15V Buck-Boost Converters with Ultralow 1.3µA Quiescent Current are Tailored to Micropower Applications and the Internet of Things

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The proliferation of wireless sensors supporting the “Internet of Things” has increased the need for small, efficient power converters tailored to untethered low power devices. The new LTC3129 and LTC3129-1 are designed to satisfy this need. The LTC3129 and LTC3129-1 are monolithic buck-boost DC/DC converters with an input voltage range of 2.42V to 15V. The LTC3129 has an output voltage range of 1.4V to 15.75V, while the LTC3129-1 offers eight pin-selectable fixed output voltages between 1.8V and 15V. Both parts can supply a minimum output current of 200mA in buck mode.

Low power sensors can take advantage the LTC3129’s and LTC3129-1’s zero current when disabled (on both VIN and VOUT), and a quiescent current on VIN of just 1.3µA when power saving Burst Mode® operation is selected, making them ideal for power and energy harvesting applications, where high efficiency at extremely light loads is crucial. Their buck-boost architecture makes them well suited to a wide variety of power sources.

Other key features of the LTC3129 and LTC3129-1 include a fixed 1.2MHz operating frequency, current mode control, internal loop compensation, automatic Burst Mode operation or low noise PWM mode, an accurate RUN pin threshold to allow the UVLO threshold to be programmed, a power good output and an MPCC (maximum power point control) function for optimizing power transfer when operating from photovoltaic cells.

The compact 3mm × 3mm QFN package and the high level of integration ease the LTC3129/LTC3129-1’s placement into space-constrained applications. Only a few external components and an inductor, which can be as small as 2mm × 3mm, are required to complete the power supply design. Internal loop compensation further simplifies the design process.

3.3V CONVERSER OPERATES FROM INDOOR LIGHT USING A SMALL SOLAR CELL

The circuit in Figure 1 exploits the unique ability of the LTC3129 and LTC3129-1 to start up and operate from an input power source as weak as 7.5 microwatts—making them capable of operating from small (less than 1in²), low cost solar cells with indoor light levels less than 200-lux. This enables such applications as indoor light powered wireless sensors, where the DC/DC converter must support an extremely low average power requirement, due to a low duty cycle of operation, from very low available power, while consuming as little power as possible.

To make this low current start-up possible, the LTC3129 and LTC3129-1 draw a meager two microamps of current (less in shutdown) until three conditions are satisfied:

- The RUN pin must exceed 1.22V (typical).
- The VIN pin must exceed 1.9V (typical).
- VCC (which is internally generated from VIN but can also be supplied externally) must exceed 2.25V (typical).

Until all three of these conditions are satisfied, the part remains in a “soft-shutdown” or standby state, drawing just 2µA.
The LTC3129 and LTC3129-1 can start up and operate from an input power source as \textit{weak} as 7.5 \textit{microwatts}—making them capable of operating from small (less than 1in$^2$), low cost solar cells with indoor light levels less than 200-lux. This enables such applications as indoor light powered wireless sensors.

Figure 2. Solar powered converter with coin cell backup

This allows a weak input source to charge the input storage capacitor until the voltage is high enough to satisfy all three previously mentioned conditions, at which point the LTC3129/LTC3129-1 begins switching, and $V_{\text{OUT}}$ rises to regulation. Provided the input capacitor has sufficient stored energy, the input voltage at which the part exits UVLO can be set anywhere from 2.4V to 1V using the external resistive divider on the RUN pin. With a RUN pin current of less than 1mA typical, high value resistors may be used to minimize current draw on $V_{\text{IN}}$.

In the application example shown in Figure 1, the energy stored on $C_{\text{IN}}$ is used to bring $V_{\text{OUT}}$ into regulation once the converter starts. If the average power demand on $V_{\text{OUT}}$ is less than the power delivered by the solar cell, the LTC3129/LTC3129-1 remains in Burst Mode operation, and $V_{\text{OUT}}$ remains in regulation.

If the average output power demand exceeds the input power available, then $V_{\text{IN}}$ drops until UVLO is reached, at which point the converter reenters soft-shutdown. At this point, $V_{\text{IN}}$ begins recharging, allowing the cycle to repeat. In this hiccup mode of operation, $V_{\text{IN}}$ is positioned hysteretically about the UVLO point, with a $V_{\text{IN}}$ ripple of approximately 290mV in this example. This ripple is set by the 100mV hysteresis at the RUN pin, gained up by the UVLO divider ratio.

Note that by setting the converter’s UVLO voltage to the MPP (maximum power point) voltage for the chosen solar cell (typically between 70% to 80% of the open-circuit voltage), the cell always operates near its maximum power transfer voltage (unless the average load requirement is less than the power output of the solar cell, in which case $V_{\text{IN}}$ climbs and remains above the UVLO voltage).

To further optimize efficiency and eliminate unnecessary loading of $V_{\text{OUT}}$, the LTC3129/LTC3129-1 does not draw any current from $V_{\text{OUT}}$ during soft-start or at any time if Burst Mode operation is selected. This prevents the converter from discharging $V_{\text{OUT}}$ during soft-start, thereby preserving charge on the output capacitor. In fact, when the LTC3129 is sleeping, there is no current draw at all on $V_{\text{OUT}}$. In the case of the LTC3129-1, the $V_{\text{OUT}}$ current draw is sub-microamp, due to the high resistance internal feedback divider.

\textbf{ADDING A BATTERY BACKUP}

In many solar powered applications, a backup battery provides power when solar power is insufficient. Figure 2 shows an application where a primary lithium coin cell and a few external components have been added to the converter from the previous example to provide backup power to the output in the event that the light source is unable to provide the necessary power to maintain $V_{\text{OUT}}$. The LTC3129 is used in this case, allowing $V_{\text{OUT}}$ to be programmed for 3.2V to better match the voltage of the coin cell.

In this example, the battery is used on the output side of the converter, and the LTC3129 is set to regulate $V_{\text{OUT}}$ slightly
The LTC3129-1 can operate at high efficiency over a wide range of loads and input voltages, with a minimal number of external components. The flexibility of running seamlessly from a wide variety of power sources is an asset in critical field applications, such as military radios.

above the battery voltage. This assures that there is no load on the battery whenever \( V_{\text{OUT}} \) can be powered by the solar input. In the event that \( V_{\text{OUT}} \) droops due to insufficient light to power the load, the \( \text{PGOOD} \) output from the LTC3129 goes low, switching the load from the converter output to the battery, thus holding \( V_{\text{OUT}} \) at the battery voltage. During this time, the converter’s input and output capacitors are able to recharge (if some light is available), enabling the load to be periodically switched from the battery back to the converter by the \( \text{PGOOD} \) signal. In this manner the load is powered by the solar input as much as possible, and the battery is only used in a time-shared manner, extending its life.

The diode connected from \( \text{PGOOD} \) to \( V_{\text{CC}} \) is used to hold \( \text{PGOOD} \) low during start-up, before \( V_{\text{CC}} \) (and therefore \( \text{PGOOD} \)) is valid.

CHOOSING WHERE TO PUT THE BACKUP BATTERY

In the previous example, the backup battery was placed on the output. For light load applications, this has the advantage of not exposing the battery—which may be a low capacity battery with high internal resistance—to relatively high converter start-up input current bursts, causing significant battery droop and lossy internal power dissipation, in turn reducing battery life.

The disadvantages of putting the backup battery on the output of the converter are that the battery voltage must be well matched to the desired output voltage, and it must have a relatively flat discharge curve so as to maintain reasonable regulation of \( V_{\text{OUT}} \). The 3V lithium cell satisfies both of these requirements.

Putting the backup battery on the input side of the converter allows its voltage to be different from the desired output voltage, but it must be able to withstand the higher currents that the converter draws during start-up or load transients. If used on the input side, a lithium-thionyl chloride battery is generally a better choice for long life applications. It can be diode-or’d with the solar cell or switched in and out with MOSFET switches, in a similar manner to Figure 2.

5V CONVERTER OPERATES SEAMLESSLY FROM A VARIETY OF INPUT SOURCES

The ability of the LTC3129-1 to operate at high efficiency over a wide range of loads and input voltages with a minimal number of external components is illustrated in Figure 3. In this example, the output, which has been programmed for 5V using the \( \text{VS1–VS3} \) pins, can be powered from a 5V USB input, a variety of battery options or a 3V to 15V wall adapter. The flexibility of running seamlessly from a wide variety of power sources is an asset in critical field applications, such as military radios.

The LTC3129-1’s low \( I_{\text{Q}} \) of just 1.3\( \mu \text{A} \) in sleep mode, combined with a high resistance internal feedback divider, enables it to maintain high efficiency over a wide range of loads, as shown in Figure 4. At a load current of just 100\( \mu \text{A} \), the efficiency is ~80% over nearly the entire \( V_{\text{IN}} \) range. This is an important feature for extending battery life in applications that spend a large percentage of the time in a low power state.

The line step response (\( V_{\text{IN}} \) is stepped from 5V to 12V) is shown in Figure 5, with \( V_{\text{OUT}} \) measured under both heavy and light load conditions. At a load of 200mA, the part is operating in PWM mode, and \( V_{\text{OUT}} \) overshoot is only 150mV (3%). At a load of 10mA, the part is in Burst Mode operation, with a burst ripple of
The LTC3129 and LTC3129-1 include a maximum power point control (MPPC) feature that allows the converter to servo \( V_{IN} \) to a minimum voltage under load, as set by the user. Regulating \( V_{IN} \) maintains optimal power transfer in applications using higher current solar cells or other sources with high internal resistance. This feature prevents the converter from crashing the input voltage when operating from a current-limited source.

100m\( V_{PK-PK} \) (2%), and less than 100mV of \( V_{OUT} \) overshoot due to the line step.

The \( V_{CC} \) pin is the output of an internal \( LDO \) that generates a nominal 3.9V from \( V_{IN} \) to power the ic. The \( LDO \) is designed so that it can be externally back-driven up to 5V. In this example, an optional bootstrap diode is shown from \( V_{OUT} \) to \( V_{CC} \).

The addition of this external bootstrap diode has two advantages. First, it improves efficiency at low \( V_{IN} \) and high load current by providing a higher gate drive voltage to the internal switches, lowering their \( r_{DS(ON)} \). Also, at high \( V_{IN} \) and light load, it improves efficiency by reducing the power lost in the internal \( LDO \) used to generate \( V_{CC} \). (Note that the \( V_{CC} \) pin must not be raised above 6V, so it cannot be diode-connected to higher output voltages.)

The second advantage of adding a bootstrap diode is that it allows operation from a lower \( V_{IN} \). After start-up, if \( V_{CC} \) is held above its minimum value of 2.4V (by the output voltage in this case), then the converter can operate at a lower input voltage, down to 1.75V, where the fixed internal \( V_{IN} \) UVLO threshold is reached. This capability extends the usable voltage range enough to make it possible to run from two depleted alkaline batteries. Note that if the battery voltage is below 2.4V and the converter is shut down (or \( V_{OUT} \) is shorted), the ic is not able to restart.

The MPPC control loop operates by reducing the average inductor current commanded by the converter, thus maintaining the minimum programmed \( V_{IN} \) voltage under load. This voltage is set using an external resistor divider connected to \( V_{IN} \) and the MPPC pin, as shown in the supercapacitor charging example of Figure 6. The MPPC control loop is designed to be stable with a minimum input capacitance of 2.2\( \mu F \).
The LTC3129 and LTC3129-1 monolithic buck-boost DC/DC converters offer exceptional low power performance and power source flexibility demanded by real-world wireless sensor and portable electronic instruments. The ultralow 1.3µA quiescent current and high conversion efficiency can extend battery lifetime indefinitely if used in concert with energy harvesting.

Note that reducing the inductor current under MPPC would cause the output voltage to droop if it were driving a conventional load. Therefore, most applications employing MPPC involve charging a large storage capacitor (or trickle charging a battery) from a solar cell. The MPPC feature assures that the capacitor or battery is charged at the highest current possible, while operating the solar cell at its maximum power point voltage.

It is important to note that when the LTC3129/LTC3129-1 is in MPPC control, Burst Mode operation is inhibited, and the \( V_{IN} \) quiescent current is several milliamps, since the IC is switching continuously at 1.2MHz. Therefore, MPPC is not appropriate for use with sources that cannot supply a minimum of about 10mA. For applications requiring an MPPC-like function with very weak input sources, the accurate Run pin should be used to program a UVLO threshold, as described in the example of Figure 1.

**INTRINSIC SAFETY USING MPPC**

The MPPC feature can be used in other applications, including those designed for intrinsic safety, where the input source has a series current limiting resistor between it and the DC/DC converter. In this case, the MPPC loop prevents the LTC3129/LTC3129-1 from drawing too much current, especially during start-up when the output capacitor is being charged, and crashing the input voltage. An example of this is shown in Figure 7, where the input voltage is maintained at a minimum of 3V, as set by the MPPC divider.

In this case, because the input capacitor value is limited to just 10µF for safety (less than the recommended minimum value of 22µF when using MPPC), an additional RC compensation network is added to the MPPC pin for improved phase margin of the MPPC loop.

**INPUT CURRENT LIMIT USING MPPC**

Note that the MPPC feature can be used to set the maximum input current to a given value. By choosing a series input resistor value and setting the MPPC voltage to a value below a fixed input source voltage, the maximum input current is limited to:

\[
I_{IN} = \frac{V_{SOURCE} - V_{MPPC}}{R_{SERIES}}
\]

**CONCLUSION**

The LTC3129 and LTC3129-1 monolithic buck-boost DC/DC converters offer exceptional low power performance and power source flexibility demanded by real-world wireless sensor and portable electronic instruments. The ultralow 1.3µA quiescent current and high conversion efficiency can extend battery lifetime indefinitely if used in concert with energy harvesting.

A choice of maximum power point control schemes allows optimization of power performance over a wide range of power sources. The expanding reach of wireless monitoring applications demands easy to use, efficient and flexible DC/DC power converter solutions. The LTC3129 and LTC3129-1 are ready to meet this challenge. ■

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**Figure 7. 3.3V Converter using MPPC for intrinsic safety application**

**NOTE:** \( R_C \) AND \( C_C \) HAVE BEEN ADDED FOR IMPROVED MPPC LOOP STABILITY WHEN USING AN INPUT CAPACITOR VALUE LESS THAN THE RECOMMENDED MINIMUM OF 22µF