LTC7815

Low IQ, 2.25MHz, Triple Output, Buck/Buck/Boost Synchronous Controller

DESCRIPTION

The LTC®7815 is a high performance triple output (buck/buck/boost) synchronous DC/DC switching regulator controller that drives all N-channel power MOSFET stages. Constant frequency current mode architecture allows a phase-lockable switching frequency of up to 2.25MHz. The LTC7815 operates from a wide 4.5V to 38V input supply range. When biased from the output of the boost converter or another auxiliary supply, the LTC7815 can operate from an input supply as low as 2.5V after start-up.

The 28μA no-load quiescent current extends operating runtime in battery powered systems. OPTI-LOOP compensation allows the transient response to be optimized over a wide range of output capacitance and ESR values. The LTC7815 features a precision 0.8V reference for the bucks, 1.2V reference for the boost and a power good output indicator. The PLLIN/MODE pin selects among Burst Mode operation, pulse-skipping mode, or continuous inductor current mode at light loads.

FEATURES

- Dual Buck Plus Single Boost Synchronous Controllers
- Wide Bias Input Voltage Range: 4.5V to 38V
- Outputs Remain in Regulation Through Cold Crank Down to a 2.5V Input Supply Voltage
- Buck Output Voltage Range: 0.8V ≤ VOUT ≤ 24V
- Boost Output Voltage Up to 60V
- Low Operating IQ: 28μA (One Channel On)
- RSENSE or DCR Current Sensing
- 100% Duty Cycle for Boost Synchronous MOSFET Even in Burst Mode® Operation
- Phase-Lockable Frequency (320kHz to 2.25MHz)
- Programmable Fixed Frequency (320kHz to 2.25MHz)
- Very Low Buck Dropout Operation: 98% Duty Cycle
- Small 38-Lead 5mm × 7mm QFN Package

APPLICATIONS

- Automotive Always-On and Start-Stop Systems
- Battery Operated Digital Devices
- Distributed DC Power Systems
- Multioutput Buck-Boost Applications

TYPICAL APPLICATION

For more information www.linear.com/LTC7815
LTC7815

**ABSOLUTE MAXIMUM RATINGS** (Note 1)

- **Bias Input Supply Voltage (V\text{BIAS})**
  - –0.3V to 40V

- **Buck Top Side Driver Voltages**
  - (BOOST1, BOOST2) — –0.3V to 46V
  - (BOOST3) — –0.3V to 71V

- **Boost Top Side Driver Voltages**
  - (BOOST1–SW1), (BOOST2–SW2), (BOOST3–SW3) — –0.3V to 6V
  - BG1, BG2, BG3, TG1, TG2, TG3 — (Note 8)

- **Buck Switch Voltage (SW1, SW2)**
  - –5V to 40V

- **Boost Switch Voltage (SW3)**
  - –5V to 65V

- **INT\text{CC}, (BOOST1–SW1), (BOOST2–SW2), (BOOST3–SW3)**
  - –0.3V to 6V

- **BG1, BG2, BG3, TG1, TG2, TG3** — (Note 8)

- **RUN1, RUN2, RUN3** — –0.3V to 8V

- **Maximum Current Sourced Into Pin from Source >8V** — 100µA

- **SENSE1\text{+}, SENSE2\text{+}, SENSE1\text{–}, SENSE2\text{–} Voltages**
  - –0.3V to 28V

- **SENSE3\text{+}, SENSE3\text{–} Voltages**
  - –0.3V to 40V

- **FREQ Voltages**
  - –0.3V to INT\text{CC}
  - EXT\text{CC} — –0.3V to 14V

- **IT\text{H1}, IT\text{H2}, IT\text{H3}, V\text{FB1}, V\text{FB2}, V\text{FB3} Voltages**
  - –0.3V to 6V

- **PLL\text{IN/MODE}, PGOOD1, OV3 Voltages**
  - –0.3V to 6V

- **TRACK/SS1, TRACK/SS2, SS3 Voltages**
  - –0.3V to 6V

- **Operating Junction Temperature Range (Notes 2, 3)**
  - LTC 7815E, LTC7815I — –40°C to 125°C
  - LTC 7815H — –40°C to 150°C

- **Storage Temperature Range**
  - –65°C to 150°C

---

**PIN CONFIGURATION**
## ORDER INFORMATION

http://www.linear.com/product/LTC7815#orderinfo

<table>
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<th>LEAD FREE FINISH</th>
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<th>PART MARKING*</th>
<th>PACKAGE DESCRIPTION</th>
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<td>LTC7815EUHF#TRPBF</td>
<td>7815</td>
<td>38-Lead (5mm × 7mm) Plastic QFN</td>
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<td>7815</td>
<td>38-Lead (5mm × 7mm) Plastic QFN</td>
<td>–40°C to 150°C</td>
</tr>
</tbody>
</table>

Consult ADI Marketing for parts specified with wider operating temperature ranges. *The temperature grade is identified by a label on the shipping container.

For more information on lead free part marking, go to: [http://www.linear.com/leadfree/](http://www.linear.com/leadfree/)

For more information on tape and reel specifications, go to: [http://www.linear.com/tapeandreel/](http://www.linear.com/tapeandreel/).

Some packages are available in 500 unit reels through designated sales channels with #TRMPBF suffix.

## ELECTRICAL CHARACTERISTICS

The ● denotes the specifications which apply over the specified operating junction temperature range, otherwise specifications are at $T_A = 25°C$ (Notes 2, 4). $V_{BIAS} = 12V$, $V_{RUN1,2,3} = 5V$, $EXTV_{CC} = 0V$ unless otherwise noted.

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<th>SYMBOL</th>
<th>PARAMETER</th>
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<th>TYP</th>
<th>MAX</th>
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<td>4.5</td>
<td></td>
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<td>V</td>
</tr>
<tr>
<td></td>
<td></td>
<td>$V_{FB1,2}$ Buck Regulated Feedback Voltage</td>
<td>0.792</td>
<td>0.800</td>
<td>0.808</td>
<td>V</td>
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<tr>
<td></td>
<td></td>
<td>$V_{FB1,2}$ Buck Regulated Feedback Voltage</td>
<td>0.788</td>
<td>0.800</td>
<td>0.812</td>
<td>V</td>
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<td></td>
<td></td>
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<td>0.786</td>
<td>0.800</td>
<td>0.812</td>
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<tr>
<td>$I_{FB1,2,3}$</td>
<td>Feedback Current</td>
<td>(Note 4)</td>
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<td>±50</td>
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<td>$V_{REFLNREG}$</td>
<td>Reference Voltage Line Regulation</td>
<td>(Note 4): $V_{TH} = 4.5V$ to 38V</td>
<td>0.002</td>
<td>0.02</td>
<td></td>
<td>%/V</td>
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<td>$V_{LOADREG}$</td>
<td>Output Voltage Load Regulation</td>
<td>(Note 4)</td>
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<tr>
<td></td>
<td></td>
<td>$V_{LOADREG}$</td>
<td></td>
<td></td>
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<tr>
<td></td>
<td></td>
<td>$V_{LOADREG}$</td>
<td></td>
<td></td>
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<tr>
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<td>2</td>
<td></td>
<td></td>
<td>mmho</td>
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For more information [www.linear.com/LTC7815](http://www.linear.com/LTC7815)
## ELECTRICAL CHARACTERISTICS

The ● denotes the specifications which apply over the specified operating junction temperature range, otherwise specifications are at $T_A = 25°C$ (Notes 2, 4). $V_{BIAS} = 12V$, $V_{RUN1,2,3} = 5V$, $EXTV_{CC} = 0V$ unless otherwise noted.

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<td>Pulse-Skipping or Forced Continuous Mode (One Channel On)</td>
<td>RUN1 = 5V and RUN2,3 = 0V or RUN2 = 5V and RUN1,3 = 0V or RUN3 = 5V and RUN1,2 = 0V $V_{FB1,2}$ ON = 0.83V (No Load) $V_{FB3}$ = 1.25V</td>
<td>1.5</td>
<td>mA</td>
<td></td>
<td></td>
</tr>
<tr>
<td></td>
<td>Pulse-Skipping or Forced Continuous Mode (All Channels On)</td>
<td>RUN1,2,3 = 5V, $V_{FB1,2}$ = 0.83V (No Load) $V_{FB3}$ = 1.25V</td>
<td>3</td>
<td>mA</td>
<td></td>
<td></td>
</tr>
<tr>
<td></td>
<td>Sleep Mode (One Channel On, Buck)</td>
<td>RUN1 = 5V and RUN2,3 = 0V or RUN2 = 5V and RUN1,3 = 0V $V_{FB,ON}$ = 0.83V (No Load)</td>
<td>●</td>
<td>28</td>
<td>48</td>
<td>µA</td>
</tr>
<tr>
<td></td>
<td></td>
<td></td>
<td>●</td>
<td>35</td>
<td>59</td>
<td>µA</td>
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<tr>
<td></td>
<td>Sleep Mode (One Channel On, Boost)</td>
<td>RUN3 = 5V and RUN1,2 = 0V $V_{FB3}$ = 1.25V</td>
<td>33</td>
<td>53</td>
<td>µA</td>
<td></td>
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<tr>
<td></td>
<td>Sleep Mode (Buck and Boost Channel On)</td>
<td>RUN1 = 5V and RUN2 = 0V or RUN2 = 5V and RUN1 = 0V RUN3 = 5V $V_{FB1,2}$ = 0.83V (No Load) $V_{FB3}$ = 1.25V</td>
<td>33</td>
<td>46</td>
<td>µA</td>
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<td></td>
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<td>40</td>
<td>59</td>
<td>µA</td>
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<tr>
<td></td>
<td>Sleep Mode (All Three Channels On)</td>
<td>RUN1,2,3 = 5V, $V_{FB1,2}$ = 0.83V (No Load) $V_{FB3}$ = 1.25V</td>
<td>38</td>
<td>56</td>
<td>µA</td>
<td></td>
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<td></td>
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<td>RUN1,2,3 = 0V</td>
<td></td>
<td></td>
<td></td>
<td>10</td>
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<td>$UVLO$</td>
<td>Undervoltage Lockout</td>
<td>$INTV_{CC}$ Ramping Up</td>
<td></td>
<td></td>
<td></td>
<td>4.15</td>
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<td></td>
<td></td>
<td>$INTV_{CC}$ Ramping Down</td>
<td></td>
<td></td>
<td></td>
<td>●</td>
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<td>$V_{OV1,2}$</td>
<td>Buck Feedback Overvoltage Protection</td>
<td>Measured at $V_{FB1,2}$ Relative to Regulated $V_{FB1,2}$</td>
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<td>10</td>
<td>13</td>
<td>%</td>
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<tr>
<td>$I_{SENSE1,2,+}$</td>
<td>SENSE+ Pin Current (Bucks (Channels 1 and 2) $V_{OUT} = 3.3V$)</td>
<td></td>
<td>±1</td>
<td>µA</td>
<td></td>
<td></td>
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<tr>
<td>$I_{SENSE3,+}$</td>
<td>SENSE+ Pin Current (Boost (Channel 3))</td>
<td></td>
<td>170</td>
<td>µA</td>
<td></td>
<td></td>
</tr>
<tr>
<td>$I_{SENSE1,2,-}$</td>
<td>SENSE- Pin Current (Bucks (Channels 1 and 2) $V_{OUT} = 3.3V$ $V_{OUT1,2} &gt; V_{INTVCC} + 0.5V$)</td>
<td></td>
<td>±2</td>
<td>µA</td>
<td></td>
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<td></td>
<td></td>
<td></td>
<td>700</td>
<td>µA</td>
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<tr>
<td>$I_{SENSE3,-}$</td>
<td>SENSE- Pin Current (Boost (Channel 3)) $V_{SENSE3+, VSENSE3-} = 12V$</td>
<td></td>
<td>±1</td>
<td>µA</td>
<td></td>
<td></td>
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<tr>
<td>$DF_{MAX,TG}$</td>
<td>Maximum Duty Factor for TG (Bucks (Channels 1, 2) in Dropout, $FREQ = 0V$ Boost (Channel 3) in Overvoltage)</td>
<td></td>
<td>97</td>
<td>98</td>
<td>100</td>
<td>%</td>
</tr>
<tr>
<td>$DF_{MAX,BG}$</td>
<td>Maximum Duty Factor for BG (Bucks (Channels 1, 2) in Overvoltage Boost (Channel 3))</td>
<td></td>
<td>100</td>
<td>%</td>
<td></td>
<td></td>
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<tr>
<td></td>
<td></td>
<td></td>
<td>90</td>
<td>%</td>
<td></td>
<td></td>
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<tr>
<td>$I_{TRACK/SS1,2}$</td>
<td>Soft-Start Charge Current $V_{TRACK/SS1,2} = 0V$</td>
<td></td>
<td>3</td>
<td>5</td>
<td>8</td>
<td>µA</td>
</tr>
<tr>
<td>$I_{SS3}$</td>
<td>Soft-Start Charge Current $V_{SS3} = 0V$</td>
<td></td>
<td>3</td>
<td>5</td>
<td>8</td>
<td>µA</td>
</tr>
<tr>
<td>$V_{RUN1,2,3}$</td>
<td>RUN1,2,3 Pin Threshold</td>
<td></td>
<td></td>
<td></td>
<td></td>
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<td></td>
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<td>$V_{RUN1,2,3}$</td>
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<td>$V_{RUN1}$ Rising</td>
<td></td>
<td></td>
<td></td>
<td>1.18</td>
</tr>
<tr>
<td></td>
<td></td>
<td>$V_{RUN2,3}$ Rising</td>
<td></td>
<td></td>
<td></td>
<td>1.21</td>
</tr>
<tr>
<td>$V_{RUN1,2,3}$</td>
<td>RUN Pin Hysteresis</td>
<td></td>
<td></td>
<td></td>
<td></td>
<td>70</td>
</tr>
<tr>
<td>$V_{SENSE1,2,3,(MAX)}$</td>
<td>Maximum Current Sense Threshold $V_{FB1,2} = 0.7V$, $V_{SENSE1,2,-} = 3.3V$ $V_{FB1,2} = 1.1V$, $V_{SENSE3+, VSENSE3,-} = 12V$</td>
<td></td>
<td>43</td>
<td>50</td>
<td>57</td>
<td>mV</td>
</tr>
<tr>
<td>$V_{SENSE3,(CM)}$</td>
<td>SENSE3 Pins Common Mode Range (BOOST Converter Input Supply Voltage)</td>
<td></td>
<td>2.5</td>
<td>38</td>
<td></td>
<td>V</td>
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</table>

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### ELECTRICAL CHARACTERISTICS

#### SYMBOL | PARAMETER | CONDITIONS | MIN | TYP | MAX | UNITS
--- | --- | --- | --- | --- | --- | ---
**Gate Driver**
| TG1,2 | Pull-Up On-Resistance | | 2.5 | Ω | |
| | Pull-Down On-Resistance | | 1.5 | Ω | |
| BG1,2 | Pull-Up On-Resistance | | 2.4 | Ω | |
| | Pull-Down On-Resistance | | 1.1 | Ω | |
| TG3 | Pull-Up On-Resistance | | 1.2 | Ω | |
| | Pull-Down On-Resistance | | 1.0 | Ω | |
| BG3 | Pull-Up On-Resistance | | 1.2 | Ω | |
| | Pull-Down On-Resistance | | 1.0 | Ω | |

#### TG1,2,3 tr

| Symbol | Parameter | Conditions | Min | TYP | Max | Units
--- | --- | --- | --- | --- | --- | ---
| TG1,2,3 tr | Rise Time | | 25 | ns | |
| | Fall Time | | 16 | ns | |

#### BG1,2,3 tr

| Symbol | Parameter | Conditions | Min | TYP | Max | Units
--- | --- | --- | --- | --- | --- | ---
| BG1,2,3 tr | Rise Time | | 28 | ns | |
| | Fall Time | | 13 | ns | |

#### TG/BG 1tD

| Symbol | Parameter | Conditions | Min | TYP | Max | Units
--- | --- | --- | --- | --- | --- | ---
| TG/BG 1tD | Top Gate Off to Bottom Gate On Delay | | 25 | ns | |
| | Synchronous Switch-On Delay Time | | 30 | ns | |

#### BG/TG 1tD

| Symbol | Parameter | Conditions | Min | TYP | Max | Units
--- | --- | --- | --- | --- | --- | ---
| BG/TG 1tD | Bottom Gate Off to Top Gate On Delay | | 20 | ns | |
| | Top Switch-On Delay Time | | 20 | ns | |

#### tON(MIN)1,2

| Symbol | Parameter | Conditions | Min | TYP | Max | Units
--- | --- | --- | --- | --- | --- | ---
| tON(MIN)1,2 | Buck Minimum On-Time | | 45 | ns | |

#### tON(MIN)3

| Symbol | Parameter | Conditions | Min | TYP | Max | Units
--- | --- | --- | --- | --- | --- | ---
| tON(MIN)3 | Boost Minimum On-Time | | 70 | ns | |

#### INTVCC Linear Regulator

| Symbol | Parameter | Conditions | Min | TYP | Max | Units
--- | --- | --- | --- | --- | --- | ---
| VINTVCC | Internal VCC Voltage | 6V < $V_{BIAS} < 38V$, $V_{EXTVCC} = 0V$, $I_{INTVCC} = 0mA$ | 5.0 | 5.4 | 5.6 | V

#### INTVCC Load Regulation

| Symbol | Parameter | Conditions | Min | TYP | Max | Units
--- | --- | --- | --- | --- | --- | ---
| $V_{LDOVBIAS}$ | INTVCC Load Regulation | $I_{CC} = 0mA$ to $100mA$, $V_{EXTVCC} = 0V$ | 0.8 | 2.5 | % |

#### EXTVCC Load Regulation

| Symbol | Parameter | Conditions | Min | TYP | Max | Units
--- | --- | --- | --- | --- | --- | ---
| $V_{LDOEXTV}$ | EXTVCC Load Regulation | $I_{CC} = 0mA$ to $100mA$, $V_{EXTVCC} = 8.5V$ | 0.8 | 2.5 | % |

#### EXTVCC Switchover Voltage

| Symbol | Parameter | Conditions | Min | TYP | Max | Units
--- | --- | --- | --- | --- | --- | ---
| $V_{EXTVCC}$ | EXTVCC Switchover Voltage | EXTVCC Ramping Positive | 4.5 | 4.7 | % |

#### EXTVCC Hysteresis

| Symbol | Parameter | Conditions | Min | TYP | Max | Units
--- | --- | --- | --- | --- | --- | ---
| $V_{LDOHYS}$ | EXTVCC Hysteresis | | 200 | mV | |

### Oscillator and Phase-Locked Loop

| Symbol | Parameter | Conditions | Min | TYP | Max | Units
--- | --- | --- | --- | --- | --- | ---
| $f_{25K}$ | Programmable Frequency | $R_{REF} = 25k$; PLLIN/MODE = DC Voltage | 0.25 | 0.32 | 0.37 | MHz |
| $f_{65K}$ | Programmable Frequency | $R_{REF} = 65k$; PLLIN/MODE = DC Voltage | 1.18 | MHz |
| $f_{100K}$ | Programmable Frequency | $R_{REF} = 100k$; PLLIN/MODE = DC Voltage | 1.75 | 2.1 | 2.4 | MHz |
| $f_{LOW}$ | Low Fixed Frequency | $V_{FREQ} = 0V$ PLLIN/MODE = DC Voltage | 0.77 | 0.94 | 1.13 | MHz |
| $f_{HIGH}$ | High Fixed Frequency | $V_{FREQ} = INTVCC$ PLLIN/MODE = DC Voltage | 1.2 | 1.44 | 1.75 | MHz |
| $f_{SYNC}$ | Synchronizable Frequency | PLLIN/MODE = External Clock | 0.32 | 2.25 | MHz |
| PLLIN $V_{IH}$ | PLLIN/MODE Input High Level | PLLIN/MODE = External Clock | 2.5 | V |
| PLLIN $V_{IL}$ | PLLIN/MODE Input Low Level | PLLIN/MODE = External Clock | 0.5 | V |
**ELECTRICAL CHARACTERISTICS**

The "" denotes the specifications which apply over the specified operating junction temperature range, otherwise specifications are at $T_A = 25°C$ (Notes 2, 4). $V_{BIAS} = 12V$, $V_{RUN1,2,3} = 5V$, $EXTVCC = 0V$ unless otherwise noted.

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<td>$V_{PGL1}$</td>
<td>PGOOD1 Voltage Low</td>
<td>$I_{PGOOD1} = 2mA$</td>
<td>0.2</td>
<td>0.4</td>
<td></td>
<td>V</td>
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<tr>
<td>$I_{PGOOD1}$</td>
<td>PGOOD1 Leakage Current</td>
<td>$V_{PGOOD1} = 5V$</td>
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<td></td>
<td></td>
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<td>$V_{FG1}$</td>
<td>PGOOD1 Trip Level</td>
<td>$V_{FB1}$ With Respect to Set Regulated Voltage</td>
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<td>–10</td>
<td>–7</td>
<td>%</td>
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<td></td>
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<td>$V_{FB1}$ Ramping Negative</td>
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<td>Hysteresis</td>
<td>2.5</td>
<td></td>
<td></td>
<td>%</td>
</tr>
<tr>
<td></td>
<td></td>
<td>$V_{FB1}$ Ramping Positive</td>
<td>7</td>
<td>10</td>
<td>13</td>
<td>%</td>
</tr>
<tr>
<td>$T_{FG1}$</td>
<td>Delay For Reporting a Fault</td>
<td></td>
<td>40</td>
<td></td>
<td></td>
<td>µs</td>
</tr>
</tbody>
</table>

**OV3 Boost Overvoltage Indicator Output**

<table>
<thead>
<tr>
<th>SYMBOL</th>
<th>PARAMETER Description</th>
<th>CONDITIONS</th>
<th>MIN</th>
<th>TYP</th>
<th>MAX</th>
<th>UNITS</th>
</tr>
</thead>
<tbody>
<tr>
<td>OV3 Voltage Low</td>
<td></td>
<td>$I_{OV3} = 2mA$</td>
<td>0.2</td>
<td>0.4</td>
<td></td>
<td>V</td>
</tr>
<tr>
<td>$I_{OV3}$</td>
<td>OV3 Leakage Current</td>
<td>$V_{OV3} = 5V$</td>
<td>±1</td>
<td></td>
<td></td>
<td>µA</td>
</tr>
<tr>
<td>$V_{OV}$</td>
<td>OV3 Trip Level</td>
<td>$V_{FB3}$ Ramping Positive with Respect to Set Regulated Voltage</td>
<td>6</td>
<td>10</td>
<td>13</td>
<td>%</td>
</tr>
<tr>
<td></td>
<td></td>
<td>Hysteresis</td>
<td>1.5</td>
<td></td>
<td></td>
<td>%</td>
</tr>
</tbody>
</table>

**BOOST3 Charge Pump**

<table>
<thead>
<tr>
<th>SYMBOL</th>
<th>PARAMETER Description</th>
<th>CONDITIONS</th>
<th>MIN</th>
<th>TYP</th>
<th>MAX</th>
<th>UNITS</th>
</tr>
</thead>
<tbody>
<tr>
<td>$I_{BST3}$</td>
<td>BOOST3 Charge Pump Available Output Current</td>
<td>$V_{BOOST3} = 16V; V_{SW3} = 12V; Forced Continuous Mode</td>
<td>65</td>
<td></td>
<td></td>
<td>µA</td>
</tr>
</tbody>
</table>

**Note 1:** Stresses beyond those listed under Absolute Maximum Ratings may cause permanent damage to the device. Exposure to any Absolute Maximum Rating condition for extended periods may affect device reliability and lifetime.

**Note 2:** The LTC7815 is tested under pulsed load conditions such that $T_J = T_A$. The LTC7815E is guaranteed to meet performance specifications from 0°C to 85°C. Specifications over the –40°C to 125°C operating junction temperature range are assured by design, characterization and correlation with statistical process controls. The LTC7815I is guaranteed over the –40°C to 125°C operating junction temperature range and the LTC7815H is guaranteed over the –40°C to 150°C operating junction temperature range. High junction temperatures degrade operating lifetimes; operating lifetime is derated for junction temperatures greater than 125°C. Note that the maximum ambient temperature consistent with these specifications is determined by specific operating conditions in conjunction with board layout, the rated package thermal impedance and other environmental factors. $T_J$ is calculated from the ambient temperature $T_A$ and power dissipation $P_D$ according to the following formula: $T_J = T_A + (P_D \times \theta_{JA})$, where $\theta_{JA} = 34.7°C/W$.

**Note 3:** This IC includes overtemperature protection that is intended to protect the device during momentary overload conditions. The maximum rated junction temperature will be exceeded when this protection is active. Continuous operation above the specified absolute maximum operating junction temperature may impair device reliability or permanently damage the device.

**Note 4:** The LTC7815 is tested in a feedback loop that servos $V_{ITH1,2,3}$ to a specified voltage and measures the resultant $V_{FB}$. The specification at 85°C is not tested in production and is assured by design, characterization and correlation to production testing at other temperatures (125°C for the LTC7815E/LTC7815I, 150°C for the LTC7815H). For the LTC7815I and LTC7815H, the specification at 0°C is not tested in production and is assured by design, characterization and correlation to production testing at –40°C.

**Note 5:** Dynamic supply current is higher due to the gate charge being delivered at the switching frequency. See the Applications Information section.

**Note 6:** Rise and fall times are measured using 10% and 90% levels. Delay times are measured using 50% levels.

**Note 7:** The minimum on-time condition is specified for an inductor peak-to-peak ripple current ≥ 40% of $I_{MAX}$ (See the Minimum On-Time Considerations in the Applications Information section).

**Note 8:** Do not apply a voltage or current source to these pins. They must be connected to capacitive loads only, otherwise permanent damage may occur.
TYPICAL PERFORMANCE CHARACTERISTICS

Efficiency and Power Loss vs Output Current (Buck)

Efficiency vs Output Current (Buck)

Efficiency vs Input Voltage (Buck)

Load Step (Buck) Burst Mode Operation

Load Step (Buck) Pulse-Skipping Mode

Load Step (Buck) Forced Continuous Mode

Inductor Current at Light Load (Buck)

Soft Start-Up (Buck)

Buck Regulated Feedback Voltage vs Temperature

For more information www.linear.com/LTC7815
TYPICAL PERFORMANCE CHARACTERISTICS

Efficiency and Power Loss vs Output Current (Boost)

Efficiency vs Output Current (Boost)

Efficiency vs Input Voltage (Boost)

Load Step (Boost) Burst Mode Operation

Load Step (Boost) Pulse-Skipping Mode

Load Step (Boost) Forced Continuous Mode

Inductor Current at Light Load (Boost)

Soft Start-Up (Boost)

Boost Regulated Feedback Voltage vs Temperature

For more information www.linear.com/LTC7815
TYPICAL PERFORMANCE CHARACTERISTICS

- **INTVCC Line Regulation**

- **INTVCC and EXTVCC vs Load Current**

- **EXTVCC Switchover and INTVCC Voltages vs Temperature**

- **SENSE Pins Total Input Current vs VSENSE Voltage**

- **Buck SENSE- Pin Input Bias Current vs Temperature**

- **Boost SENSE Pin Total Input Current vs Temperature**

- **INPUT VOLTAGE (V)**

  - INTVCC
  - VOUT < INTVCC – 0.5V
  - VOUT > INTVCC + 0.5V

- **SENSE CURRENT (µA)**

  - SENSE1, 2 PINS
  - SENSE3 PINS

- **Maximum Current Sense Threshold vs Duty Cycle**

- **Maximum Current Sense Threshold vs ITH Voltage**

- **TRACK/SS Pull-Up Current vs Temperature**

For more information [www.linear.com/LTC7815](http://www.linear.com/LTC7815)
TYPICAL PERFORMANCE CHARACTERISTICS

**Shutdown Current vs Temperature**

![Graph showing Shutdown Current vs Temperature](image1)

- **VBIAS = 12V**

**ShUTDOWN CURRENT (µA)**

- -75°C: 20 µA
- -50°C: 16 µA
- -25°C: 14 µA
- 0°C: 10 µA
- 25°C: 12 µA
- 50°C: 8 µA
- 75°C: 6 µA
- 100°C: 4 µA
- 125°C: 2 µA
- 150°C: 1 µA

**Oscillator Frequency vs Temperature**

![Graph showing Oscillator Frequency vs Temperature](image2)

- **FREQ = 100kHz**
- **FREQ = INTVCC**
- **FREQ = GND**

**Undervoltage Lockout Threshold vs Temperature**

![Graph showing Undervoltage Lockout Threshold vs Temperature](image3)

**Charge Pump Charging Current vs Operating Frequency**

![Graph showing Charge Pump Charging Current vs Operating Frequency](image4)

**Charge Pump Charging Current vs Switch Voltage**

![Graph showing Charge Pump Charging Current vs Switch Voltage](image5)

**Shutdown (RUN) Threshold vs Temperature**

![Graph showing Shutdown (RUN) Threshold vs Temperature](image6)

- **RUN2.3 RISING**
- **RUN1 RISING**
- **RUN2.3 FALLING**
- **RUN1 FALLING**

**Shutdown (RUN) Threshold vs Temperature**

- **VBOOST3 = 16V**
- **VSW3 = 12V**
- **–55°C**
- **25°C**
- **150°C**

For more information [www.linear.com/LTC7815](http://www.linear.com/LTC7815)
PIN FUNCTIONS

FREQ (Pin 1): The Frequency Control Pin for the Internal VCO. Connecting the pin to GND forces the VCO to a fixed low frequency of 0.94MHz. Connecting the pin to INTVCC forces the VCO to a fixed high frequency of 1.44MHz. Other frequencies between 0.32MHz and 2.25MHz can be programmed using a resistor between FREQ and GND. The resistor and an internal 20µA source current create a voltage used by the internal oscillator to set the frequency.

PLLIN/MODE (Pin 2): External Synchronization Input to Phase Detector and Forced Continuous Mode Input. When an external clock is applied to this pin, the phase-locked loop will force the rising TG1 signal to be synchronized with the rising edge of the external clock, and the regulators operate in forced continuous mode. When not synchronizing to an external clock, this input, which acts on all three controllers, determines how the LTC7815 operates at light loads. Pulling this pin to ground selects Burst Mode operation. An internal 100k resistor to ground also invokes Burst Mode operation when the pin is floated. Tying this pin to INTVCC forces continuous inductor current operation. Tying this pin to a voltage greater than 1.2V and less than INTVCC – 1.3V selects pulse-skipping operation. This can be done by connecting a 100k resistor from this pin to INTVCC.

SGND (Pin 8): Small Signal Ground common to all three controllers, must be routed separately from high current grounds to the common (–) terminals of the CIN capacitors.

RUN1, RUN2, RUN3 (Pins 9, 10, 11): Digital Run Control Inputs for Each Controller. Forcing RUN1 below 1.17V and RUN2/RUN3 below 1.20V shuts down that controller. Forcing all of these pins below 0.7V shuts down the entire LTC7815, reducing quiescent current to approximately 10µA.

OV3 (Pin 17): Overvoltage Open-Drain Logic Output for the Boost Regulator. OV3 is pulled to ground when the voltage on the VFB3 pin is under 110% of its set point, and becomes high impedance when VFB3 goes over 110% of its set point.

INTVCC (Pin 22): Output of the Internal Linear Low Dropout Regulator. The driver and control circuits are powered from this voltage source. Must be decoupled to PGND with a minimum of 4.7µF ceramic or tantalum capacitor.

EXTVCC (Pin 23): External Power Input to an Internal LDO Connected to INTVCC. This LDO supplies INTVCC power, bypassing the internal LDO powered from VBIAS whenever EXTVCC is higher than 4.7V. See EXTVCC Connection in the Applications Information section. Do not float or exceed 14V on this pin.

VBIAS (Pin 24): Main Bias Input Supply Pin. A bypass capacitor should be tied between this pin and the SGND pin.

BG1, BG2, BG3 (Pins 29, 21, 25): High Current Gate Drives for Bottom (Synchronous) N-Channel MOSFETs. Voltage swing at these pins is from ground to INTVCC.

BOOST1, BOOST2, BOOST3 (Pins 30, 20, 26): Bootstrapped Supplies to the Top Side Floating Drivers. Capacitors are connected between the BOOST and SW pins and Schottky diodes are tied between the BOOST and INTVCC pins. Voltage swing at the BOOST pins is from INTVCC to (VIN + INTVCC).

SW1, SW2, SW3 (Pins 31, 19, 28): Switch Node Connections to Inductors.

TG1, TG2, TG3 (Pins 32, 18, 27): High Current Gate Drives for Top N-Channel MOSFETs. These are the outputs of floating drivers with a voltage swing equal to INTVCC superimposed on the switch node voltage SW.

PGOOD1 (Pin 33): Open-Drain Logic Output. PGOOD1 is pulled to ground when the voltage on the VFB1 pin is not within ±10% of its set point.

TRACK/SS1, TRACK/SS2, SS3 (Pins 34, 16, 3): External Tracking and Soft-Start Input. For the buck channels, the LTC7815 regulates the VFB1,2 voltage to the smaller of 0.8V, or the voltage on the TRACK/SS1,2 pin. For the boost channel, the LTC7815 regulates the VFB3 voltage to the smaller of 1.2V, or the voltage on the SS3 pin. An
PIN FUNCTIONS

Internal 5µA pull-up current source is connected to this pin. A capacitor to ground at this pin sets the ramp time to final regulated output voltage. Alternatively, a resistor divider on another voltage supply connected to the TRACK/SS pins of the buck channels allow the LTC7815 to track the other supply during start-up.

ITH1, ITH2, ITH3 (Pins 35, 15, 7): Error Amplifier Outputs and Switching Regulator Compensation Points. Each associated channel’s current comparator trip point increases with this control voltage.

VFB1, VFB2, VFB3 (Pins 36, 14, 6): Receives the remotely sensed feedback voltage for each controller from an external resistive divider across the output.

SENSE1+, SENSE2+, SENSE3+ (Pins 37, 13, 4): The (+) Input to the Differential Current Comparators. The ITH pin voltage and controlled offsets between the SENSE- and SENSE+ pins in conjunction with RSENSE set the current trip threshold. For the boost channel, the SENSE3+ pin supplies current to the current comparator.

SENSE1-, SENSE2-, SENSE3- (Pins 38, 12, 5): The (–) Input to the Differential Current Comparators. When SENSE1,2- for the buck channels is greater than INTVCC, then SENSE1,2- pin supplies current to the current comparator.

PGND (Exposed Pad Pin 39): Driver Power Ground. Connects to the sources of bottom N-channel MOSFETs and the (–) terminal(s) of CIN. The exposed pad must be soldered to the PCB for rated electrical and thermal performance.
**OPERATION** *(Refer to Functional Diagram)*

**Main Control Loop**

The LTC7815 uses a constant frequency, current mode step-down architecture. The two buck controllers, channels 1 and 2, operate 180 degrees out of phase with each other. The boost controller, channel 3, operates in phase with channel 1. During normal operation, the external top MOSFET for the buck channels (the external bottom MOSFET for the boost channel) is turned on when the clock for that channel sets the RS latch, and is turned off when the main current comparator, ICMP, resets the RS latch. The peak inductor current at which ICMP trips and resets the latch is controlled by the voltage on the ITH pin, which is the output of the error amplifier EA. The error amplifier compares the output voltage feedback signal at the VFB pin, (which is generated with an external resistor divider connected across the output voltage, VOUT, to ground) to the internal 0.800V reference voltage for the bucks (1.2V reference voltage for the boost). When the load current increases, it causes a slight decrease in VFB relative to the reference, which causes the EA to increase the ITH voltage until the average inductor current matches the new load current.

After the top MOSFET for the bucks (the bottom MOSFET for the boost) is turned off each cycle, the bottom MOSFET is turned on (the top MOSFET for the boost) until either the inductor current starts to reverse, as indicated by the current comparator IR, or the beginning of the next clock cycle.

**INTVCC/EXTVCC Power**

Power for the top and bottom MOSFET drivers and most other internal circuitry is derived from the INTVCC pin. When the EXTVCC pin is left open or tied to a voltage less than 4.7V, the VBIAS LDO (low dropout linear regulator) supplies 5.4V from VBIAS to INTVCC. If EXTVCC is taken above 4.7V, the VBIAS LDO is turned off and an EXTVCC LDO is turned on. Once enabled, the EXTVCC LDO supplies 5.4V from EXTVCC to INTVCC. Using the EXTVCC pin allows the INTVCC power to be derived from a high efficiency external source such as one of the LTC7815 switching regulator outputs.

Each top MOSFET driver is biased from the floating bootstrap capacitor CB, which normally recharges during each cycle through an external diode when the switch voltage goes low.

For buck channels 1 and 2, if the buck’s input voltage decreases to a voltage close to its output, the loop may enter dropout and attempt to turn on the top MOSFET continuously. The dropout detector detects this and forces the top MOSFET off for a short time every tenth cycle to allow CB to recharge resulting in about 98% duty cycle at 1MHz operation.

**Shutdown and Start-Up (RUN1, RUN2, RUN3 and TRACK/SS1, TRACK/SS2, SS3 Pins)**

The three channels of the LTC7815 can be independently shut down using the RUN1, RUN2 and RUN3 pins. Pulling RUN1 below 1.17V and RUN2/RUN3 below 1.20V shuts down the main control loop for that channel. Pulling all three pins below 0.7V disables all controllers and most internal circuits, including the INTVCC LDOs. In this state, the LTC7815 draws only 10µA of quiescent current.

Releasing a RUN pin allows a small internal current to pull up the pin to enable that controller. The RUN1 pin has a 7µA pull-up current while the RUN2 and RUN3 pins have a smaller 160nA. The 7µA current on RUN1 is designed to be large enough so that the RUN1 pin can be safely floated (to always enable the controller) without worry of condensation or other small board leakage pulling the pin down. This is ideal for always-on applications where one or more controllers are enabled continuously and never shut down.

Each RUN pin may also be externally pulled up or driven directly by logic. When driving a RUN pin with a low impedance source, do not exceed the absolute maximum rating of 8V. Each RUN pin has an internal 11V voltage clamp that allows the RUN pin to be connected through a resistor to a higher voltage (for example, VBIAS), so long as the maximum current in the RUN pin does not exceed 100µA.

The start-up of each channel’s output voltage VOUT is controlled by the voltage on the TRACK/SS pin (TRACK/SS1 for channel 1, TRACK/SS2 for channel 2, SS3 for channel 3). When the voltage on the TRACK/SS pin is less than the 0.8V internal reference for the bucks and the 1.2V internal
reference for the boost, the LTC7815 regulates the $V_{FB}$ voltage to the TRACK/SS pin voltage instead of the corresponding reference voltage. This allows the TRACK/SS pin to be used to program a soft-start by connecting an external capacitor from the TRACK/SS pin to SGND. An internal 5µA pull-up current charges this capacitor creating a voltage ramp on the TRACK/SS pin. As the TRACK/SS voltage rises linearly from 0V to 0.8V/1.2V (and beyond up to INTVCC), the output voltage $V_{OUT}$ rises smoothly from zero to its final value.

Alternatively the TRACK/SS pins for buck channels 1 and 2 can be used to cause the start-up of $V_{OUT}$ to track that of another supply. Typically, this requires connecting to the TRACK/SS pin an external resistor divider from the other supply to ground (see the Applications Information section).

Light Load Current Operation (Burst Mode Operation, Pulse-Skipping, or Continuous Conduction) (PLLIN/MODE Pin)

The LTC7815 can be enabled to enter high efficiency Burst Mode operation, constant frequency pulse-skipping mode or forced continuous conduction mode at low load currents. To select Burst Mode operation, tie the PLLIN/MODE pin to ground. To select forced continuous operation, tie the PLLIN/MODE pin to INTVCC. To select pulse-skipping mode, tie the PLLIN/MODE pin to a DC voltage greater than 1.2V and less than INTVCC – 1.3V.

When a controller is enabled for Burst Mode operation, the minimum peak current in the inductor is set to approximately 25% of the maximum sense voltage (30% for the boost) even though the voltage on the $I_{TH}$ pin indicates a lower value. If the average inductor current is higher than the load current, the error amplifier EA will decrease the voltage on the $I_{TH}$ pin. When the $I_{TH}$ voltage drops below 0.425V, the internal sleep signal goes high (enabling sleep mode) and both external MOSFETs are turned off. The $I_{TH}$ pin is then disconnected from the output of the EA and parked at 0.450V.

In sleep mode, much of the internal circuitry is turned off, reducing the quiescent current that the LTC7815 draws. If channel 1 is in sleep mode and the other two are shut down, the LTC7815 draws only 28µA of quiescent current. If channels 1 and 3 are in sleep mode and channel 2 is shut down, it draws only 33µA of quiescent current. If all three controllers are enabled in sleep mode, the LTC7815 draws only 38µA of quiescent. In sleep mode, the load current is supplied by the output capacitor. As the output voltage decreases, the EA’s output begins to rise. When the output voltage drops enough, the $I_{TH}$ pin is reconnected to the output of the EA, the sleep signal goes low, and the controller resumes normal operation by turning on the top external MOSFET on the next cycle of the internal oscillator.

When a controller is enabled for Burst Mode operation, the inductor current is not allowed to reverse. The reverse current comparator (IR) turns off the bottom external MOSFET (the top external MOSFET for the boost) just before the inductor current reaches zero, preventing it from reversing and going negative. Thus, the controller operates in discontinuous operation.

In forced continuous operation or clocked by an external clock source to use the phase-locked loop (see the Frequency Selection and Phase-Locked Loop section), the inductor current is allowed to reverse at light loads or under large transient conditions. The peak inductor current is determined by the voltage on the $I_{TH}$ pin, just as in normal operation. In this mode, the efficiency at light loads is lower than in Burst Mode operation. However, continuous operation has the advantage of lower output voltage ripple and less interference to audio circuitry. In forced continuous mode, the output ripple is independent of load current.

When the PLLIN/MODE pin is connected for pulse-skipping mode, the LTC7815 operates in PWM pulse-skipping mode at light loads. In this mode, constant frequency operation is maintained down to approximately 1% of designed maximum output current. At very light loads, the current comparator ICMP may remain tripped for several cycles and force the external top MOSFET to stay off for the same number of cycles (i.e., skipping pulses). The inductor current is not allowed to reverse (discontinuous operation). This mode, like forced continuous operation, exhibits low output ripple as well as low audio noise and reduced RF interference as compared to Burst Mode operation. It provides higher low current efficiency than forced continuous mode, but not nearly as high as Burst Mode operation.
OPERATION

Frequency Selection and Phase-Locked Loop (FREQ and PLLIN/MODE Pins)

The selection of switching frequency is a tradeoff between efficiency and component size. Low frequency operation increases efficiency by reducing MOSFET switching losses, but requires larger inductance and/or capacitance to maintain low output ripple voltage.

The switching frequency of the LTC7815’s controllers can be selected using the FREQ pin.

If the PLLIN/MODE pin is not being driven by an external clock source, the FREQ pin can be tied to SGND, tied to INTVCC, or programmed through an external resistor. Tying FREQ to SGND selects 0.94MHz while tying FREQ to INTVCC selects 1.44MHz. Placing a resistor between FREQ and SGND allows the frequency to be programmed between 0.32MHz and 2.25MHz.

A phase-locked loop (PLL) is available on the LTC7815 to synchronize the internal oscillator to an external clock source that is connected to the PLLIN/MODE pin. The LTC7815’s phase detector adjusts the voltage (through an internal lowpass filter) of the VCO input to align the turn-on of controller 1’s external top MOSFET to the rising edge of the synchronizing signal. Thus, the turn-on of controller 2’s external top MOSFET is 180 degrees out of phase to the rising edge of the external clock source.

The VCO input voltage is pre-biased to the operating frequency set by the FREQ pin before the external clock is applied. If prebiased near the external clock frequency, the PLL loop only needs to make slight changes to the VCO input in order to synchronize the rising edge of the external clock’s to the rising edge of TG1. The ability to pre-bias the loop filter allows the PLL to lock in rapidly without deviating far from the desired frequency.

The typical capture range of the LTC7815’s phase-locked loop is from approximately 0.3MHz to 2.3MHz, with a guarantee over all manufacturing variations to be between 0.32MHz and 2.25MHz. In other words, the LTC7815’s PLL is guaranteed to lock to an external clock source whose frequency is between 0.32MHz and 2.25MHz.

The typical input clock thresholds on the PLLIN/MODE pin are 1.6V (rising) and 1.1V (falling). It is recommended that the external clock source swings from ground (0V) to at least 2.5V.

Boost Controller Operation When VIN > VOUT

When the input voltage to the boost channel rises above its regulated VOUT voltage, the controller can behave differently depending on the mode, inductor current and VIN voltage. In forced continuous mode, the loop works to keep the top MOSFET on continuously once VIN rises above VOUT. An internal charge pump delivers current to the boost capacitor from the BOOST3 pin to maintain a sufficiently high TG voltage. (The amount of current the charge pump can deliver is characterized by two curves in the Typical Performance Characteristics section.)

In pulse-skipping mode, if VIN is between 100% and 110% of the regulated VOUT voltage, TG3 turns on if the inductor current rises above approximately 3% of the programmed Ilim current. If the part is programmed in Burst Mode operation under this same VIN window, then TG3 turns on at the same threshold current as long as the chip is awake (one of the buck channels is awake and switching). If both buck channels are asleep or shut down in this VIN window, then TG3 will remain off regardless of the inductor current.

If VIN rises above 110% of the regulated VOUT voltage in any mode, the controller turns on TG3 regardless of the inductor current. In Burst Mode operation, however, the internal charge pump turns off if the entire chip is asleep (the two buck channels are asleep or shut down). Without the charge pump, there would be nothing to prevent the boost capacitor from discharging, resulting in an insufficient TG voltage needed to keep the top MOSFET completely on. The charge pump turns back on when the chip wakes up, and it remains on as long as one of the buck channels is actively switching.

Boost Controller at Low SENSE Pin Common Voltage

The current comparator of the boost controller is powered directly from the SENSE3+ pin and can operate to voltages as low as 2.5V. Since this is lower than the VBias UVLO of the chip, VBias can be connected to the output of the boost controller, as illustrated in the typical application circuit in Figure 9. This allows the boost controller to
handle input voltage transients down to 2.5V while maintaining output voltage regulation. If the SENSE\textsuperscript{3+} rises back above 2.5V, the SS3 pin will be released initiating a new soft-start sequence.

**Buck Controller Output Overvoltage Protection**

The two buck channels have an overvoltage comparator that guards against transient overshoots as well as other more serious conditions that may overvoltage their outputs. When the $V_{FB1,2}$ pin rises by more than 10% above its regulation point of 0.800V, the top MOSFET is turned off and the bottom MOSFET is turned on until the overvoltage condition is cleared.

**Channel 1 Power Good (PGOOD1)**

Channel 1 has a PGOOD1 pin that is connected to an open drain of an internal N-channel MOSFET. The MOSFET turns on and pulls the PGOOD1 pin low when the $V_{FB1}$ pin voltage is not within ±10% of the 0.8V reference voltage for the buck channel. The PGOOD1 pin is also pulled low when the RUN1 pin is low (shut down). When the $V_{FB1}$ pin voltage is within the ±10% requirement, the MOSFET is turned off and the pin is allowed to be pulled up by an external resistor to a source no greater than 6V.

**Boost Overvoltage Indicator (OV3)**

The OV3 pin is an overvoltage indicator that signals whether the output voltage of the channel 3 boost controller goes over its programmed regulated voltage. The pin is connected to an open drain of an internal N-channel MOSFET. The MOSFET turns on and pulls the OV3 pin low when the $V_{FB3}$ pin voltage is less than 110% of the 1.2V reference voltage for the boost channel. The OV3 pin is also pulled low when the RUN3 pin is low (shut down). When the $V_{FB3}$ pin voltage goes higher than 110% of the 1.2V reference, the MOSFET is turned off and the pin is allowed to be pulled up by an external resistor to a source no greater than 6V.

**Buck Foldback Current**

When the buck output voltage falls to less than 70% of its nominal level, foldback current limiting is activated, progressively lowering the peak current limit in proportion to the severity of the overcurrent or short-circuit condition. Foldback current limiting is disabled during the soft-start interval (as long as the $V_{FB}$ voltage is keeping up with the TRACK/SS1,2 voltage). There is no foldback current limiting for the boost channel.
APPLICATIONS INFORMATION

The Typical Application on the first page is a basic LTC7815 application circuit. LTC7815 can be configured to use either DCR (inductor resistance) sensing or low value resistor sensing. The choice between the two current sensing schemes is largely a design trade-off between cost, power consumption, and accuracy. DCR sensing is becoming popular because it saves expensive current sensing resistors and is more power efficient, especially in high current applications. However, current sensing resistors provide the most accurate current limits for the controller. Other external component selection is driven by the load requirement, and begins with the selection of \( R_{\text{SENSE}} \) (if \( R_{\text{SENSE}} \) is used) and inductor value. Next, the power MOSFETs and Schottky diodes are selected. Finally, input and output capacitors are selected.

**SENSE+ and SENSE− Pins**

The SENSE+ and SENSE− pins are the inputs to the current comparators.

*Buck Controllers (SENSE1+/SENSE1−, SENSE2+/SENSE2−):* The common mode voltage range on these pins is 0V to 28V (absolute maximum), enabling the LTC7815 to regulate buck output voltages up to a nominal 24V (allowing margin for tolerances and transients). The SENSE+ pin is high impedance drawing less than \( \approx 1\mu A \). This high impedance allows the current comparators to be used in inductor DCR sensing. The impedance of the SENSE− pin changes depending on the common mode voltage. When SENSE− is less than \( \text{INTV}_{\text{CC}}−0.5V \), it is high impedance, drawing less than \( \approx 1\mu A \). When SENSE− is above \( \text{INTV}_{\text{CC}}+0.5V \), a higher current (\( \approx 700\mu A \)) flows into the pin. Between \( \text{INTV}_{\text{CC}}−0.5V \) and \( \text{INTV}_{\text{CC}}+0.5V \), the current transitions from the smaller current to the higher current.

*Boost Controller (SENSE3+/SENSE3−):* The common mode input range for these pins is 2.5V to 38V, allowing the boost converter to operate from inputs over this full range. The SENSE3+ pin also provides power to the current comparator and draws about 170\( \mu A \) during normal operation (when not shut down or asleep in Burst Mode operation). There is a small bias current of less than 1\( \mu A \) that flows out of the SENSE3− pin. This high impedance on the SENSE3− pin allows the current comparator to be used in inductor DCR sensing.

Filter components mutual to the sense lines should be placed close to the LTC7815, and the sense lines should run close together to a Kelvin connection underneath the current sense element (shown in Figure 1). Sensing current elsewhere can effectively add parasitic inductance and capacitance to the current sense element, degrading the information at the sense terminals and making the programmed current limit unpredictable. If DCR sensing is used (Figure 2b), sense resistor \( R_1 \) should be placed close to the switching node, to prevent noise from coupling into sensitive small-signal nodes.

![Figure 1. Sense Lines Placement with Inductor or Sense Resistor](image-url)

**Low Value Resistor Current Sensing**

A typical sensing circuit using a discrete resistor is shown in Figure 2a. \( R_{\text{SENSE}} \) is chosen based on the required output current.

The current comparators have a maximum threshold \( V_{\text{SENSE(MAX)}} \) of 50mV. The current comparator threshold sets the peak of the inductor current, yielding a maximum average output current, \( I_{\text{MAX}} \), equal to the peak value less half the peak-to-peak ripple current, \( \Delta I_{\text{L}} \). To calculate the sense resistor value, use the equation:

\[
R_{\text{SENSE}} = \frac{V_{\text{SENSE(MAX)}}}{I_{\text{MAX}} + \frac{\Delta I_{\text{L}}}{2}}
\]

When using the buck controllers in very low dropout conditions, the maximum output current level will be reduced due to the internal compensation required to meet stability criterion for buck regulators operating at greater than 50% duty factor. A curve is provided in the Typical Performance Characteristics section to estimate this reduction in peak output current level depending upon the operating duty factor.
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**Inductor DCR Sensing**

For applications requiring the highest possible efficiency at high load currents, the LTC7815 is capable of sensing the voltage drop across the inductor DCR, as shown in Figure 2b. The DCR of the inductor represents the small amount of DC winding resistance of the copper, which can be less than 1mΩ for today’s low value, high current inductors. In a high current application requiring such an inductor, conduction loss through a sense resistor would cost several points of efficiency compared to DCR sensing.

If the external R1||R2 • C1 time constant is chosen to be exactly equal to the L/DCR time constant, the voltage drop across the external capacitor is equal to the drop across the inductor DCR multiplied by R2/(R1 + R2). R2 scales the voltage across the sense terminals for applications where the DCR is greater than the target sense resistor value. To properly dimension the external filter components, the DCR of the inductor must be known. It can be measured using a good RLC meter, but the DCR tolerance is not always the same and varies with temperature; consult the manufacturers’ data sheets for detailed information.

Using the inductor ripple current value from the Inductor Value Calculation section, the target sense resistor value is:

\[
R_{\text{EQUIV}} = \frac{V_{\text{SENSE(MAX)}}}{I_{\text{MAX}}} + \frac{\Delta I}{2}
\]

To ensure that the application will deliver full load current over the full operating temperature range, determine RSENSE(EQUIV), keeping in mind that the maximum current sense threshold (VSENSE(MAX)) for the LTC7815 is fixed at 50mV.

Next, determine the DCR of the inductor. Where provided, use the manufacturer’s maximum value, usually given at 20°C. Increase this value to account for the temperature coefficient of resistance, which is approximately 0.4%/°C. A conservative value for TL(MAX) is 100°C.

To scale the maximum inductor DCR to the desired resistor value, use the divider ratio:

\[
R_D = \frac{R_{\text{SENSE(EQUIV)}}}{DCR_{\text{MAX}} \cdot T_{L\text{(MAX)}}}
\]

C1 is usually selected to be in the range of 0.1μF to 0.47μF. This forces R1||R2 to around 2k, reducing error that might have been caused by the SENSE+ pin’s ±1μA current.

The equivalent resistance R1||R2 is scaled to the room temperature inductance and maximum DCR:

\[
R_1 || R_2 = \frac{L}{(DCR \text{ at } 20°C) \cdot C_1}
\]
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The sense resistor values are:

\[ R_1 = \frac{R_1 \parallel R_2}{R_D}; \quad R_2 = \frac{R_1 \cdot R_D}{1 - R_D} \]

The maximum power loss in R1 is related to duty cycle. For the buck controllers, the maximum power loss will occur in continuous mode at the maximum input voltage:

\[ P_{LOSS \, R1} = \frac{(V_{IN}(MAX) - V_{OUT}) \cdot V_{OUT}}{R_1} \]

For the boost controller, the maximum power loss in R1 will occur in continuous mode at \( V_{IN} = 1/2 \cdot V_{OUT} \):

\[ P_{LOSS \, R1} = \frac{(V_{OUT}(MAX) - V_{IN}) \cdot V_{IN}}{R_1} \]

Ensure that R1 has a power rating higher than this value. If high efficiency is necessary at light loads, consider this power loss when deciding whether to use DCR sensing or sense resistors. Light load power loss can be modestly higher with a DCR network than with a sense resistor, due to the extra switching losses incurred through R1. However, DCR sensing eliminates a sense resistor, reduces conduction losses and provides higher efficiency at heavy loads. Peak efficiency is about the same with either method.

Inductor Value Calculation

The operating frequency and inductor selection are interrelated in that higher operating frequencies allow the use of smaller inductor and capacitor values. So why would anyone ever choose to operate at lower frequencies with larger components? The answer is efficiency. A higher frequency generally results in lower efficiency because of MOSFET gate charge losses. In addition to this basic trade-off, the effect of inductor value on ripple current and low current operation must also be considered.

The inductor value has a direct effect on ripple current. The inductor ripple current \( \Delta I_L \) decreases with higher inductance or frequency. For the buck controllers, \( \Delta I_L \) increases with higher \( V_{IN} \):

\[ \Delta I_L = \frac{1}{(f)(L)} \left( V_{OUT} \right) \left( 1 - \frac{V_{OUT}}{V_{IN}} \right) \]

For the boost controller, the inductor ripple current \( \Delta I_L \) increases with higher \( V_{OUT} \):

\[ \Delta I_L = \frac{1}{(f)(L)} \left( V_{IN} \right) \left( 1 - \frac{V_{IN}}{V_{OUT}} \right) \]

Accepting larger values of \( \Delta I_L \) allows the use of low inductances, but results in higher output voltage ripple and greater core losses. A reasonable starting point for setting ripple current is \( \Delta I_L = 0.3(I_{MAX}) \). The maximum \( \Delta I_L \) occurs at the maximum input voltage for the bucks and \( V_{IN} = 1/2 \cdot V_{OUT} \) for the boost.

The inductor value also has secondary effects. The transition to Burst Mode operation begins when the average inductor current required results in a peak current below 25% of the current limit (30% for the boost) determined by \( R_{SENSE} \). Lower inductor values (higher \( \Delta I_L \)) will cause this to occur at lower load currents, which can cause a dip in efficiency in the upper range of low current operation. In Burst Mode operation, lower inductance values will cause the burst frequency to decrease.

Inductor Core Selection

Once the value for L is known, the type of inductor must be selected. High efficiency converters generally cannot afford the core loss found in low cost powdered iron cores, forcing the use of more expensive ferrite or molypermalloy cores. Actual core loss is independent of core size for a fixed inductor value, but it is very dependent on inductance selected. As inductance increases, core losses go down. Unfortunately, increased inductance requires more turns of wire and therefore copper losses will increase.

Ferrite designs have very low core loss and are preferred at high switching frequencies, so design goals can concentrate on copper loss and preventing saturation. Ferrite
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core material saturates “hard,” which means that inductance collapses abruptly when the peak design current is exceeded. This results in an abrupt increase in inductor ripple current and consequent output voltage ripple. Do not allow the core to saturate!

Power MOSFET and Schottky Diode
(Optional) Selection

Two external power MOSFETs must be selected for each controller in the LTC7815: one N-channel MOSFET for the top switch (main switch for the buck, synchronous for the boost), and one N-channel MOSFET for the bottom switch (main switch for the boost, synchronous for the buck).

The peak-to-peak drive levels are set by the INTVCC voltage. This voltage is typically 5.4V during start-up (see EXTVCC Pin Connection). Consequently, logic-level threshold MOSFETs must be used in most applications. Pay close attention to the BVdss specification for the MOSFETs as well; many of the logic level MOSFETs are limited to 30V or less.

Selection criteria for the power MOSFETs include the on-resistance $R_{DS(ON)}$, Miller capacitance $C_{MILLER}$, input voltage and maximum output current. Miller capacitance, $C_{MILLER}$, can be approximated from the gate charge curve usually provided on the MOSFET manufacturers’ data sheet. $C_{MILLER}$ is equal to the increase in gate charge along the horizontal axis while the curve is approximately flat divided by the specified change in $V_{DS}$. This result is then multiplied by the ratio of the application applied $V_{DS}$ to the gate charge curve specified $V_{DS}$. When the IC is operating in continuous mode the duty cycles for the top and bottom MOSFETs are given by:

- **Buck Main Switch Duty Cycle**
  $$\frac{V_{OUT}}{V_{IN}}$$
- **Buck Sync Switch Duty Cycle**
  $$\frac{V_{IN} - V_{OUT}}{V_{IN}}$$
- **Boost Main Switch Duty Cycle**
  $$\frac{V_{OUT} - V_{IN}}{V_{OUT}}$$
- **Boost Sync Switch Duty Cycle**
  $$\frac{V_{IN}}{V_{OUT}}$$

The MOSFET power dissipations at maximum output current are given by:

$$P_{MAIN_BUCK} = \frac{V_{OUT}}{V_{IN}} \left(\frac{I_{OUT(MAX)}}{2}\right)^2 \left(1 + \delta\right)R_{DS(ON)} + \left(\frac{V_{IN}}{2}\right)^2 \left(\frac{I_{OUT(MAX)}}{V_{IN}}\right)^2 \left(1 + \delta\right)R_{DS(ON)}$$

$$P_{SYNC_BUCK} = \frac{V_{IN} - V_{OUT}}{V_{IN}} \left(\frac{I_{OUT(MAX)}}{2}\right)^2 \left(1 + \delta\right)R_{DS(ON)}$$

$$P_{MAIN_BOOST} = \frac{V_{OUT} - V_{IN}}{V_{IN}} \left(\frac{I_{OUT(MAX)}}{V_{OUT}}\right)^2 \left(1 + \delta\right)R_{DS(ON)}$$

$$P_{SYNC_BOOST} = \frac{V_{IN}}{V_{OUT}} \left(\frac{I_{OUT(MAX)}}{V_{OUT}}\right)^2 \left(1 + \delta\right)R_{DS(ON)}$$

where $\delta$ is the temperature dependency of $R_{DS(ON)}$ and $R_{DR}$ (approximately 2Ω) is the effective driver resistance at the MOSFET’s Miller threshold voltage. $V_{THMIN}$ is the typical MOSFET minimum threshold voltage.

Both MOSFETs have $I^2R$ losses while the main N-channel equations for the buck and boost controllers include an additional term for transition losses, which are highest at high input voltages for the bucks and low input voltages for the boost. For $V_{IN} < 20V$ (high $V_{IN}$ for the boost) the high current efficiency generally improves with larger MOSFETs, while for $V_{IN} > 20V$ (low $V_{IN}$ for the boost) the transition losses rapidly increase to the point that the use of a higher $R_{DS(ON)}$ device with lower $C_{MILLER}$ actually
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provides higher efficiency. The synchronous MOSFET losses for the buck controllers are greatest at high input voltage when the top switch duty factor is low or during a short-circuit when the synchronous switch is on close to 100% of the period. The synchronous MOSFET losses for the boost controller are greatest when the input voltage approaches the output voltage or during an overvoltage event when the synchronous switch is on 100% of the period.

The term \((1 + \zeta)\) is generally given for a MOSFET in the form of a normalized \(R_{DS(ON)}\) vs Temperature curve, but \(\zeta = 0.005/°C\) can be used as an approximation for low voltage MOSFETs.

A Schottky diode can be inserted in parallel with the synchronous MOSFET to conduct during the dead-time between the conduction of the two power MOSFETs. This prevents the body diode of the synchronous MOSFET from turning on, storing charge during the dead-time and requiring a reverse recovery period that could cost as much as 3% in efficiency at high \(V_{IN}\). A 1A to 3A Schottky is generally a good compromise for both regions of operation due to the relatively small average current. Larger diodes result in additional transition losses due to their larger junction capacitance.

Boost \(C_{IN}, C_{OUT}\) Selection

The input ripple current in a boost converter is relatively low (compared with the output ripple current), because this current is continuous. The boost input capacitor \(C_{IN}\) voltage rating should comfortably exceed the maximum input voltage. Although ceramic capacitors can be relatively tolerant of overvoltage conditions, aluminum electrolytic capacitors are not. Be sure to characterize the input voltage for any possible overvoltage transients that could apply excess stress to the input capacitors.

The value of \(C_{IN}\) is a function of the source impedance, and in general, the higher the source impedance, the higher the required input capacitance. The required amount of input capacitance is also greatly affected by the duty cycle. High output current applications that also experience high duty cycles can place great demands on the input supply, both in terms of DC current and ripple current.

In a boost converter, the output has a discontinuous current, so \(C_{OUT}\) must be capable of reducing the output voltage ripple. The effects of ESR (equivalent series resistance) and the bulk capacitance must be considered when choosing the right capacitor for a given output ripple voltage. The steady ripple due to charging and discharging the bulk capacitance is given by:

\[
\text{Ripple} = \frac{I_{OUT(MAX)} \cdot (V_{OUT} - V_{IN(MIN)})}{C_{OUT} \cdot V_{OUT} \cdot f}
\]

where \(C_{OUT}\) is the output filter capacitor.

The steady ripple due to the voltage drop across the ESR is given by:

\[
\Delta V_{ESR} = I_{L(MAX)} \cdot ESR
\]

Multiple capacitors placed in parallel may be needed to meet the ESR and RMS current handling requirements. Dry tantalum, special polymer, aluminum electrolytic and ceramic capacitors are all available in surface mount packages. Ceramic capacitors have excellent low ESR characteristics but can have a high voltage coefficient. Capacitors are now available with low ESR and high ripple current ratings such as OS-CON and POSCAP.

Buck \(C_{IN}, C_{OUT}\) Selection

The selection of \(C_{IN}\) for the two buck controllers is simplified by the 2-phase architecture and its impact on the worst-case RMS current drawn through the input network (battery/fuse/capacitor). It can be shown that the worst-case capacitor RMS current occurs when only one controller is operating. The controller with the highest \((V_{OUT})(I_{OUT})\) product needs to be used in the formula shown in Equation (1) to determine the maximum RMS capacitor current requirement. Increasing the output current drawn from the other controller will actually decrease the input RMS ripple current from its maximum value. The out-of-phase technique typically reduces the input
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capacitor’s RMS ripple current by a factor of 30% to 70% when compared to a single phase power supply solution.

In continuous mode, the source current of the top MOSFET is a square wave of duty cycle \( \frac{V_{OUT}}{V_{IN}} \). To prevent large voltage transients, a low ESR capacitor sized for the maximum RMS current of one channel must be used. The maximum RMS capacitor current is given by:

\[
C_{IN \text{ Required}} \approx \frac{I_{MAX}}{V_{IN}} \left[ \left( \frac{V_{OUT}}{} \right) \left( V_{IN} - V_{OUT} \right) \right]^{1/2} \tag{1}
\]

This formula has a maximum at \( V_{IN} = 2V_{OUT} \), where \( I_{RMS} = \frac{1}{2}I_{OUT} \). This simple worst-case condition is commonly used for design because even significant deviations do not offer much relief. Note that capacitor manufacturers’ ripple current ratings are often based on only 2000 hours of life. This makes it advisable to further derate the capacitor, or to choose a capacitor rated at a higher temperature than required. Several capacitors may be paralleled to meet size or height requirements in the design. Due to the high operating frequency of the LTC7815, ceramic capacitors can also be used for \( C_{IN} \). Always consult the manufacturer if there is any question.

The benefit of the LTC7815 2-phase operation can be calculated by using Equation (1) for the higher power controller and then calculating the loss that would have resulted if both controller channels switched on at the same time. The total RMS power lost is lower when both controllers are operating due to the reduced overlap of current pulses required through the input capacitor’s ESR. This is why the input capacitor’s requirement calculated above for the worst-case controller is adequate for the dual controller design. Also, the input protection fuse resistance, battery resistance, and PC board trace resistance losses are also reduced due to the reduced peak currents in a 2-phase system. The overall benefit of a multiphase design will only be fully realized when the source impedance of the power supply/battery is included in the efficiency testing. The drains of the top MOSFETs should be placed within 1cm of each other and share a common \( C_{IN} \). Separating the drains and \( C_{IN} \) may produce undesirable voltage and current resonances at \( V_{IN} \).

A small (0.1µF to 1µF) bypass capacitor between the chip \( V_{IN} \) pin and ground, placed close to the LTC7815, is also suggested. A small (1Ω to 10Ω) resistor placed between \( C_{IN} \) (C1) and the \( V_{IN} \) pin provides further isolation between the two channels.

The selection of \( C_{OUT} \) is driven by the effective series resistance (ESR). Typically, once the ESR requirement is satisfied, the capacitance is adequate for filtering. The output ripple (\( \Delta V_{OUT} \)) is approximated by:

\[
\Delta V_{OUT} \approx \Delta I \left( \text{ESR} + \frac{1}{8fC_{OUT}} \right)
\]

where \( f \) is the operating frequency, \( C_{OUT} \) is the output capacitance and \( \Delta I \) is the ripple current in the inductor. The output ripple is highest at maximum input voltage since \( \Delta I \) increases with input voltage.

Setting Output Voltage

The LTC7815 output voltages are each set by an external feedback resistor divider carefully placed across the output, as shown in Figure 3. The regulated output voltages are determined by:

\[
V_{OUT, BUCK} = 0.8V \left( 1 + \frac{R_B}{R_A} \right)
\]

\[
V_{OUT, BOOST} = 1.2V \left( 1 + \frac{R_B}{R_A} \right)
\]

To improve the frequency response, a feedforward capacitor, \( C_{FF} \), may be used. Great care should be taken to route the \( V_{FB} \) line away from noise sources, such as the inductor or the SW line.
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Tracking and Soft-Start
(TRACK/SS1, TRACK/SS2, SS3 Pins)

The start-up of each OUT is controlled by the voltage on the respective TRACK/SS pin (TRACK/SS1 for channel 1, TRACK/SS2 for channel 2, SS3 for channel 3). When the voltage on the TRACK/SS pin is less than the internal 0.8V reference (1.2V reference for the boost channel), the LTC7815 regulates the VFB pin voltage to the voltage on the TRACK/SS pin instead of the internal reference. Likewise, the TRACK/SS pin for the buck channels can be used to program an external soft-start function or to allow OUT to track another supply during start-up.

Soft-start is enabled by simply connecting a capacitor from the TRACK/SS pin to ground, as shown in Figure 4. An internal 5µA current source charges the capacitor, providing a linear ramping voltage at the TRACK/SS pin. The LTC7815 will regulate the VFB pin (and hence OUT) according to the voltage on the TRACK/SS pin, allowing OUT to rise smoothly from 0V to its final regulated value. The total soft-start time will be approximately:

\[
\begin{align*}
t_{\text{SS,Buck}} &= C_{\text{SS}} \cdot \frac{0.8\text{V}}{5\mu\text{A}} \\
t_{\text{SS,Boost}} &= C_{\text{SS}} \cdot \frac{1.2\text{V}}{5\mu\text{A}}
\end{align*}
\]

Alternatively, the TRACK/SS1 and TRACK/SS2 pins for the two buck controllers can be used to track two (or more) supplies during start-up, as shown qualitatively in Figures 5a and 5b. To do this, a resistor divider should be connected from the master supply (VX) to the TRACK/SS pin of the slave supply (VOUT), as shown in Figure 6. During start-up VOUT will track VX according to the ratio set by the resistor divider:

\[
\frac{V_X}{V_{\text{OUT}}} = \frac{R_A}{R_{\text{trackA}}} + \frac{R_{\text{trackB}}}{R_A + R_B}
\]

For coincident tracking (VOUT = VX during start-up),

\[
\begin{align*}
R_A &= R_{\text{trackA}} \\
R_B &= R_{\text{trackB}}
\end{align*}
\]
INTVCC Regulators

The LTC7815 features two separate internal P-channel low dropout linear regulators (LDO) that supply power at the INTVCC pin from either the VBIAS supply pin or the EXTVCC pin depending on the connection of the EXTVCC pin. INTVCC powers the gate drivers and much of the LTC7815’s internal circuitry. The VBIAS LDO and the EXTVCC LDO regulate INTVCC to 5.4V. Each of these must be bypassed to ground with a minimum of 4.7µF ceramic capacitor. No matter what type of bulk capacitor is used, an additional 1µF ceramic capacitor placed directly adjacent to the INTVCC and PGND IC pins is highly recommended. Good bypassing is needed to supply the high transient currents required by the MOSFET gate drivers and to prevent interaction between the channels.

High input voltage applications in which large MOSFETs are being driven at high frequencies may cause the maximum junction temperature rating for the LTC7815 to be exceeded. The INTVCC current, which is dominated by the gate charge current, may be supplied by either the VBIAS LDO or the EXTVCC LDO. When the voltage on the EXTVCC pin is less than 4.7V, the VBIAS LDO is enabled. Power dissipation for the IC in this case is highest and is equal to VBIAS • IINTVCC. The gate charge current is dependent on operating frequency as discussed in the Efficiency Considerations section. The junction temperature can be estimated by using the equations given in Note 2 of the Electrical Characteristics. For example, the LTC7815 INTVCC current is limited to less than 40mA from a 40V supply when not using the EXTVCC supply at a 70°C ambient temperature:

\[
T_J = 70°C + (40mA)(40V)(34.7°C/W) = 125°C
\]

To prevent the maximum junction temperature from being exceeded, the input supply current must be checked while operating in continuous conduction mode (PLLIN/MODE = INTVCC) at maximum VIN.

When the voltage applied to EXTVCC rises above 4.7V, the VBIAS LDO is turned off and the EXTVCC LDO is enabled. The EXTVCC LDO remains on as long as the voltage applied to EXTVCC remains above 4.5V. The EXTVCC LDO attempts to regulate the INTVCC voltage to 5.4V, so while EXTVCC is less than 5.4V, the LDO is in dropout and the INTVCC voltage is approximately equal to EXTVCC. When EXTVCC is greater than 5.4V, up to an absolute maximum of 14V, INTVCC is regulated to 5.4V.

Using the EXTVCC LDO allows the MOSFET driver and control power to be derived from one of the LTC7815’s switching regulator outputs (4.7V ≤ VOUT ≤ 14V) during normal operation and from the VBIAS LDO when the output is out of regulation (e.g., start-up, short-circuit). If more current is required through the EXTVCC LDO than is specified, an external Schottky diode can be added between the EXTVCC and INTVCC pins. In this case, do not apply more than 6V to the EXTVCC pin and make sure that EXTVCC ≤ VBIAS.

Significant efficiency and thermal gains can be realized by powering INTVCC from the buck output, since the VIN current resulting from the driver and control currents will be scaled by a factor of (Duty Cycle)/(Switcher Efficiency). For 5V to 14V regulator outputs, this means connecting the EXTVCC pin directly to VOUT. Tying the EXTVCC pin to a 8.5V supply reduces the junction temperature in the previous example from 125°C to:

\[
T_J = 70°C + (40mA)(8.5V)(34.7°C/W) = 82°C
\]

However, for 3.3V and other low voltage outputs, additional circuitry is required to derive INTVCC power from the output.

The following list summarizes the three possible connections for EXTVCC:

1. EXTVCC grounded. This will cause INTVCC to be powered from the internal 5.4V regulator resulting in an efficiency penalty of up to 10% at high input voltages.
2. EXTVCC connected directly to the output voltage of one of the buck regulators. This is the normal connection for a 5V to 14V regulator and provides the highest efficiency.
3. EXTVCC connected to an external supply. If an external supply is available in the 5V to 14V range, it may be used to power EXTVCC providing it is compatible with the MOSFET gate drive requirements. Ensure that EXTVCC ≤ VBIAS.
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Topside MOSFET Driver Supply (C_B, D_B)

External bootstrap capacitors C_B connected to the BOOST pins supply the gate drive voltages for the topside MOSFETs. Capacitor C_B in the Functional Diagram is charged though external diode D_B from INTVCC when the SW pin is low. When one of the topside MOSFETs is to be turned on, the driver places the C_B voltage across the gate-source of the desired MOSFET. This enhances the MOSFET and turns on the topside switch. The switch node voltage, SW, rises to \( V_{IN} \) for the buck channels (\( V_{OUT} \) for the boost channel) and the BOOST pin follows. With the topside MOSFET on, the boost voltage is above the input supply: \( V_{BOOT} = V_{IN} + V_{INTVCC} \) (\( V_{BOOT} = V_{OUT} + V_{INTVCC} \) for the boost controller). The value of the boost capacitor C_B needs to be 100 times that of the total input capacitance of the topside MOSFET(s). The reverse breakdown of the external Schottky diode must be greater than \( V_{IN(MAX)} \) for the buck channels and \( V_{OUT(MAX)} \) for the boost channel.

The external diode D_B can be a Schottky diode or silicon diode, but in either case it should have low leakage and fast recovery. Pay close attention to the reverse leakage at high temperatures where it generally increases substantially.

The topside MOSFET driver for the boost channel includes an internal charge pump that delivers current to the bootstrap capacitor from the BOOST3 pin. This charge current maintains the bias voltage required to keep the top MOSFET on continuously during dropout/overvoltage conditions. The Schottky/silicon diode selected for the boost topside driver should have a reverse leakage less than the available output current the charge pump can supply. Curves displaying the available charge pump current under different operating conditions can be found in the Typical Performance Characteristics section.

A leaky diode D_B in the boost converter can not only prevent the top MOSFET from fully turning on but it can also completely discharge the bootstrap capacitor C_B and create a current path from the input voltage to the BOOST3 pin to INTVCC. This can cause INTVCC to rise if the diode leakage exceeds the current consumption on INTVCC. This is particularly a concern in Burst Mode operation where the load on INTVCC can be very small. There is an internal voltage clamp on INTVCC that prevents the INTVCC voltage from running away, but this clamp should be regarded as a failsafe only. The external Schottky or silicon diode should be carefully chosen such that INTVCC never gets charged up much higher than its normal regulation voltage.

Care should also be taken when choosing the external diode D_B for the buck converters. A leaky diode not only increases the quiescent current of the buck converter, but it can also cause a similar leakage path to INTVCC from \( V_{OUT} \) for applications with output voltages greater than the INTVCC voltage (~5.4V).

Fault Conditions: Buck Current Limit and Current Foldback

The LTC7815 includes current foldback for the buck channels to help limit load current when the output is shorted to ground. If the buck output falls below 70% of its nominal output level, then the maximum sense voltage is progressively lowered from 100% to 40% of its maximum selected value. Under short-circuit conditions with very low duty cycles, the buck channel will begin cycle skipping in order to limit the short-circuit current. In this situation the bottom MOSFET will be dissipating most of the power but less than in normal operation. The short-circuit ripple current is determined by the minimum on-time \( t_{ON(MIN)} \) of the LTC7815 (~40ns), the input voltage and inductor value:

\[
\Delta I_{L(SC)} = t_{ON(MIN)} \left( \frac{V_{IN}}{L} \right)
\]

The resulting average short-circuit current is:

\[
I_{SC} = 40\% \times I_{LIM(MAX)} - \frac{1}{2} \Delta I_{L(SC)}
\]

Fault Conditions: Buck Overvoltage Protection (Crowbar)

The overvoltage crowbar is designed to blow a system input fuse when the output voltage of the one of the buck regulators rises much higher than nominal levels. The crowbar causes huge currents to flow, that blow the fuse to protect against a shorted top MOSFET if the short occurs while the controller is operating.

A comparator monitors the buck output for overvoltage conditions. The comparator detects faults greater than 10% above the nominal output voltage. When this condition is sensed, the top MOSFET of the buck controller is...
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turned off and the bottom MOSFET is turned on until the overvoltage condition is cleared. The bottom MOSFET remains on continuously for as long as the overvoltage condition persists; if VO < returns to a safe level, normal operation automatically resumes.

A shorted top MOSFET for the buck channel will result in a high current condition which will open the system fuse. The switching regulator will regulate properly with a leaky top MOSFET by altering the duty cycle to accommodate the leakage.

Fault Conditions: Over Temperature Protection

At higher temperatures, or in cases where the internal power dissipation causes excessive self heating on chip (such as INTVCC short to ground), the over temperature shutdown circuitry will shut down the LTC7815. When the junction temperature exceeds approximately 170°C, the over temperature circuitry disables the INTVCC LDO, causing the INTVCC supply to collapse and effectively shutting down the entire LTC7815 chip. Once the junction temperature drops back to approximately 155°C, the INTVCC LDO turns back on. Long term overstress (TJ > 125°C) should be avoided as it can degrade the performance or shorten the life of the part.

Frequency Synchronization and Selection

The LTC7815 has an internal phase-locked loop (PLL) comprised of a phase frequency detector, a lowpass filter, and a voltage-controlled oscillator (VCO). This allows the turn-on of the top MOSFET of controller 1 to be locked to the rising edge of an external clock signal applied to the PLLIN/MODE pin. The turn-on of controller 2’s top MOSFET is thus 180 degrees out of phase with the external clock. The phase detector is an edge sensitive digital type that provides zero degrees phase shift between the external and internal oscillators. This type of phase detector does not exhibit false lock to harmonics of the external clock.

If the external clock frequency is greater than the internal oscillator’s frequency, fosc, then current is sourced continuously from the phase detector output, pulling up the VCO input. When the external clock frequency is less than fosc, current is sunk continuously, pulling down the VCO input. If the external and internal frequencies are the same but exhibit a phase difference, the current sources turn on for an amount of time corresponding to the phase difference. The voltage at the VCO input is adjusted until the phase and frequency of the internal and external oscillators are identical. At the stable operating point, the phase detector output is high impedance and the internal filter capacitor, CLP, holds the voltage at the VCO input.

Note that the LTC7815 can only be synchronized to an external clock whose frequency is within range of the LTC7815’s internal VCO, which is guaranteed to be between 0.32MHz to 2.25MHz.

Typically, the external clock (on PLLIN/MODE pin) input high threshold is 1.6V, while the input low threshold is 1.1V. The LTC7815 is guaranteed to synchronize to an external clock that swings up to at least 2.5V and down to 0.5V or less.

Rapid phase-locking can be achieved by using the FREQ pin to set a free-running frequency near the desired synchronization frequency. The VCO’s input voltage is prebiased at a frequency correspond to the frequency set by the FREQ pin. Once prebiased, the PLL only needs to adjust the frequency slightly to achieve phase-lock and synchronization. Although it is not required that the free-running frequency be near external clock frequency, doing so will prevent the operating frequency from passing through a large range of frequencies as the PLL locks.

If the PLLIN/MODE pin is not being driven by an external clock source, the FREQ pin can be tied to SGND, tied to INTVCC or programmed through an external resistor. Tying FREQ to SGND selects 0.94MHz while tying FREQ
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Figure 7. Relationship Between Oscillator Frequency and Resistor Value at the FREQ Pin

Table 1 summarizes the different states in which the FREQ pin can be used.

<table>
<thead>
<tr>
<th>FREQ PIN</th>
<th>PLLIN/MODE PIN</th>
<th>FREQUENCY</th>
</tr>
</thead>
<tbody>
<tr>
<td>0V</td>
<td>DC Voltage</td>
<td>0.94MHz</td>
</tr>
<tr>
<td>INTVCC</td>
<td>DC Voltage</td>
<td>1.44MHz</td>
</tr>
<tr>
<td>Resistor to SGND</td>
<td>DC Voltage</td>
<td>0.32MHz to 2.25MHz</td>
</tr>
<tr>
<td>Any of the Above</td>
<td>External Clock</td>
<td>Phase-Locked to External Clock</td>
</tr>
</tbody>
</table>

Minimum On-Time Considerations

Minimum on-time \( t_{ON(MIN)} \) is the smallest time duration that the LTC7815 is capable of turning on the top MOSFET (bottom MOSFET for the boost controller). It is determined by internal timing delays and the gate charge required to turn on the top MOSFET. Low duty cycle applications may approach this minimum on-time limit and care should be taken to ensure that

\[
 t_{ON(MIN)}_{BUCK} < \frac{V_{OUT}}{V_{IN}(f)} \\
 t_{ON(MIN)}_{BOOST} < \frac{V_{OUT} - V_{IN}}{V_{OUT}(f)}
\]

If the duty cycle falls below what can be accommodated by the minimum on-time, the controller will begin to skip cycles. The output voltage will continue to be regulated, but the ripple voltage and current will increase.

The minimum on-time for the LTC7815 is approximately 45ns for the bucks and 70ns for the boost. However, as the peak sense voltage decreases the minimum on-time for the bucks gradually increases up to about 70ns. This is of particular concern in forced continuous applications with low ripple current at light loads. If the duty cycle drops below the minimum on-time limit in this situation, a significant amount of cycle skipping can occur with correspondingly larger current and voltage ripple.

Efficiency Considerations

The percent efficiency of a switching regulator is equal to the output power divided by the input power times 100%. It is often useful to analyze individual losses to determine what is limiting the efficiency and which change would produce the most improvement. Percent efficiency can be expressed as:

\[
\%\text{Efficiency} = 100\% - \left( L_1 + L_2 + L_3 + \ldots \right)
\]

where \( L_1, L_2, \text{etc.} \) are the individual losses as a percentage of input power.

Although all dissipative elements in the circuit produce losses, four main sources usually account for most of the losses in LTC7815 circuits: 1) IC \( V_{BIAS} \) current, 2) INTVCC regulator current, 3) \( I^2R \) losses, 4) Topside MOSFET transition losses.

1. The \( V_{BIAS} \) current is the DC supply current given in the Electrical Characteristics table, which excludes MOSFET driver and control currents. \( V_{BIAS} \) current typically results in a small (<0.1%) loss.

2. INTVCC current is the sum of the MOSFET driver and control currents. The MOSFET driver current results from switching the gate capacitance of the power MOSFETs. Each time a MOSFET gate is switched from low to high to low again, a packet of charge, \( dQ \), moves from INTVCC to ground. The resulting \( dQ/dt \) is a current...
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out of INTVCC that is typically much larger than the control circuit current. In continuous mode, \( I_{GATECHG} = f(Q_T + Q_B) \), where \( Q_T \) and \( Q_B \) are the gate charges of the topside and bottom side MOSFETs.

Supplying INTVCC from an output-derived source power through EXTVCC will scale the \( V_{IN} \) current required for the driver and control circuits by a factor of (Duty Cycle)/(Efficiency). For example, in a 20V to 5V application, 10mA of INTVCC current results in approximately 2.5mA of \( V_{IN} \) current. This reduces the mid-current loss from 10% or more (if the driver was powered directly from \( V_{IN} \)) to only a few percent.

3. I^2R losses are predicted from the DC resistances of the fuse (if used), MOSFET, inductor, current sense resistor, and input and output capacitor ESR. In continuous mode the average output current flows through \( L \) and \( R_{SENSE} \), but is “chopped” between the topside MOSFET and the synchronous MOSFET. If the two MOSFETs have approximately the same \( R_{DS(ON)} \), then the resistance of one MOSFET can simply be summed with the resistances of \( L \), \( R_{SENSE} \) and ESR to obtain I^2R losses. For example, if each \( R_{DS(ON)} = 30m\Omega \), \( R_L = 50m\Omega \), \( R_{SENSE} = 10m\Omega \) and \( R_{ESR} = 40m\Omega \) (sum of both input and output capacitance losses), then the total resistance is 130m\( \Omega \). This results in losses ranging from 3% to 13% as the output current increases from 1A to 5A for a 5V output, or a 4% to 20% loss for a 3.3V output. Efficiency varies as the inverse square of \( V_{OUT} \) for the same external components and output power level. The combined effects of increasingly lower output voltages and higher currents required by high performance digital systems is not doubling but quadrupling the importance of loss terms in the switching regulator system!

4. Transition losses apply only to the top MOSFET(s) (bottom MOSFET for the boost), and become significant only when operating at high input voltages (typically 15V or greater). Transition losses can be estimated from:

\[
\text{Transition Loss} = (1.7)V_{IN}^2 \cdot I_{0(MAX)} \cdot C_{RSS} \cdot f
\]

Other hidden losses such as copper trace and internal battery resistances can account for an additional 5% to 10% efficiency degradation in portable systems. It is very important to include these “system” level losses during the design phase. The internal battery and fuse resistance losses can be minimized by making sure that \( C_{IN} \) has adequate charge storage and very low ESR at the switching frequency. A 25W supply will typically require a minimum of 20\( \mu \)F to 40\( \mu \)F of capacitance having a maximum of 20m\( \Omega \) to 50m\( \Omega \) of ESR. The LTC7815 2-phase architecture typically halves this input capacitance requirement over competing solutions. Other losses including Schottky conduction losses during dead-time and inductor core losses generally account for less than 2% total additional loss.

Checking Transient Response

The regulator loop response can be checked by looking at the load current transient response. Switching regulators take several cycles to respond to a step in DC (resistive) load current. When a load step occurs, \( V_{OUT} \) shifts by an amount equal to \( \Delta I_{LOAD} \cdot (ESR) \), where ESR is the effective series resistance of \( C_{OUT} \). \( \Delta I_{LOAD} \) also begins to charge or discharge \( C_{OUT} \) generating the feedback error signal that forces the regulator to adapt to the current change and return \( V_{OUT} \) to its steady-state value. During this recovery time \( V_{OUT} \) can be monitored for excessive overshoot or ringing, which would indicate a stability problem. OPTI-LOOP compensation allows the transient response to be optimized over a wide range of output capacitance and ESR values. The availability of the \( I_{TH} \) pin not only allows optimization of control loop behavior, but it also provides a DC coupled and AC filtered closed loop response test point. The DC step, rise time and settling at this test point truly reflects the closed loop response. Assuming a predominantly second order system, phase margin and/or damping factor can be estimated using the percentage of overshoot seen at this pin. The bandwidth can also be estimated by examining the rise time at the pin. The \( I_{TH} \) external components shown in Figure 9 will provide an adequate starting point for most applications.

The \( I_{TH} \) series RC-CC filter sets the dominant pole-zero loop compensation. The values can be modified slightly (from 0.5 to 2 times their suggested values) to optimize
transient response once the final PC layout is done and
the particular output capacitor type and value have been
determined. The output capacitors need to be selected
because the various types and values determine the loop
gain and phase. An output current pulse of 20% to 80%
of full-load current having a rise time of 1µs to 10µs will
produce output voltage and ITH pin waveforms that will
give a sense of the overall loop stability without breaking
the feedback loop.

Placing a power MOSFET directly across the output
capacitor and driving the gate with an appropriate signal
generator is a practical way to produce a realistic load step
condition. The initial output voltage step resulting from
the step change in output current may not be within the
bandwidth of the feedback loop, so this signal cannot be
used to determine phase margin. This is why it is better to
look at the ITH pin signal which is in the feedback loop and
is the filtered and compensated control loop response.

The gain of the loop will be increased by increasing
RC and the bandwidth of the loop will be increased by
decreasing CC. If RC is increased by the same factor that
CC is decreased, the zero frequency will be kept the same,
thereby keeping the phase shift the same in the most
critical frequency range of the feedback loop. The output
voltage settling behavior is related to the stability of the
closed-loop system and will demonstrate the actual overall
supply performance.

A second, more severe transient is caused by switching
in loads with large (>1µF) supply bypass capacitors. The
discharged bypass capacitors are effectively put in parallel
with COUT, causing a rapid drop in VOUT. No regulator can
alter its delivery of current quickly enough to prevent this
sudden step change in output voltage if the load switch
resistance is low and it is driven quickly. If the ratio of
CLOAD to COUT is greater than 1:50, the switch rise time
should be controlled so that the load rise time is limited to
approximately 25 • CLOAD. Thus a 10µF capacitor would
require a 250µs rise time, limiting the charging current
to about 200mA.

Buck Design Example
As a design example for one of the buck channels, assume
V_IN = 12V_NOMINAL, V_IN = 22V_MAX, V_OUT = 3.3V, I_MAX =
5A, VSENSE_MAX = 50mV, and f = 1MHz.

The inductance value is chosen first based on a 30% rip-
ple current assumption. The highest value of ripple cur-
cent occurs at the maximum input voltage. Tie the FREQ
pin with 54.9k resistor to GND, generating approximately
1MHz operation. The inductor ripple current can be cal-
culated from the following equation:

$$\Delta I_L = \frac{V_{OUT}}{(f)(L)} \left(1 - \frac{V_{OUT}}{V_{IN\,(NOMINAL)}}\right)$$

A 1.5µH inductor will produce 32% ripple current. The
peak inductor current will be the maximum DC value plus
one half the ripple current, or 5.8A. Increasing the ripple
current will also help ensure that the minimum on-time
of 45ns is not violated. The minimum on-time occurs at
maximum V_IN:

$$t_{ON\,(MIN)} = \frac{V_{OUT}}{V_{IN\,(MAX)}}(f) = \frac{3.3V}{22V\,(1MHz)} = 150ns$$

The RSENSE resistor value can be calculated by using the
minimum value for the maximum current sense threshold
(43mV):

$$R_{SENSE} \leq \frac{43mV}{5.8A} = 0.007\Omega$$

Choosing 1% resistors: R_A = 25k and R_B = 80.6k yields
an output voltage of 3.38V.

The power dissipation on the top side MOSFET can be
easily estimated. Choosing an Infineon BSZ097N04LSG
MOSFET results in: R_DS(ON) = 11.4mΩ, C_MILLER = 16pF.
At maximum input voltage with T(estimated) = 50°C:

$$P_{MAIN} = \frac{3.3V}{22V} (5A)^2 \left(1 + (0.005)(50^\circ C - 25^\circ C)\right)$$

$$= (11.4mΩ) + (22V)^2 \frac{5A}{2} (2.5Ω)(16pF) \cdot$$

$$\left(\frac{1}{5V - 1.5V} + \frac{1}{1.5V}\right) (1MHz) = 94mW$$

$$P_{SYNC} = \frac{22V - 3.3V}{22V} (5A)^2 (1.125)(11.4mΩ) = 273mW$$
A short-circuit to ground will result in a folded back current of:

\[ I_{SC} = \frac{20 \text{ mV}}{0.007 \Omega} - \frac{1}{2} \left( \frac{40 \text{ ns}(22 \text{ V})}{1.5 \mu\text{H}} \right) = 2.56 \text{ A} \]

with a typical value of \( R_{DS(ON)} \) and \( \zeta = (0.005/\degree\text{C})(25\degree\text{C}) = 0.125. \) The resulting power dissipated in the bottom MOSFET is:

\[ P_{SYNC,SC} = (2.56\text{ A})^2(1.125)(11.4\mu\Omega) = 84\text{ mW} \]

The input capacitor to the buck regulator \( C_{IN} \) is chosen for an RMS current rating of at least 3A at temperature. \( C_{OUT} \) is chosen with an ESR of 0.02Ω for low output ripple. The output ripple in continuous mode will be highest at the maximum input voltage. The output voltage ripple due to ESR is approximately:

\[ V_{ORIPPLE} = R_{ESR}(\Delta I_L) = 0.02\Omega(1.6\text{ A}) = 32\text{ mV}_{P-P} \]

**PC Board Layout Checklist**

When laying out the printed circuit board, the following checklist should be used to ensure proper operation of the IC. Figure 8 illustrates the current waveforms present in the various branches of the 2-phase synchronous buck regulators operating in the continuous mode. Check the following in your layout:

1. Are the top N-channel MOSFETs MTOP1 and MTOP2 located within 1cm of each other with a common drain connection at \( C_{IN} \)? Do not attempt to split the input decoupling for the two channels as it can cause a large resonant loop.

2. Are the signal and power grounds kept separate? The combined IC signal ground pin and the ground return of \( C_{INTVCC} \) must return to the combined \( C_{OUT} \) terminals. The path formed by the top N-channel MOSFET, Schottky diode and the \( C_{IN} \) capacitor should have short leads and PC trace lengths. The output capacitor (-) terminals should be connected as close as possible to the (-) terminals of the input capacitor by placing the capacitors next to each other and away from the Schottky loop described above.

3. Do the LTC7815 \( V_{FB} \) pins’ resistive dividers connect to the (+) terminals of \( C_{OUT} \)? The resistive divider must be connected between the (+) terminal of \( C_{OUT} \) and signal ground. The feedback resistor connections should not be along the high current input feeds from the input capacitor(s).

4. Are the SENSE- and SENSE+ leads routed together with minimum PC trace spacing? The filter capacitor between SENSE+ and SENSE- should be as close as possible to the IC. Ensure accurate current sensing with Kelvin connections at the sense resistor.

5. Is the \( INTVCC \) decoupling capacitor connected close to the IC, between the \( INTVCC \) and the power ground pins? This capacitor carries the MOSFET drivers’ current peaks. An additional 1µF ceramic capacitor placed immediately next to the \( INTVCC \) and PGND pins can help improve noise performance substantially.

6. Keep the switching nodes (SW1, SW2, SW3), top gate nodes (TG1, TG2, TG3), and boost nodes (BOOST1, BOOST2, BOOST3) away from sensitive small-signal nodes, especially from the opposite channel’s voltage and current sensing feedback pins. All of these nodes have very large and fast moving signals and therefore should be kept on the output side of the LTC7815 and occupy minimum PC trace area.

7. Use a modified star ground technique: a low impedance, large copper area central grounding point on the same side of the PC board as the input and output capacitors with tie-ins for the bottom of the \( INTVCC \) decoupling capacitor, the bottom of the voltage feedback resistive divider and the SGND pin of the IC.

**PC Board Layout Debugging**

Start with one controller on at a time. It is helpful to use a DC-50MHz current probe to monitor the current in the inductor while testing the circuit. Monitor the output switching node (SW pin) to synchronize the oscilloscope to the internal oscillator and probe the actual output voltage as well. Check for proper performance over the operating voltage and current range expected in the.
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The duty cycle percentage should be maintained from cycle to cycle in a well-designed, low noise PCB implementation. Variation in the duty cycle at a subharmonic rate can suggest noise pickup at the current or voltage sensing inputs or inadequate loop compensation. Overcompensation of the loop can be used to tame a poor PC layout if regulator bandwidth optimization is not required. Only after each controller is checked for its individual performance should both controllers be turned on at the same time. A particularly difficult region of operation is when one controller channel is nearing its current comparator trip point when the other channel is turning on its top MOSFET. This occurs around 50% duty cycle on either channel due to the phasing of the internal clocks and may cause minor duty cycle jitter.

Reduce $V_{IN}$ from its nominal level to verify operation of the regulator in dropout. Check the operation of the undervoltage lockout circuit by further lowering $V_{IN}$ while monitoring the outputs to verify operation.

An embarrassing problem, which can be missed in an otherwise properly working switching regulator, results when the current sensing leads are hooked up backwards. The output voltage under this improper hookup will still be maintained but the advantages of current mode control will not be realized. Compensation of the voltage loop will be much more sensitive to component selection. This behavior can be investigated by temporarily shorting out the current sensing resistor—don’t worry, the regulator will still maintain control of the output voltage.
Figure 8. Branch Current Waveforms for Bucks
TYPICAL APPLICATIONS

Figure 9. High Efficiency Wide Input Range 2.1MHz Dual 5V/3.3V Regulator

* WHEN $V_{IN} < 3.5V$, MAXIMUM LOAD CURRENT AVAILABLE OF CHG IS REDUCED
* $V_{OUTS}$ IS 10V WHEN $V_{IN} < 10V$ FOLLOWS $V_{OUT}$ WHEN $V_{IN} > 10V$
* OUTPUT CURRENT CAPABILITY AT HIGH INPUT VOLTAGES MAY BE LIMITED BY THE THERMAL CHARACTERISTICS OF THE OVERALL SYSTEM AND PRINTED CIRCUIT BOARD DESIGN

For more information www.linear.com/LTC7815
Figure 10. High Efficiency Wide Input Range 600kHz Triple 5V/8.5V/18V Regulator
RELATED PARTS

<table>
<thead>
<tr>
<th>PART NUMBER</th>
<th>DESCRIPTION</th>
</tr>
</thead>
<tbody>
<tr>
<td>LTC3859AL</td>
<td>38V Triple Output, Buck/Buck/Boost Synchronous Controller PLL Fixed Operating Frequency 50kHz to 900kHz</td>
</tr>
<tr>
<td></td>
<td>4.5V (Down to 2.5V After Start-Up) ( \leq V_{IN} \leq 38V ), ( I_{O} = 28\mu A ) Buck ( V_{OUT} ) Range: 0.8V to 24V, Boost ( V_{OUT} ) Up to 60V</td>
</tr>
<tr>
<td>VT7812</td>
<td>38V Synchronous Boost-Buck Controller Low EMI and Low Input/Output Ripple</td>
</tr>
<tr>
<td></td>
<td>4.5V (Down to 2.5V After Start-Up) ( \leq V_{IN} \leq 38V ), Boost ( V_{OUT} ) up to 60V, Buck ( V_{OUT} ) Range: 0.8V to 24V, ( I_{O} = 29\mu A ), 5mm x 5mm QFN-32</td>
</tr>
<tr>
<td>LTC3857/LTC3857-1</td>
<td>38V Low ( I_{O} ), Dual Output 2-Phase Synchronous Step-Down Controller with 99% Duty Cycle</td>
</tr>
<tr>
<td>LTC3858/LTC3858-1</td>
<td>4V ( \leq V_{IN} \leq 38V ), 0.8V ( \leq V_{OUT} \leq 24V ), ( I_{O} = 50\mu A / 170\mu A ), PLL Fixed Operating Frequency 50kHz to 900kHz</td>
</tr>
<tr>
<td>VT7800</td>
<td>60V Low ( I_{O} ), High Frequency Synchronous Step-Down Controller</td>
</tr>
<tr>
<td></td>
<td>4V ( \leq V_{IN} \leq 60V ), 0.8V ( \leq V_{OUT} \leq 24V ), ( I_{O} = 50\mu A ), PLL Fixed Frequency 320kHz to 2.25MHz</td>
</tr>
<tr>
<td>VT7899</td>
<td>60V Low ( I_{O} ), Triple Output, Buck/Buck/Boost Synchronous Controller</td>
</tr>
<tr>
<td></td>
<td>4.5V (Down to 2.2V After Start-Up) ( \leq V_{IN} \leq 60V ), ( I_{O} = 28\mu A ), Buck and Boost ( V_{OUT} ) Up to 60V</td>
</tr>
<tr>
<td>VT7897</td>
<td>65V Low ( I_{O} ), Single Output 2-Phase Synchronous Boost Controller with Input/Output Protection</td>
</tr>
<tr>
<td></td>
<td>4.5V ( \leq V_{IN} \leq 65V ), ( V_{OUT} ) Up to 60V, ( I_{O} = 55\mu A ), PLL Fixed Frequency 50kHz to 900kHz</td>
</tr>
<tr>
<td>VT7892</td>
<td>60V Low ( I_{O} ), Dual 2-Phase Synchronous Step-Down Controller with Adjustable Gate Drive Voltage</td>
</tr>
<tr>
<td></td>
<td>4.5V ( \leq V_{IN} \leq 60V ), 0.8V ( \leq V_{OUT} \leq 0.99V_{IN} ), ( I_{O} = 50\mu A ), PLL Fixed Frequency 50kHz to 900kHz</td>
</tr>
</tbody>
</table>