s on-time of $M_{Tn}$ each switching cycle should be designed to exceed the LTM4655 control loop’s specified minimum on-time of 60ns, $t_{ON(MIN)}$, (guardband to 90ns). For example, Equation 21.

$$D_n \cdot f_{SWn} > t_{ON(MIN)}$$  \hspace{1em} (21)$$

where $D_n$ (unitless) is the duty-cycle of $M_{Tn}$, given by Equation 22.

$$D = \frac{V_{OUTn^+} - V_{OUTn^-}}{V_{INn} - V_{OUTn}}$$  \hspace{1em} (22)$$

Combining Equation 22 with Equation 19, it can be illustrative to see Equation 23.

$$I_{OUTn(CAPABILITY)} = (1 - D_n) \cdot (I_{nPK} - \frac{\Delta I_{nPK-PK}}{2}) \cdot \eta_n$$  \hspace{1em} (23)$$
In rare cases where the minimum on-time restriction is violated, the frequency of the affected LTM4655 channel(s) automatically and gradually folds back down to one-fifth of its programmed switching frequency to allow $V_{OUTn}$ to remain in regulation.

Be reminded of Notes 2, and 3 in the Electrical Characteristics section regarding output current guidelines.

### Input Capacitors, Negative-$V_{OUT}$ Operation

The LTM4655 achieves low input conducted EMI noise due to tight layout and high-frequency bypassing of MOSFETs $M_{Tn}$ and $M_{Bn}$ within the module itself. A small filter inductor (400nH) is integrated in the input line (from $V_{INn}$ to $V_{DN}$) provides further noise attenuation—again, local to the switching MOSFETs. The $V_{DN}$ and $V_{INn}$ pins are available for external input capacitors—$C_{Dn}$ and $C_{INHn}$—to form a high-frequency π filter. As shown in the Simplified Block Diagram, the ceramic capacitor $C_{Dn}$ on the LTM4655’s $V_{DN}$ pins handles the majority of the RMS current into the DC/DC converter power stage and requires careful selection, for that reason.

To meet the radiated emissions requirements of EN55022B, an additional filter capacitor, $C_{INOUTn}$, is needed—connecting from $V_{INn}$ to $V_{OUTn}$—. See Figure 7 through Figure 9 for EMI performance.

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**Figure 7.** Radiated Emissions Scan of the LTM4655. Producing $24V_{OUT}$ at 7A, from 36$V_{IN}$. DC2898A Hardware. $f_{SW}$ = 1.2MHz. Measured in a 10m Chamber. Peak Detect Method

**Figure 8.** Radiated Emissions Scan of the LTM4655. Producing $-24V_{OUT}$ at 2A, from 12$V_{IN}$. DC2899A Hardware. $f_{SW}$ = 1.2MHz. Measured in a 10m Chamber. Peak Detect Method

**Figure 9.** Radiated Emissions Scan of the LTM4655. Producing $-12V_{OUT}$ at 4A, from 12$V_{IN}$. DC2899A Hardware. $f_{SW}$ = 700kHz. Measured in a 10m Chamber. Peak Detect Method
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The input capacitance, $C_{Di}$, is needed to filter the pulsed current drawn by $M_{Tri}$. To prevent excessive voltage sag on $V_{Di}$, a low-effective series resistance (low-ESR) input capacitor should be used, sized appropriately for the maximum $C_{Di}$ RMS ripple current (see Equation 24).

$$I_{CDn(RMS)} = I_{PK} \cdot \sqrt{D_n \cdot (1-D_n)}$$

(24)

$I_{CDn(RMS)}$ is maximum for $D_n = 1/2$. For $D_n = 1/2$, $I_{CDn(RMS)} = 1/2 \cdot I_{PK}$ or 3A. This simplification of the worst-case condition is commonly used for design purposes because even significant deviations in $D_n$ do not offer much relief in practice. Furthermore: note that ripple current ratings from capacitor manufacturers are often based on 2000 hours of life; therefore, it is advisable to significantly over-design $C_{Di}$, and/or choose a capacitor rated at a higher temperature than required. Err on the side of caution and contact the capacitor manufacturer to understand the capacitor vendor’s derating methodology.

Several capacitors may be paralleled to meet the application’s target size, height, and $C_{Di}$ RMS ripple current rating. For lower input voltage applications, sufficient bulk input capacitance is needed for $C_{INLn}$ to counteract line sag and transient effects during output load changes. Suggested values for $C_{Di}$ and $C_{INHn}$ are found in Table 12. Take note that $C_{Di}$ is connected from $V_{Di}$ to $V_{OUT^-}$, whereas $C_{INHn}$ and $C_{INLn}$ are connected from $V_{INn}$ to power ground; this is deliberate.

A final precaution regarding ceramic capacitors concerns the maximum input voltage rating of the LTM4655’s $V_{INn}$, $SV_{INn}$, and $V_{Di}$ pins. A ceramic input capacitor combined with trace or cable inductance forms a high Q (under-damped) tank circuit. If the LTM4655 circuit is plugged into a live supply, the input voltage can ring to twice its nominal value, possibly exceeding the device’s rating. This situation is easily avoided; see the Hot Plugging Safely section.

Output Capacitors, Negative-$V_{OUT^-}$ Operation

Output capacitors $C_{OUTn}$ and $C_{OUTL}$ are applied across the LTM4655’s $V_{OUT^-}/V_{OUT^-}$ power output pins: sufficient capacitance and low ESR are called for, to meet the output voltage ripple, loop stability, and transient requirements. $C_{OUTL}$ can be a low ESR tantalum or polymer capacitor. $C_{OUTn}$ is a ceramic capacitor. The typical output capacitance is 22μF (type X5R material, or better), if ceramic-only output capacitors are used.

For highest reliability designs, polarized output capacitors ($C_{OUTL}$) are not recommended, as there is a possibility of a diode-drop of reverse voltage appearing transiently on $V_{OUT^-}$ during rapid application of input voltage or when $RUNn$ is toggled logic high (see Figure 49). When polarized capacitors are used on $V_{OUT^-}$, contact the capacitor vendor to understand what reverse voltage their polarized capacitor can withstand. Be advised, polarized capacitor reverse voltage rating is sometimes temperature-dependent.

Output voltage ripple ($\Delta V_{OUTn(PK-PK)}$) is governed by charge lost in $C_{OUTn}$ and $C_{OUTL}$ while $M_{Tri}$ is on, in addition to the contribution of a resistive drop across the ESR of the output capacitors. This is expressed by Equation 25.

$$\Delta V_{OUTn(PK-PK)} = \frac{I_{LOADn} \cdot D}{C_{OUTn} \cdot f_{SWn}} + \frac{I_{LOADn} \cdot ESR_n}{D_n}$$

(25)

Table 12 shows a matrix of suggested output capacitors optimized for transient step-loads that are 50% of the full load capability for that combination of $V_{INn}$, $V_{OUT^-}$, and $f_{SW}$. The table optimizes total equivalent ESR and total bulk capacitance to yield the stated transient-load performance. Additional output filtering may be required by the system designer, if further reduction of output ripple or dynamic transient spike is required. The LTPowerCAD design tool is available for transient and stability analysis.

Optional Diodes to Guard Against Overstress, Negative-$V_{OUT^-}$ Operation

Just prior to output voltage start-up, a mechanism exists whereby a diode-drop of reverse polarity can appear on $V_{OUT^-}$. See the Simplified Block Diagram and observe: just prior to output voltage start-up, $SV_{INn}$ bias current ($I_{SVINn}$) flows through the module’s control IC, to $SV_{OUT^-}$; from there, the bias current (now $I_{SVOUT^-}$) flows into $V_{OUT^-}$ and through $MBn$’s body diode, to $SWn$. This current (now $I_{LE}$) continues to flow—though the 4μH power inductor—to $V_{OUT^-}$ and thus ground, closing the control IC bias circuit’s path. It is this current through $MBn$’s
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A diode that creates a diode-drop of reverse polarity (positive voltage) on \( V_{OUT}^- \), as shown in Figure 49. The voltage excursion is highest when \( RUNn \) toggles high because that is the instant when \( INTVCC \) powers-up, with a corresponding increase in \( I_{SVINn}/I_{SVOUTn}^-/I_{Ln} \) current flow. With higher current flow, the forward voltage drop \( (VF) \) of \( MBn \)’s body diode—and thus, the positive voltage excursion on \( V_{OUT}^- \) is higher.

If this transient voltage excursion is unwelcome for the load or polarized output capacitors, minimize it with a low \( V_F \) Schottky diode that straddles \( V_{OUT}^- \) and \( V_{OUT}^+ \) (see Figure 48 circuit and Figure 49 performance). Additionally, the voltage excursion can be empirically reduced by increasing output capacitance.

Lastly: in applications where it is anticipated that \( V_{INn} \) may be rapidly applied (e.g., <10\( \mu \)s) and \( C_{INOUTn} \) is used, the resulting capacitor-divider network formed by \( C_{INOUTn} \) and \( C_{INHn} \) may transiently drag \( V_{OUT}^- \) positive. It is recommended to apply a low \( V_F \) Schottky diode from \( V_{OUT}^- \) to \( V_{OUT}^+ \) in such applications. The reverse mechanism applies, as well: in applications where it is anticipated that \( V_{INn} \) may be rapidly discharged and \( C_{INOUTn} \) is used, the resulting capacitor-divider network formed by \( C_{INOUTn} \) and \( C_{INLn} \) may transiently drag \( V_{OUT}^- \) excessively negative. It is recommended to straddle \( V_{OUT}^- \) and \( V_{OUT}^+ \) with a TVS diode, if output voltage excursions during \( V_{INn} \)-discharge are anticipated.

Frequency Adjustment, Negative-\( V_{OUT}^- \) Operation

The default switching frequency \( (f_{SWn}) \) of channel \( n \) of the LTM4655 is 400kHz. This is suitable for mainly low-\( V_{IN} \) or low-\( V_{OUT}^- \) applications (\( V_{INn} < 5 \text{V} \) or \( |V_{OUTn}^-| < 5 \text{V} \)). For a practical design, the LTM4655’s inductor ripple current \( (Δ_{IPK–PK}) \) is suggested to be less than \( 2A_{PK–PK} \). From Equation 20, it follows that \( f_{SW} \) should be chosen such that Equation 26.

\[
f_{SWn} = \frac{1}{L_n \cdot \Delta_{IPK–PK} \cdot \left( \frac{1}{V_{INn}} - \frac{1}{V_{OUTn}^-} \right)} \tag{26}
\]

In some cases, the value of \( f_{SWn} \) yielded by Equation 26 violates the supported minimum on-time of the LTM4655 (see Equation 21). If this occurs, choose \( f_{SWn} \) instead according to Equation 12.

The primary consequence of using a lower switching frequency than that dictated by Equation 26 is that the output current capability of the LTM4655 is reduced, according to Equation 23.

To configure the channel \( n \) of the LTM4655 for a higher switching frequency than 400kHz default, apply a resistor \( R_{SETn} \) between the \( f_{SETn} \) pin and \( SV_{OUTn}^- \). \( R_{SETn} \) is given (in M\( \Omega \)) by Equation 13.

The relationship of \( R_{SETn} \) to programmed \( f_{SWn} \) is shown in Figure 1.

See Table 1 and Table 12 for Recommended \( f_{SWn} \) and associated \( R_{SETn} \) values for various combinations of \( V_{INn} \) and \( V_{OUTn}^- \).

Table 1. Recommended Channel \( n \) Switching Frequency \( (f_{SWn}) \) and \( R_{SETn} \) for Common Combinations of \( V_{INn} \) and \( V_{OUTn}^- \), Negative-\( V_{OUT}^- \) Operation

<table>
<thead>
<tr>
<th>( V_{INn} ) (V)</th>
<th>( V_{OUT}^- ) (V)</th>
<th>( f_{SWn} )</th>
<th>( R_{SETn} )</th>
</tr>
</thead>
<tbody>
<tr>
<td>3.6</td>
<td>( -0.5 )</td>
<td>400kHz, No ( R_{SETn} )</td>
<td>400kHz, No ( R_{SETn} )</td>
</tr>
<tr>
<td>5</td>
<td>( 3.3 )</td>
<td>400kHz, No ( R_{SETn} )</td>
<td>400kHz, No ( R_{SETn} )</td>
</tr>
<tr>
<td>12</td>
<td>( -5 )</td>
<td>450kHz, 2.2M( \Omega )</td>
<td>450kHz, 2.2M( \Omega )</td>
</tr>
<tr>
<td>24</td>
<td>( -12 )</td>
<td>600kHz, 499k( \Omega )</td>
<td>800kHz, 249k( \Omega )</td>
</tr>
<tr>
<td>36</td>
<td>( -15 )</td>
<td>825kHz, 237k( \Omega )</td>
<td>1.1MHz, 143k( \Omega )</td>
</tr>
<tr>
<td>50k( \Omega ), 665k( \Omega )</td>
<td>( 1.2MHz )</td>
<td>( 1.2MHz, 124k( \Omega )</td>
<td>N/A</td>
</tr>
<tr>
<td>500kHz, 1M( \Omega )</td>
<td>( N/A ) Due to SOA Criteria Violation</td>
<td></td>
<td></td>
</tr>
</tbody>
</table>

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Radiated EMI Noise

The generation of radiated EMI noise is an inherent disadvantage of switching regulators. Fast switching turn-on and turn-off of the power MOSFETs—necessary for achieving high efficiency—create high-frequency (~30MHz+) \( \Delta V/\Delta t \) changes within DC/DC converters. This activity tends to be the dominant source of high-frequency EMI radiation in such systems. The high level of device integration within LTM4655—including optimized gate-driver and critical front-end \( \pi \) filter inductor—delivers low radiated EMI noise performance. Figure 7 through Figure 9 show typical examples of LTM4655 meeting the radiated emission limits established by EN55022 Class B.

Thermal Considerations and Output Current Derating

The thermal resistances reported in the Pin Configuration section are consistent with those parameters defined by JESD51-12 and are intended for use with finite element analysis (FEA) software modeling tools that leverage the outcome of thermal modeling, simulation, and correlation to hardware evaluation performed on a µModule package mounted to a hardware test board. The motivation for providing these thermal coefficients is found in JESD51-12 ("Guidelines for Reporting and Using Electronic Package Thermal Information").

Many designers may opt to use laboratory equipment and a test vehicle such as the demo board to predict the µModule regulator’s thermal performance in their application at various electrical and environmental operating conditions to compliment any FEA activities. Without FEA software, the thermal resistances reported in the Pin Configuration section are, in and of themselves, not relevant to providing guidance of thermal performance; instead, the derating curves provided in this data sheet can be used in a manner that yields insight and guidance pertaining to one’s application-usage, and can be adapted to correlate thermal performance to one’s own application.

The Pin Configuration section gives four thermal coefficients explicitly defined in JESD51-12; these coefficients are quoted or paraphrased below:

1. \( \theta_JA \), the thermal resistance from junction-to-ambient, is the natural convection junction-to-ambient air thermal resistance measured in a one cubic foot sealed enclosure. This environment is sometimes referred to as “still air” although natural convection causes the air to move. This value is determined with the part mounted to a JESD51-9 defined test board, which does not reflect an actual application or viable operating condition.

2. \( \theta_{J\text{bottom}} \), the thermal resistance from junction to the bottom of the product case, is determined with all of the component power dissipation flowing through the bottom of the package. In the typical µModule regulator, the bulk of the heat flows out the bottom of the package, but there is always heat flow out into the ambient environment. As a result, this thermal resistance value may be useful for comparing packages but the test conditions don’t generally match the user’s application.

3. \( \theta_{J\text{top}} \), the thermal resistance from junction to top of the product case, is determined with nearly all of the component power dissipation flowing through the top of the package. As the electrical connections of the typical µModule regulator are on the bottom of the package, it is rare for an application to operate such that most of the heat flows from the junction to the top of the part. As in the case of \( \theta_{J\text{bottom}} \), this value may be useful for comparing packages but the test conditions don’t generally match the user’s application.

4. \( \theta_{JB} \), the thermal resistance from junction to the printed circuit board, is the junction-to-board thermal resistance where almost all of the heat flows through the bottom of the µModule regulator and into the board, and is really the sum of the \( \theta_{J\text{bottom}} \) and the thermal resistance of the bottom of the part through the solder joints and through a portion of the board. The board temperature is measured a specified distance from the package, using a two sided, two layer board. This board is described in JESD51-9.

A graphical representation of the aforementioned thermal resistances is given in Figure 10: blue resistances are contained within the µModule regulator, whereas green resistances are external to the µModule package.
As a practical matter, it should be clear to the reader that no individual or sub-group of the four thermal resistance parameters defined by JESD51-12 or provided in the Pin Configuration section replicates or conveys normal operating conditions of a µModule regulator. For example, in normal board-mounted applications, never does 100% of the device’s total power loss (heat) thermally conduct exclusively through the top or exclusively through bottom of the µModule package—as the standard defines for $\theta_{JC\text{top}}$ and $\theta_{JC\text{bottom}}$, respectively. In practice, power loss is thermally dissipated in both directions away from the package—granted, in the absence of a heat sink and airflow, a majority of the heat flow is into the board.

Within the LTM4655, be aware there are multiple power devices and components dissipating power, with a consequence that the thermal resistances relative to different junctions of components or die are not exactly linear with respect to total package power loss. To reconcile this complication without sacrificing modeling simplicity—but also not ignoring practical realities—an approach has been taken using FEA software modeling along with laboratory testing in a controlled-environment chamber to reasonably define and correlate the thermal resistance values supplied in this data sheet: (1) Initially, FEA software is used to accurately build the mechanical geometry of the LTM4655 and the specified PCB with all of the correct material coefficients along with accurate power loss source definitions; (2) this model simulates a software-defined JEDEC environment consistent with JESD51-9 and JESD51-12 to predict power loss heat flow and temperature readings at different interfaces that enable the calculation of the JEDEC-defined thermal resistance values; (3) the model and FEA software is used to evaluate the LTM4655 with heat sink and airflow; (4) having solved for and analyzed these thermal resistance values and simulated various operating conditions in the software model, a thorough laboratory evaluation replicates the simulated conditions with thermocouples within a controlled environment chamber while operating the device at the same power loss as that which was simulated. The outcome of this process and due diligence yields the set of derating curves provided in later sections of this data sheet, along with well-correlated JESD51-12-defined $\theta$ values provided in the Pin Configuration section.

For positive-$V_{OUT}$ applications, the $12V_{IN}$ and $24V_{IN}$ power loss curves in Figure 11 and Figure 12, respectively, can be used with the load current derating curves in Figure 13 to Figure 24 for calculating an approximate $\theta_{JA}$ thermal resistance for the LTM4655 with various heat sinking and air flow conditions. For negative-$V_{OUT}$ applications: use instead the $-5V_{OUT}$, $-12V_{OUT}$ and $-24V_{OUT}$ power loss curves in Figure 25 to Figure 27, respectively, in combination with the load current derating curves in Figure 28 to Figure 43. For split-supply applications, total power loss within the module will dictate the thermal derating; interpolate the relevant derating curves. These thermal resistances represent demonstrated performance of the LTM4655 on DC2898A and DC2899A hardware; 4-layer FR4 PCB measuring 97mm $\times$ 116mm $\times$ 1.6mm using outer and inner copper weights of 2oz and 1oz,
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respectively. The power loss curves are taken at room temperature, and are increased with multiplicative factors with ambient temperature. These approximate factors are listed in Table 1. (Compute the factor by interpolation, for intermediate temperatures.) The derating curves are plotted with the LTM4655’s outputs paralleled and inteleaved, sourcing its maximum output capability, in an environment with temperature-controlled ambient. The output voltages are 1V\text{OUT}, 5V\text{OUT}, 15V\text{OUT}, –5V\text{OUT}, –15V\text{OUT} and –24V\text{OUT}. These are chosen to include the lower and higher output voltage ranges for correlating the thermal resistance. Thermal models are derived from several temperature measurements in a controlled temperature chamber along with thermal modeling analysis. The junction temperatures are monitored while ambient temperature is increased with and without air flow, and with and without a heat sink attached with thermally conductive adhesive tape. The power loss increase with ambient temperature change is factored into the derating curves. The junctions are maintained at 120°C maximum while lowering output current or power while increasing ambient temperature. The decreased output current decreases the internal module loss as ambient temperature is increased. The monitored junction temperature of 120°C minus the ambient operating temperature specifies how much module temperature rise can be allowed. As an example in Figure 30, the load current is derated to 3.05A per channel (6.1A, combined) at 60°C ambient with no airflow and no heat sink and the room temperature (25°C) per channel power loss for this 24V\text{IN} to –5V\text{OUT} at 3.05A out condition is 2.45W; 4.9W, combined. A 5.39W loss is calculated by multiplying the 4.9W room temperature loss from the 24V\text{IN} to –5V\text{OUT} power loss curve at 4.9W (Figure 25), with the 1.1 multiplying factor at 60°C ambient (from Table 2). If the 60°C ambient temperature is subtracted from the 120°C junction temperature, then the difference of 60°C divided by 5.39W yields a thermal resistance, θ_{JA}, of 11.1°C/W—in good agreement with Table 6. Table 3 to Table 5 provide equivalent thermal resistances for 1V, 5V, and 15V outputs with and without airflow and heatsinking. Table 6 to Table 8 provide equivalent thermal resistances for –5V, –15V and –24V outputs with and without airflow and heatsinking. The derived thermal resistances in Table 3 to Table 8 for the various conditions can be multiplied by the calculated power loss as a function of ambient temperature to derive temperature rise above ambient, thus maximum junction temperature. Room temperature power loss can be derived from the efficiency curves in the Typical Performance Characteristics section and adjusted with ambient temperature multiplicative factors from Table 2.

Table 2. Power Loss Multiplicative Factors vs Ambient Temperature

<table>
<thead>
<tr>
<th>AMBIENT TEMPERATURE</th>
<th>POWER LOSS MULTIPLICATIVE FACTOR</th>
</tr>
</thead>
<tbody>
<tr>
<td>Up to 40°C</td>
<td>1.00</td>
</tr>
<tr>
<td>50°C</td>
<td>1.05</td>
</tr>
<tr>
<td>60°C</td>
<td>1.10</td>
</tr>
<tr>
<td>70°C</td>
<td>1.15</td>
</tr>
<tr>
<td>80°C</td>
<td>1.20</td>
</tr>
<tr>
<td>90°C</td>
<td>1.25</td>
</tr>
<tr>
<td>100°C</td>
<td>1.30</td>
</tr>
<tr>
<td>110°C</td>
<td>1.35</td>
</tr>
<tr>
<td>120°C</td>
<td>1.40</td>
</tr>
</tbody>
</table>

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### Table 3. 1V Output

<table>
<thead>
<tr>
<th>DERATING CURVE</th>
<th>V&lt;sub&gt;IN&lt;/sub&gt; (V)</th>
<th>POWER LOSS CURVE</th>
<th>AIRFLOW (LFM)</th>
<th>HEAT SINK</th>
<th>θ&lt;sub&gt;JA&lt;/sub&gt; (°C/W)</th>
</tr>
</thead>
<tbody>
<tr>
<td>Figure 13, Figure 14, Figure 15</td>
<td>5, 12, 24</td>
<td>Figure 11, Figure 12</td>
<td>0</td>
<td>None</td>
<td>11.9</td>
</tr>
<tr>
<td>Figure 13, Figure 14, Figure 15</td>
<td>5, 12, 24</td>
<td>Figure 11, Figure 12</td>
<td>200</td>
<td>None</td>
<td>10.9</td>
</tr>
<tr>
<td>Figure 13, Figure 14, Figure 15</td>
<td>5, 12, 24</td>
<td>Figure 11, Figure 12</td>
<td>400</td>
<td>None</td>
<td>10.0</td>
</tr>
<tr>
<td>Figure 16, Figure 17, Figure 18</td>
<td>5, 12, 24</td>
<td>Figure 11, Figure 12</td>
<td>0</td>
<td>BGA Heat Sink</td>
<td>11.2</td>
</tr>
<tr>
<td>Figure 16, Figure 17, Figure 18</td>
<td>5, 12, 24</td>
<td>Figure 11, Figure 12</td>
<td>200</td>
<td>BGA Heat Sink</td>
<td>10.1</td>
</tr>
<tr>
<td>Figure 17, Figure 17, Figure 18</td>
<td>5, 12, 24</td>
<td>Figure 11, Figure 12</td>
<td>400</td>
<td>BGA Heat Sink</td>
<td>9.1</td>
</tr>
</tbody>
</table>

### Table 4. 5V Output

<table>
<thead>
<tr>
<th>DERATING CURVE</th>
<th>V&lt;sub&gt;IN&lt;/sub&gt; (V)</th>
<th>POWER LOSS CURVE</th>
<th>AIRFLOW (LFM)</th>
<th>HEAT SINK</th>
<th>θ&lt;sub&gt;JA&lt;/sub&gt; (°C/W)</th>
</tr>
</thead>
<tbody>
<tr>
<td>Figure 19, Figure 20</td>
<td>12, 24</td>
<td>Figure 11, Figure 12</td>
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<td>None</td>
<td>11.9</td>
</tr>
<tr>
<td>Figure 19, Figure 20</td>
<td>12, 24</td>
<td>Figure 11, Figure 12</td>
<td>200</td>
<td>None</td>
<td>10.9</td>
</tr>
<tr>
<td>Figure 19, Figure 20</td>
<td>12, 24</td>
<td>Figure 11, Figure 12</td>
<td>400</td>
<td>None</td>
<td>10.0</td>
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<tr>
<td>Figure 21, Figure 22</td>
<td>12, 24</td>
<td>Figure 11, Figure 12</td>
<td>0</td>
<td>BGA Heat Sink</td>
<td>11.2</td>
</tr>
<tr>
<td>Figure 21, Figure 22</td>
<td>12, 24</td>
<td>Figure 11, Figure 12</td>
<td>200</td>
<td>BGA Heat Sink</td>
<td>10.1</td>
</tr>
<tr>
<td>Figure 21, Figure 22</td>
<td>12, 24</td>
<td>Figure 11, Figure 12</td>
<td>400</td>
<td>BGA Heat Sink</td>
<td>9.1</td>
</tr>
</tbody>
</table>

### Table 5. 15V Output

<table>
<thead>
<tr>
<th>DERATING CURVE</th>
<th>V&lt;sub&gt;IN&lt;/sub&gt; (V)</th>
<th>POWER LOSS CURVE</th>
<th>AIRFLOW (LFM)</th>
<th>HEAT SINK</th>
<th>θ&lt;sub&gt;JA&lt;/sub&gt; (°C/W)</th>
</tr>
</thead>
<tbody>
<tr>
<td>Figure 23</td>
<td>24</td>
<td>Figure 12</td>
<td>0</td>
<td>None</td>
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<tr>
<td>Figure 23</td>
<td>24</td>
<td>Figure 12</td>
<td>200</td>
<td>None</td>
<td>10.9</td>
</tr>
<tr>
<td>Figure 23</td>
<td>24</td>
<td>Figure 12</td>
<td>400</td>
<td>None</td>
<td>10.0</td>
</tr>
<tr>
<td>Figure 24</td>
<td>24</td>
<td>Figure 12</td>
<td>0</td>
<td>BGA Heat Sink</td>
<td>11.2</td>
</tr>
<tr>
<td>Figure 24</td>
<td>24</td>
<td>Figure 12</td>
<td>200</td>
<td>BGA Heat Sink</td>
<td>10.1</td>
</tr>
<tr>
<td>Figure 24</td>
<td>24</td>
<td>Figure 12</td>
<td>400</td>
<td>BGA Heat Sink</td>
<td>9.1</td>
</tr>
</tbody>
</table>
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### Table 6. –5V Output

<table>
<thead>
<tr>
<th>DERATING CURVE</th>
<th>V_IN (V)</th>
<th>POWER LOSS CURVE</th>
<th>AIRFLOW (LFM)</th>
<th>HEAT SINK</th>
<th>θ_JA (°C/W)</th>
</tr>
</thead>
<tbody>
<tr>
<td>Figure 28, Figure 29, Figure 30</td>
<td>5, 12, 24</td>
<td>Figure 25</td>
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<td>None</td>
<td>11.9</td>
</tr>
<tr>
<td>Figure 28, Figure 29, Figure 30</td>
<td>5, 12, 24</td>
<td>Figure 25</td>
<td>200</td>
<td>None</td>
<td>10.9</td>
</tr>
<tr>
<td>Figure 28, Figure 29, Figure 30</td>
<td>5, 12, 24</td>
<td>Figure 25</td>
<td>400</td>
<td>None</td>
<td>10.0</td>
</tr>
<tr>
<td>Figure 31, Figure 32, Figure 33</td>
<td>5, 12, 24</td>
<td>Figure 25</td>
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<td>BGA Heat Sink</td>
<td>11.2</td>
</tr>
<tr>
<td>Figure 31, Figure 32, Figure 33</td>
<td>5, 12, 24</td>
<td>Figure 25</td>
<td>200</td>
<td>BGA Heat Sink</td>
<td>10.1</td>
</tr>
<tr>
<td>Figure 31, Figure 32, Figure 33</td>
<td>5, 12, 24</td>
<td>Figure 25</td>
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<td>BGA Heat Sink</td>
<td>9.1</td>
</tr>
</tbody>
</table>

### Table 7. –15V Output

<table>
<thead>
<tr>
<th>DERATING CURVE</th>
<th>V_IN (V)</th>
<th>POWER LOSS CURVE</th>
<th>AIRFLOW (LFM)</th>
<th>HEAT SINK</th>
<th>θ_JA (°C/W)</th>
</tr>
</thead>
<tbody>
<tr>
<td>Figure 34, Figure 35, Figure 36</td>
<td>5, 12, 24</td>
<td>Figure 26</td>
<td>0</td>
<td>None</td>
<td>11.9</td>
</tr>
<tr>
<td>Figure 34, Figure 35, Figure 36</td>
<td>5, 12, 24</td>
<td>Figure 26</td>
<td>200</td>
<td>None</td>
<td>10.9</td>
</tr>
<tr>
<td>Figure 34, Figure 35, Figure 36</td>
<td>5, 12, 24</td>
<td>Figure 26</td>
<td>400</td>
<td>None</td>
<td>10.0</td>
</tr>
<tr>
<td>Figure 37, Figure 38, Figure 39</td>
<td>5, 12, 24</td>
<td>Figure 26</td>
<td>0</td>
<td>BGA Heat Sink</td>
<td>11.2</td>
</tr>
<tr>
<td>Figure 37, Figure 38, Figure 39</td>
<td>5, 12, 24</td>
<td>Figure 26</td>
<td>200</td>
<td>BGA Heat Sink</td>
<td>10.1</td>
</tr>
<tr>
<td>Figure 37, Figure 38, Figure 39</td>
<td>5, 12, 24</td>
<td>Figure 26</td>
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<td>9.1</td>
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</tbody>
</table>

### Table 8. –24V Output

<table>
<thead>
<tr>
<th>DERATING CURVE</th>
<th>V_IN (V)</th>
<th>POWER LOSS CURVE</th>
<th>AIRFLOW (LFM)</th>
<th>HEAT SINK</th>
<th>θ_JA (°C/W)</th>
</tr>
</thead>
<tbody>
<tr>
<td>Figure 40, Figure 41</td>
<td>5, 12</td>
<td>Figure 27</td>
<td>0</td>
<td>None</td>
<td>11.9</td>
</tr>
<tr>
<td>Figure 40, Figure 41</td>
<td>5, 12</td>
<td>Figure 27</td>
<td>200</td>
<td>None</td>
<td>10.9</td>
</tr>
<tr>
<td>Figure 40, Figure 41</td>
<td>5, 12</td>
<td>Figure 27</td>
<td>400</td>
<td>None</td>
<td>10.0</td>
</tr>
<tr>
<td>Figure 42, Figure 43</td>
<td>5, 12</td>
<td>Figure 27</td>
<td>0</td>
<td>BGA Heat Sink</td>
<td>11.2</td>
</tr>
<tr>
<td>Figure 42, Figure 43</td>
<td>5, 12</td>
<td>Figure 27</td>
<td>200</td>
<td>BGA Heat Sink</td>
<td>10.1</td>
</tr>
<tr>
<td>Figure 42, Figure 43</td>
<td>5, 12</td>
<td>Figure 27</td>
<td>400</td>
<td>BGA Heat Sink</td>
<td>9.1</td>
</tr>
</tbody>
</table>

### Table 9. Heat Sink Manufacturer (Thermally Conductive Adhesive Tape Pre-Attached)

<table>
<thead>
<tr>
<th>HEAT SINK MANUFACTURER</th>
<th>PART NUMBER</th>
<th>WEBSITE</th>
</tr>
</thead>
<tbody>
<tr>
<td>Aavid Thermalloy</td>
<td>375424B00034G</td>
<td><a href="http://www.aavid.com">www.aavid.com</a></td>
</tr>
<tr>
<td>Cool Innovations</td>
<td>4-050503PT411</td>
<td><a href="http://www.coolinnovations.com">www.coolinnovations.com</a></td>
</tr>
<tr>
<td>Wakefield Engineering</td>
<td>LTN20069</td>
<td><a href="http://www.wakefield.com">www.wakefield.com</a></td>
</tr>
</tbody>
</table>

### Table 10. Thermally Conductive Adhesive Tape Vendor

<table>
<thead>
<tr>
<th>THERMALLY CONDUCTIVE ADHESIVE TAPE MANUFACTURER</th>
<th>PART NUMBER</th>
<th>WEBSITE</th>
</tr>
</thead>
<tbody>
<tr>
<td>Chomerics</td>
<td>T411</td>
<td><a href="http://www.chomerics.com">www.chomerics.com</a></td>
</tr>
</tbody>
</table>
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### Table 11. Positive Output Voltage Response vs Component Matrix. Performance of a Channel of LTM4655 in Figure 51 Circuit, with Values Here Indicated. Load-Stepping from 2A to 4A Load Current, at 2A/μs. Typical Measured Values

<table>
<thead>
<tr>
<th>C(_{\text{OUTn}}) VENDORS</th>
<th>PART NUMBER</th>
<th>C(_{\text{OUTn}})</th>
<th>C(_{\text{INH}})</th>
<th>C(_{\text{D}})</th>
<th>R(_{\text{TH}}) (Ω)</th>
<th>C(_{\text{INH}}) (nF)</th>
<th>R(_{\text{SETn}}) (kΩ)</th>
<th>R(_{\text{PDFFn}}) (kΩ)</th>
<th>f(_{\text{SW}}) (kHz)</th>
<th>R(_{\text{REvCC}}) (kΩ)</th>
<th>LOAD STEP TRANSIENT DROOP (mV)</th>
<th>LOAD STEP PK-PK DEVIATION (mV)</th>
<th>RECOVERY TIME (μs)</th>
</tr>
</thead>
<tbody>
<tr>
<td>AVX</td>
<td>12066J107MAT2A (100μF, 6.3V, 1206 Case Size)</td>
<td>4.7μF</td>
<td>4.7μF</td>
<td>100μF x 3</td>
<td>681</td>
<td>6.8</td>
<td>20</td>
<td>3.32</td>
<td>400</td>
<td>N/A</td>
<td>N/A</td>
<td>70</td>
<td>145</td>
</tr>
<tr>
<td>Murata</td>
<td>GRM31CR60107M (100μF, 6.3V, 1206 Case Size)</td>
<td>4.7μF</td>
<td>4.7μF</td>
<td>100μF x 3</td>
<td>681</td>
<td>6.8</td>
<td>20</td>
<td>3.32</td>
<td>400</td>
<td>N/A</td>
<td>N/A</td>
<td>70</td>
<td>145</td>
</tr>
<tr>
<td>Taiyo Yuden</td>
<td>JMK316BJ07MLHT (100μF, 6.3V, 1206 Case Size)</td>
<td>4.7μF</td>
<td>4.7μF</td>
<td>100μF x 3</td>
<td>681</td>
<td>6.8</td>
<td>20</td>
<td>3.32</td>
<td>400</td>
<td>N/A</td>
<td>N/A</td>
<td>70</td>
<td>145</td>
</tr>
<tr>
<td>Murata</td>
<td>GRM32ER61H106M (10μF, 50V, 1206 Case Size)</td>
<td>4.7μF</td>
<td>4.7μF</td>
<td>100μF x 3</td>
<td>681</td>
<td>6.8</td>
<td>20</td>
<td>3.32</td>
<td>400</td>
<td>N/A</td>
<td>N/A</td>
<td>70</td>
<td>145</td>
</tr>
<tr>
<td>Taiyo Yuden</td>
<td>UMK326BJ06M (10μF, 50V, 1210 Case Size)</td>
<td>4.7μF</td>
<td>4.7μF</td>
<td>100μF x 3</td>
<td>681</td>
<td>6.8</td>
<td>20</td>
<td>3.32</td>
<td>400</td>
<td>N/A</td>
<td>N/A</td>
<td>70</td>
<td>145</td>
</tr>
<tr>
<td>AVX</td>
<td>1210YD478MAT2A (47μF, 16V, 1210 Case Size)</td>
<td>4.7μF</td>
<td>4.7μF</td>
<td>100μF x 3</td>
<td>681</td>
<td>6.8</td>
<td>20</td>
<td>3.32</td>
<td>400</td>
<td>N/A</td>
<td>N/A</td>
<td>70</td>
<td>145</td>
</tr>
<tr>
<td>Murata</td>
<td>GRM32ER71K475M (10μF, 16V, 1206 Case Size)</td>
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<td>4.7μF</td>
<td>100μF x 3</td>
<td>681</td>
<td>6.8</td>
<td>20</td>
<td>3.32</td>
<td>400</td>
<td>N/A</td>
<td>N/A</td>
<td>70</td>
<td>145</td>
</tr>
<tr>
<td>Taiyo Yuden</td>
<td>UMK316AB7475ML (4.7μF, 50V, 1206 Case Size)</td>
<td>4.7μF</td>
<td>4.7μF</td>
<td>100μF x 3</td>
<td>681</td>
<td>6.8</td>
<td>20</td>
<td>3.32</td>
<td>400</td>
<td>N/A</td>
<td>N/A</td>
<td>70</td>
<td>145</td>
</tr>
<tr>
<td>AVX</td>
<td>12103D226MAT2A (22μF, 25V, 1210 Case Size)</td>
<td>4.7μF</td>
<td>4.7μF</td>
<td>100μF x 3</td>
<td>681</td>
<td>6.8</td>
<td>20</td>
<td>3.32</td>
<td>400</td>
<td>N/A</td>
<td>N/A</td>
<td>70</td>
<td>145</td>
</tr>
<tr>
<td>Murata</td>
<td>GRM31CR71H475M (4.7μF, 50V, 1206 Case Size)</td>
<td>4.7μF</td>
<td>4.7μF</td>
<td>100μF x 3</td>
<td>681</td>
<td>6.8</td>
<td>20</td>
<td>3.32</td>
<td>400</td>
<td>N/A</td>
<td>N/A</td>
<td>70</td>
<td>145</td>
</tr>
<tr>
<td>Taiyo Yuden</td>
<td>UMK316AB7475ML (4.7μF, 50V, 1206 Case Size)</td>
<td>4.7μF</td>
<td>4.7μF</td>
<td>100μF x 3</td>
<td>681</td>
<td>6.8</td>
<td>20</td>
<td>3.32</td>
<td>400</td>
<td>N/A</td>
<td>N/A</td>
<td>70</td>
<td>145</td>
</tr>
</tbody>
</table>

For more information [www.analog.com](http://www.analog.com)
**APPLICATIONS INFORMATION**

Table 12. Negative Output Voltage Response vs Component Matrix. Performance of Figure 48 Circuit with Values Here Indicated. Load-Stepping from 50% of Full Scale (F.S.) to 100% of F.S. Load Current, in 1μs. Typical Measured Values.

<table>
<thead>
<tr>
<th>vendors</th>
<th>part number</th>
<th>cinh</th>
<th>cd</th>
<th>couth</th>
<th>part number</th>
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<tr>
<td>avx</td>
<td>12066d107mat2a (100µf, 6.3v, 1206 case size)</td>
<td>murata</td>
<td>grm32er71k475m (4.7µf, 80v, 1210 case size)</td>
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<tr>
<td>murata</td>
<td>grms31cr6uj07m (100µf, 6.3v, 1206 case size)</td>
<td>avx</td>
<td>12065c475mat2a (4.7µf, 50v, 1206 case size)</td>
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<tr>
<td>taiyo yuden</td>
<td>jmk316bbj107mlht (100µf, 6.3v, 1206 case size)</td>
<td>murata</td>
<td>grm31cr71h475m (4.7µf, 50v, 1206 case size)</td>
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<td></td>
</tr>
<tr>
<td>tdk</td>
<td>c3216srru107m (100µf, 6.3v, 1206 case size)</td>
<td>tdk</td>
<td>umk318ab7475ml (4.7µf, 50v, 1206 case size)</td>
<td></td>
<td></td>
</tr>
<tr>
<td>avx</td>
<td>1210yd476mat2a (47µf, 16v, 1206 case size)</td>
<td>tdk</td>
<td>c3216srsr1h475m (4.7µf, 50v, 1206 case size)</td>
<td></td>
<td></td>
</tr>
<tr>
<td>murata</td>
<td>grm32er61c476m (47µf, 16v, 1210 case size)</td>
<td>tdk</td>
<td>c3216srru1h475m (4.7µf, 50v, 1206 case size)</td>
<td></td>
<td></td>
</tr>
<tr>
<td>taiyo yuden</td>
<td>emk325u476mm (47µf, 16v, 1210 case size)</td>
<td>avx</td>
<td>1210s226mat2a (22µf, 25v, 1206 case size)</td>
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<td></td>
</tr>
<tr>
<td>tdk</td>
<td>c3225xr1e226m (22µf, 25v, 1206 case size)</td>
<td>avx</td>
<td>1210s106mat2a (10µf, 50v, 1206 case size)</td>
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<td></td>
</tr>
<tr>
<td>tdk</td>
<td>c3225xr1h106m (10µf, 50v, 1206 case size)</td>
<td>avx</td>
<td>1210s106mat2a (10µf, 50v, 1206 case size)</td>
<td></td>
<td></td>
</tr>
<tr>
<td>tdk</td>
<td>c3225xs106mat2a (10µf, 50v, 1206 case size)</td>
<td>tdk</td>
<td>c3225xs106mat2a (10µf, 50v, 1206 case size)</td>
<td></td>
<td></td>
</tr>
</tbody>
</table>

*Internal loop compensation is used with Table 12 settings. COMPna connects to COMPnb in Figure 48.

**To avoid violating minimum on-time criteria, drive CLKin with a 200kHz, 50% duty cycle clock.
APPLICATIONS INFORMATION—DERATING CURVES

Figure 11. 12VIN Power Loss Curve

Figure 12. 24VIN Power Loss Curve

Figure 13. 5V to 1VOUT Derating Curve, No Heat Sink

Figure 14. 12V to 1VOUT Derating Curve, No Heat Sink

Figure 15. 24V to 1VOUT Derating Curve, No Heat Sink

Figure 16. 5V to 1VOUT Derating Curve, with BGA Heat Sink

Figure 17. 12V to 1VOUT Derating Curve, with BGA Heat Sink

Figure 18. 24V to 1VOUT Derating Curve, with BGA Heat Sink

Figure 19. 12V to 5VOUT Derating Curve, No Heat Sink

Settings per Table 11 and Table 12.

For more information www.analog.com
APPLIED INFORMATION—DERATING CURVES

Figure 20. 24V to 5V<sub>OUT</sub> Derating Curve, No Heat Sink

Figure 21. 12V to 5V<sub>OUT</sub> Derating Curve, with BGA Heat Sink

Figure 22. 24V to 5V<sub>OUT</sub> Derating Curve, with BGA Heat Sink

Figure 23. 24V to 15V<sub>OUT</sub> Derating Curve, No Heat Sink

Figure 24. 24V to 15V<sub>OUT</sub> Derating Curve, with BGA Heat Sink

Figure 25. –5V<sub>OUT</sub> Power Loss Curve, No Heat Sink

Figure 26. –15V<sub>OUT</sub> Power Loss Curve

Figure 27. –24V<sub>OUT</sub> Power Loss Curve

Figure 28. 5V to –5V<sub>OUT</sub> Derating Curve, No Heat Sink
Figure 29. 12V to –5V OUT
Derating Curve, No Heat Sink

Figure 30. 24V to –5V OUT
Derating Curve, No Heat Sink

Figure 31. 5V to –5V OUT Derating Curve, with BGA Heat Sink

Figure 32. 12V to –5V OUT
Derating Curve, with BGA Heat Sink

Figure 33. 24V to –5V OUT
Derating Curve, with BGA Heat Sink

Figure 34. 5V to –15V OUT
Derating Curve, No Heat Sink

Figure 35. 12V to –15V OUT
Derating Curve, No Heat Sink

Figure 36. 24V to –15V OUT
Derating Curve, No Heat Sink

Figure 37. 5V to –15V OUT Derating Curve, with BGA Heat Sink
APPLICATIONS INFORMATION—DERATING CURVES

Settings per Table 11 and Table 12.

Figure 38. 12V to –15VOUT Derating Curve, with BGA Heat Sink

Figure 39. 24V to –15VOUT Derating Curve, with BGA Heat Sink

Figure 40. 5V to –24VOUT Derating Curve, No Heat Sink

Figure 41. 12V to –24VOUT Derating Curve, No Heat Sink

Figure 42. 5V to –24VOUT Derating Curve, with BGA Heat Sink

Figure 43. 12V to –24VOUT Derating Curve, with BGA Heat Sink
APPLICATIONS INFORMATION

Safety Considerations

The LTM4655 does not provide galvanic isolation from \( V_{INn} \) to \( V_{OUTn}^+/V_{OUTn}^- \). There is no internal fuse. If required, a slow blow fuse with a rating twice the maximum input current needs to be provided to protect the unit from catastrophic failure.

The fuse or circuit breaker, if used, should be selected to limit the current to the regulator in case of a \( M_{Trn} \) MOSFET fault. If \( M_{Trn} \) fails, the system’s input supply will source very large currents to \( V_{OUTn}^+ \) through \( M_{Trn} \). This can cause excessive heat and board damage depending on how much power the input voltage can deliver to this system.

A fuse or circuit breaker can be used as a secondary fault protector in this situation. Each channel of the LTM4655 features its own, independent overcurrent and overtemperature protection.

Layout Checklist/Example

The high integration of LTM4655 makes the PCB board layout straightforward. However, to optimize its electrical and thermal performance, some layout considerations are still necessary.

- Use large PCB copper areas for high current paths, including \( V_{INn} \), \( V_{OUTn}^+ \) and \( V_{OUTn}^- \). Doing so helps to minimize the PCB conduction loss and thermal stress.
- Place high frequency ceramic input and output (and, if used, input-to-output) capacitors next to the \( V_{INn} \), \( V_{Dn} \), \( V_{OUTn}^+/V_{OUTn}^- \) pins to minimize high frequency noise.
- Place a dedicated power ground layer underneath the LTM4655.
- To minimize the via conduction loss and reduce module thermal stress, use multiple vias for interconnection between top layer and other power layers.
- Do not put vias directly on pads, unless they are capped or plated over.
- For each channel, use a separate \( SV_{OUTn}^- \) copper plane for components connected to signal pins. Connect \( SV_{OUTn}^- \) to \( V_{OUTn}^- \) directly under the module.
- For parallel applications, connect the respective \( V_{OUTn}^+ \), \( V_{OUTn}^- \), \( V_{OSNSn}^+ \), \( \text{RUNn} \), \( \text{ISETna} \), \( \text{COMPna} \), \( \text{PGOODn} \) and \( \text{IMONna} \) pins, accordingly (see Figure 45).
- Bring out test points on the signal pins for monitoring.

Figure 44 gives a good example of the recommended LTM4655 layout.

![Figure 44. Recommended PCB Layout, Package Top View](image-url)
TYPICAL APPLICATIONS

Figure 45. Single 8A, 24V Output DC/DC μModule Regulator with Optional Analog Temperature Indicator

* PLACE 470pF DIRECTLY ACROSS THE LTC2997’S D+/D− PINS.
ROUTE TEMP+/TEMP− DIFFERENTIALLY TO D+/D− AND PROTECT FROM NOISE WITH GROUND SHIELDING.
TERMINATE (CONNECT) THE D+/D− GROUND SHIELD AT THE LTC2997 GND PIN, ONLY.
FOR BEST VPTAT PERFORMANCE, THE VCC PIN OF THE LTC2997 MUST BE LOCALLY BYPASSED AND QUIET.
SEE LTC2997 DATA SHEET AND APRIL 2017 LT JOURNAL TECHNICAL ARTICLES.
Figure 46. Start-Up Waveforms at 36V\textsubscript{IN}, Figure 45 Circuit

Figure 47. Current Sharing Performance of LTM4655 Channels in Figure 45 Circuit
**TYPICAL APPLICATIONS**

![Diagram of a DC/DC μModule Regulator](image)

**Figure 48. 1.25A, –24V Output DC/DC μModule Regulator**

* D1 OPTIONAL (SEE EFFECT IN FIGURE 49): CENTRAL SEMICONDUCTOR P/N CMMSH1-40L

** ONE CHANNEL SHOWN. PINS NOT USED AND NOT SHOWN IN THIS CIRCUIT: NC, SVINF, n, IMON, LDOIN, LDOOUT, CLKSET, MOD, CLKOUT, n, TEMP+, TEMP–

**ISET, ISETb

**VIN, SVIN

**VD

**RUN

**INTVCC

**VOUTn

**PGOODn

**GND

**VSSN

**SVOUT

**PGDFB

**EXTVCC

**IMON

**CD

**CDGND

**CINOUT

**CINH

**CDGND

**CD

**PGOODn

**VINREG

**COMP

**COMPn

**FSET

**COMPnb

**LTM4655

–24VOUT

UP TO 1.25A

**COUT

10µF ×2

**LOAD

–24VOUT

UP TO 1.25A

**RfSET

165k

**RISET

481k

**CDGND

4.7/µF

**CIN

4.7/µF

**CDGND

4.7/µF

**PGOODn

100k

**VOSNS

+ GND

**VOUT

–

**SVOUT

–

**PGDFB

196k

**PGOOD

100k

**CEXTVCC

1µF

**CEXTVCC

1µF

**RUN

5V/DIV

**PGOODn

5V/DIV

**VOUTn

10V/DIV

**VOUTn

200mV/DIV

**VOUTn

200mV/DIV

**RUNn, 5V/DIV

PGOODn, 5V/DIV

VOUTn, 10V/DIV

VOUTn, 200mV/DIV

1ms/DIV

4655 F48

4655 F48

4655 F49a

4655 F49b

(a) Start-up Performance with D1 Not Installed. VOUTn Reverse-Polarity at Start-Up Transiently Reaches 500mV

(b) Start-up Performance with D1 Installed. VOUTn Reverse-Polarity at Start-Up is Transiently Limited to 360mV

**Figure 49. Start-Up Waveforms at 12VIN, Figure 48 Circuit**

For more information [www.analog.com](http://www.analog.com)
Figure 50. Concurrent ±12V Output DC/DC μModule Regulator

Figure 51. Dual 4A, 12V and 5V Output DC/DC μModule Regulator
Figure 52. A DAC-Controlled Bipolar-Output Programmable Power Supply

* SEE TABLE 6 AND APPLICATIONS INFORMATION SECTION FOR NEGATIVE OUTPUT CURRENT CAPABILITY

** BOTH HALVES OF L T6016 ON SAME SUPPLY
## PACKAGE DESCRIPTION

### Table 13. LTM4655 Component BGA Pinout

<table>
<thead>
<tr>
<th>PIN ID</th>
<th>FUNCTION</th>
<th>PIN ID</th>
<th>FUNCTION</th>
<th>PIN ID</th>
<th>FUNCTION</th>
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<th>FUNCTION</th>
<th>PIN ID</th>
<th>FUNCTION</th>
<th>PIN ID</th>
<th>FUNCTION</th>
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<tbody>
<tr>
<td>A1</td>
<td>V IN1</td>
<td>B1</td>
<td>CLKIN1</td>
<td>C1</td>
<td>IMON1b</td>
<td>D1</td>
<td>PGOOD1</td>
<td>E1</td>
<td>COMP1b</td>
<td>F1</td>
<td>ISET1b</td>
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<tr>
<td>A2</td>
<td>V IN1</td>
<td>B2</td>
<td>CLKOUT1</td>
<td>C2</td>
<td>IMON1a</td>
<td>D2</td>
<td>PGDB1</td>
<td>E2</td>
<td>COMP1a</td>
<td>F2</td>
<td>ISET1a</td>
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<tr>
<td>A3</td>
<td>V IN1</td>
<td>B3</td>
<td>V IN1</td>
<td>C3</td>
<td>SV IN1</td>
<td>D3</td>
<td>VINREG1</td>
<td>E3</td>
<td>I SET1</td>
<td>F3</td>
<td>EXTVCC1</td>
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<tr>
<td>A4</td>
<td>V B1</td>
<td>B4</td>
<td>V D1</td>
<td>C4</td>
<td>V D1</td>
<td>D4</td>
<td>GND</td>
<td>E4</td>
<td>SVOUT1+</td>
<td>F4</td>
<td>RUN1</td>
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<tr>
<td>A5</td>
<td>V OUT1+</td>
<td>B5</td>
<td>V OUT1+</td>
<td>C5</td>
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<td>V OUT1+</td>
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<td>V OUT1+</td>
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<td>B6</td>
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<td>C6</td>
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<td>D6</td>
<td>PGGOOD2</td>
<td>E6</td>
<td>COMP2b</td>
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<td>CLKOUT2</td>
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<td>PGDB2</td>
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<td>COMP2a</td>
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<td>ISET2a</td>
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<td>V IN2</td>
<td>B8</td>
<td>V IN2</td>
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<td>D8</td>
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<td>B9</td>
<td>V D2</td>
<td>C9</td>
<td>V D2</td>
<td>D9</td>
<td>GND</td>
<td>E9</td>
<td>SVOUT2–</td>
<td>F9</td>
<td>RUN2</td>
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<td>A10</td>
<td>V OUT2–</td>
<td>B10</td>
<td>V OUT2–</td>
<td>C10</td>
<td>V OUT2–</td>
<td>D10</td>
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<td>V OUT2–</td>
<td>F10</td>
<td>V OUT2–</td>
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<td>SV INF2</td>
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<tr>
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<td>B12</td>
<td>LDO IN</td>
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<td>GND</td>
<td>E12</td>
<td>MOD</td>
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<td>CLKSET</td>
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### Notes
- For more information visit [www.analog.com](http://www.analog.com)
**PACKAGE DESCRIPTION**

144-Lead (16mm × 16mm × 5.01mm) BGA Package

(Reference LTC DWG # 05-08-1551 Rev Ø)

---

**Table: Dimensions**

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<th>MAX</th>
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<td>A</td>
<td>0.50</td>
<td>5.01</td>
<td>5.21</td>
</tr>
<tr>
<td>B</td>
<td>0.50</td>
<td>4.00</td>
<td>4.50</td>
</tr>
<tr>
<td>C</td>
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<td>D</td>
<td>0.50</td>
<td>3.60</td>
<td>3.95</td>
</tr>
<tr>
<td>E</td>
<td>0.50</td>
<td>2.00</td>
<td>2.20</td>
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<tr>
<td>F</td>
<td>0.50</td>
<td>1.00</td>
<td>1.20</td>
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<td>G</td>
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<td>0.80</td>
<td>0.90</td>
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<tr>
<td>H2</td>
<td>0.50</td>
<td>0.60</td>
<td>0.70</td>
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</tbody>
</table>

---

**Notes:**

1. DIMENSIONING AND TOLERANCING PER ASME Y14.5M-1994
2. ALL DIMENSIONS ARE IN MILLIMETERS, DRAWING NOT TO SCALE
3. BALL DESIGNATION PER JESD MS-028 AND JEP95
4. PRIMARY DATUM -z- IS SEATING PLANE
5. SOLID BALL COMPOSITION IS 96.5% Sn/3.0% Ag/0.5% Cu
6. PACKAGE ROW AND COLUMN LABELING MAY VARY
7. TOTAL NUMBER OF BALLS 144

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## DESIGN RESOURCES

<table>
<thead>
<tr>
<th>SUBJECT</th>
<th>DESCRIPTION</th>
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</table>
| µModule Design and Manufacturing Resources | Design:  
  - Selector Guides  
  - Demo Boards and Gerber Files  
  - Free Simulation Tools  

Manufacturing:  
  - Quick Start Guide  
  - PCB Design, Assembly and Manufacturing Guidelines  
  - Package and Board Level Reliability |

µModule Regulator Products Search  
1. Sort table of products by parameters and download the result as a spread sheet.  
2. Search using the Quick Power Search parametric table.

### Digital Power System Management

Analog Devices’ family of digital power supply management ICs are highly integrated solutions that offer essential functions, including power supply monitoring, supervision, margining and sequencing, and feature EEPROM for storing user configurations and fault logging.

## RELATED PARTS

<table>
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<tr>
<th>PART NUMBER</th>
<th>DESCRIPTION</th>
<th>COMMENTS</th>
</tr>
</thead>
<tbody>
<tr>
<td>LTM4651</td>
<td>EN55022B Compliant 58VIN, 24W Inverting-Output DC/DC µModule Regulator</td>
<td>3.6V ≤ VIN ≤ 58V, –26.5V ≤ VOUT ≤ –0.5V, IOUT ≤ 4A, 15mm × 9mm × 5.01mm BGA</td>
</tr>
<tr>
<td>LTM4653</td>
<td>EN55022B Compliant 58VIN, 4A Step-Down DC/DC µModule Regulator</td>
<td>3.1V ≤ VIN ≤ 58V, 0.5V ≤ VOUT ≤ 0.94V ≤ VIN, 15mm × 9mm × 5.01mm BGA</td>
</tr>
<tr>
<td>LTM8045</td>
<td>SEPIC or Inverting µModule DC/DC Converter</td>
<td>2.8V ≤ VIN ≤ 10V, ±2.5V ≤ VOUT ≤ ±15V, IOUT(DC) ≤ 700mA, 6.25mm × 11.25mm × 4.92mm BGA</td>
</tr>
<tr>
<td>LTM8053</td>
<td>40V, Dual 3.5A Silent Switcher Step-Down µModule Regulator</td>
<td>3.4V ≤ VIN ≤ 40V, 0.97V ≤ VOUT ≤ 15V, 6.25mm × 9mm × 3.32mm BGA</td>
</tr>
<tr>
<td>LTM8024</td>
<td>40V, 3.5A Silent Switcher Step-Down µModule Regulator</td>
<td>3V ≤ VIN ≤ 40V, 0.8V ≤ VOUT ≤ 8V, 9mm × 11.25mm × 3.32mm BGA</td>
</tr>
<tr>
<td>LTM8049</td>
<td>Dual, SEPIC and/or Inverting µModule DC/DC Converter</td>
<td>2.6V ≤ VIN ≤ 20V, ±2.5V ≤ VOUT ≤ ±24V, IOUT(DC) ≤ 1A/Channel, 9mm × 15mm × 2.42mm BGA</td>
</tr>
<tr>
<td>LTM8071</td>
<td>60V, 5A Silent Switcher® Step-Down µModule Regulator</td>
<td>3.6V ≤ VIN ≤ 60V, 0.97V ≤ VOUT ≤ 15V, 6.25mm × 9mm × 3.32mm BGA</td>
</tr>
<tr>
<td>LTM8073</td>
<td>60V, 3A Silent Switcher Step-Down µModule Regulator</td>
<td>3.4V ≤ VIN ≤ 60V, 0.8V ≤ VOUT ≤ 15V, 9mm × 11.25mm × 3.32mm BGA</td>
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</tbody>
</table>